

# Plasma-Based CH<sub>4</sub> Conversion into Higher Hydrocarbons and H<sub>2</sub>: Modeling to Reveal the Reaction Mechanisms of Different Plasma Sources

Stijn Heijkers,\* Maryam Aghaei, and Annemie Bogaerts\*

Cite This: *J. Phys. Chem. C* 2020, 124, 7016–7030

Read Online

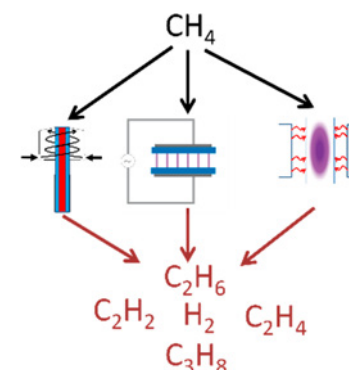
ACCESS |

Metrics & More

Article Recommendations

Supporting Information

**ABSTRACT:** Plasma is gaining interest for CH<sub>4</sub> conversion into higher hydrocarbons and H<sub>2</sub>. However, the performance in terms of conversion and selectivity toward different hydrocarbons is different for different plasma types, and the underlying mechanisms are not yet fully understood. Therefore, we study here these mechanisms in different plasma sources, by means of a chemical kinetics model. The model is first validated by comparing the calculated conversions and hydrocarbon/H<sub>2</sub> selectivities with experimental results in these different plasma types and over a wide range of specific energy input (SEI) values. Our model predicts that vibrational–translational nonequilibrium is negligible in all CH<sub>4</sub> plasmas investigated, and instead, thermal conversion is important. Higher gas temperatures also lead to a more selective production of unsaturated hydrocarbons (mainly C<sub>2</sub>H<sub>2</sub>) due to neutral dissociation of CH<sub>4</sub> and subsequent dehydrogenation processes, while three-body recombination reactions into saturated hydrocarbons (mainly C<sub>2</sub>H<sub>6</sub>, but also higher hydrocarbons) are dominant in low temperature plasmas.



## 1. INTRODUCTION

The conversion of methane (CH<sub>4</sub>) into higher hydrocarbons and H<sub>2</sub> is gaining interest as an alternative to steam reforming of crude-oil derivatives to form light olefins.<sup>1</sup> These olefins are the main building blocks in the chemical industry for fibers, synthetic rubbers, and other organic compounds.<sup>2,3</sup> Usually, CH<sub>4</sub> conversion is performed thermally, using high energy input and temperatures to activate the molecule.<sup>4</sup> Catalysts can make the process more efficient and/or selective, but catalyst instability due to carbon deposition is a major drawback.<sup>2</sup>

Plasma technology is gaining increasing interest for the nonoxidative conversion of CH<sub>4</sub>, overcoming most of the drawbacks of thermal processes.<sup>5</sup> Plasma is created by applying electric energy to a gas. It is an ionized gas, consisting of various chemically active species (i.e., various types of radicals, ions, excited atoms and molecules, and electrons), besides the neutral gas molecules. The electrons in the plasma gain most of the applied electric energy, because of their small mass, and they activate the molecules by excitation, ionization, and dissociation, creating the above-mentioned reactive species, which can further react to form new molecules. This allows chemical conversions to occur at lower temperatures (even up to room temperature) than in thermal conditions.<sup>5</sup> Plasma is also very flexible and can easily be switched on/off, so it can use intermittent green electricity, which cannot be stored on the grid.<sup>6</sup>

Various types of plasma configurations have been applied already for CH<sub>4</sub> conversion, as summarized by Scapinello et al.<sup>5</sup> The most commonly used plasma types are dielectric barrier discharges (DBDs), microwave (MW), and gliding arc (GA)

plasmas. DBDs are created by applying an electric potential difference between two electrodes, of which at least one is covered by a dielectric barrier. They typically operate at (or slightly above) room temperature, and conversions were reported in the range between 1%<sup>7</sup> and 47%,<sup>8</sup> for a specific energy input (SEI, i.e., ratio of plasma power over gas flow rate) ranging between 0.1 and 300 kJ L<sup>-1</sup>. Ethane (C<sub>2</sub>H<sub>6</sub>) is one of the main products formed, with selectivities ranging between 20%<sup>8</sup> and ca. 60%,<sup>9</sup> followed by the other C<sub>2</sub> hydrocarbons (i.e., ethylene (C<sub>2</sub>H<sub>4</sub>) and acetylene (C<sub>2</sub>H<sub>2</sub>)), C<sub>3</sub>–C<sub>5</sub> compounds and soot. According to Scapinello et al.<sup>5</sup> the best overall result in a DBD, in terms of energy efficiency, conversion and product formation, was obtained by Xu and Tu,<sup>10</sup> with a CH<sub>4</sub> conversion of 11%, C<sub>2</sub>H<sub>6</sub> selectivity of 34%, a selectivity of 19% for the other C<sub>2</sub> hydrocarbons, and the remainder being C<sub>3</sub>–C<sub>4</sub> hydrocarbons and soot. These results were obtained at an SEI of 9 kJ L<sup>-1</sup> (or 2.1 eV molec<sup>-1</sup>), yielding a rather high energy cost for CH<sub>4</sub> conversion of 20 eV molec<sup>-1</sup> and a low energy efficiency of 3.4%.

MW and GA plasmas operate at higher temperatures (typically 1000–3000 K), and are therefore called “warm plasmas”.<sup>6,11</sup> They produce more unsaturated compounds, such

Received: January 4, 2020

Revised: February 28, 2020

Published: March 4, 2020

Table 1. Species Included in the Model

molecules	charged species	radicals	excited species
CH <sub>4</sub> , H <sub>2</sub> , C <sub>2</sub> H <sub>6</sub> , C <sub>2</sub> H <sub>4</sub> , C <sub>2</sub> H <sub>2</sub> , C <sub>3</sub> H <sub>8</sub> , C <sub>3</sub> H <sub>6</sub> , C <sub>4</sub> H <sub>10</sub>	CH <sub>4</sub> <sup>+</sup> , CH <sub>5</sub> <sup>+</sup> , CH <sub>3</sub> <sup>+</sup> , CH <sub>2</sub> <sup>+</sup> , CH <sup>+</sup> , C <sub>2</sub> <sup>+</sup> , C <sup>+</sup> , H <sup>+</sup> , H <sub>2</sub> <sup>+</sup> , H <sub>3</sub> <sup>+</sup> , C <sub>2</sub> H <sub>6</sub> <sup>+</sup> , C <sub>2</sub> H <sub>5</sub> <sup>+</sup> , C <sub>2</sub> H <sub>4</sub> <sup>+</sup> , C <sub>2</sub> H <sub>3</sub> <sup>+</sup> , C <sub>2</sub> H <sub>2</sub> <sup>+</sup> , C <sub>2</sub> H <sup>+</sup> electrons	CH <sub>3</sub> , CH <sub>2</sub> , CH, C <sub>2</sub> H, C <sub>2</sub> , C, H, C <sub>2</sub> H <sub>5</sub> , C <sub>2</sub> H <sub>3</sub> , C <sub>3</sub> H <sub>7</sub> , C <sub>3</sub> H <sub>5</sub> , C <sub>4</sub> H <sub>9</sub>	CH <sub>4</sub> (V1–V4), CH <sub>4</sub> (J3, J4), H <sub>2</sub> (V1–V14)

as C<sub>2</sub>H<sub>2</sub>. The conversions in MW plasmas range from 5% until above 90%,<sup>12</sup> at SEI values varying between 6.8 and 360 kJ L<sup>-1</sup>.<sup>12,13</sup> The corresponding C<sub>2</sub>H<sub>2</sub> selectivities vary from below 10%<sup>12</sup> until approximately 90%,<sup>14</sup> depending on the input power and gas pressure used, with higher pressures and/or powers producing more C<sub>2</sub>H<sub>2</sub>. The best result was obtained by Heintze and Magureanu<sup>12</sup> at low pressure (30 mbar) and an SEI of 28 kJ L<sup>-1</sup> (or 6.5 eV molec<sup>-1</sup>), yielding a CH<sub>4</sub> conversion of 94%, an C<sub>2</sub>H<sub>2</sub> selectivity of 65%, followed mainly by C<sub>2</sub>H<sub>4</sub> (10%) and C<sub>2</sub>H<sub>6</sub> (2%), and an energy cost of 6.9 eV molec<sup>-1</sup> or energy efficiency of 23%.

Likewise, for GA plasmas, CH<sub>4</sub> conversions were reported from 0.2%<sup>15</sup> until 92%,<sup>11</sup> for SEI values between 2 and 42 kJ L<sup>-1</sup>,<sup>11,16</sup> and with C<sub>2</sub>H<sub>2</sub> selectivities between 5%<sup>17</sup> and nearly 100%.<sup>15</sup> The best result was obtained by Polak,<sup>18</sup> reporting a CH<sub>4</sub> conversion of 86% and an C<sub>2</sub>H<sub>2</sub> selectivity of 88%, followed by C<sub>2</sub>H<sub>4</sub> (3%), at an SEI of 14 kJ L<sup>-1</sup> (or 3.2 eV molec<sup>-1</sup>). This resulted in a quite high energy efficiency of 49% and a low energy cost of 3.7 eV molec<sup>-1</sup>.

Although the above plasma types show potential for CH<sub>4</sub> conversion into light olefins, only high power thermal arc discharges are up to now able to approach thermodynamic equilibrium conversions.<sup>5,18</sup> Therefore, more research is needed to improve the performance of the above plasma reactors. Specifically, we need to gain more knowledge on the most important reaction pathways in these kind of plasmas, to optimize the formation of higher hydrocarbons. Indeed, it is clear from the above that different plasma reactors yield very different hydrocarbon selectivities and CH<sub>4</sub> conversions, but the underlying reasons have not yet been studied in detail. A broad picture of possible pathways was presented by Scapinello et al.,<sup>5</sup> but to our knowledge, the importance of the different pathways in different reactors has not yet been clarified.

Therefore, in the present paper, we study the different reaction pathways of CH<sub>4</sub> conversion and (mainly) C<sub>2</sub> hydrocarbon and H<sub>2</sub> formation, using 0D chemical kinetics modeling, in the three most important plasma reactors discussed above.

A 0D chemical kinetics model is the most appropriate choice for describing a detailed plasma chemistry. In literature, some models have been presented already for CH<sub>4</sub> conversion in a DBD,<sup>19–22</sup> MW,<sup>23</sup> and GA plasma.<sup>24</sup> Also, CH<sub>4</sub>/H<sub>2</sub> mixtures were modeled in moderate pressure MW plasmas, albeit for another application, i.e., plasma-assisted diamond deposition.<sup>25,26</sup> However, electron impact excitation of the internal degrees of freedom, such as vibrational and rotational excitation of CH<sub>4</sub>, which might be important in warm plasmas (MW and GA plasmas) have not yet been taken into account into these plasma models. Moreover, a detailed comparison between the mechanisms in DBD, GA, and MW plasmas, based on such models, has not been performed yet. Hence, this will be the focus of the present paper.

## 2. MODEL DESCRIPTION

First, we will give a short outline of the 0D model and the chemistry used to describe CH<sub>4</sub> conversion, followed by

explaining the assumptions made in the 0D approach to describe the different plasma reactors.

**2.1. 0D Model Equations and Chemistry.** The conservation eq 1 in a 0D model is solved for all species (see below):

$$\frac{\partial n_s}{\partial t} = \sum_{i=1}^j [(a_{s,i}^R - a_{s,i}^L)R_i] \quad (1)$$

where  $n_s$  is the density of species  $s$  (in cm<sup>-3</sup>),  $j$  the total number of reactions in which that particular species is produced or consumed,  $a_{s,i}^L$  and  $a_{s,i}^R$  the stoichiometric coefficients at the left-hand side and right-hand side of a particular reaction equation, and  $R_i$  the rate of that reaction (in cm<sup>-3</sup> s<sup>-1</sup>), given by

$$R_i = k_i \prod_s n_s^{a_{s,i}} \quad (2)$$

where  $k_i$  is the rate constant (in cm<sup>3</sup> s<sup>-1</sup> or cm<sup>6</sup> s<sup>-1</sup> for two-body or three-body reactions, respectively) and  $a_{s,i}$  was defined above.

The chemistry set applied in this study is based on the pure CH<sub>4</sub> chemistry part of the models developed by Snoeckx et al.<sup>27</sup> and Cleiren et al.,<sup>28</sup> extended with excitation and relaxation of the lowest vibrational and rotational levels. The set contains 57 different species (see Table 1), i.e., eight ground state molecules, 12 radicals, 16 ions, the electrons, six excited species of CH<sub>4</sub>, and 14 of H<sub>2</sub>. These species interact with each other through various chemical reactions. In total, 2174 reactions are included in our model, of which 378 are electron impact reaction, 380 are ionic reactions, 507 are neutral reactions, as well as 713 are vibration-translation (VT), and 196 are vibration-vibration (VV) relaxation reactions for CH<sub>4</sub> and H<sub>2</sub>.

We solve this 0D model with the ZDPlaskin code.<sup>29</sup> The rate coefficients of the electron impact reactions are calculated from the corresponding energy-dependent cross sections and the electron energy distribution function, using the built-in Boltzmann solver BOLSIG+.<sup>30</sup> The rate coefficients of the other (i.e., heavy particle) reactions are adopted from literature. They are often a function of the gas temperature. Details of the CH<sub>4</sub> and H<sub>2</sub> vibrational levels and their reactions are given in the Supporting Information (SI, Table S.1). In addition, the full list of all the reactions and their corresponding rate coefficients, as well as the references of the cross sections used, are presented in Tables S.2–S.5 of the SI.

**2.2. Modeling the Different Plasma Reactors with a 0D Approach.** **2.2.1. General Aspects.** In all simulations, we made some general approximations, independent of the plasma reactor used:

1. Gas expansion can occur upon conversion of CH<sub>4</sub>, e.g., when two new species are formed out of one, so we calculate the gas pressure and mass flow rate at every time step from the actual species densities, gas temperature, and velocity. To conserve the gas pressure and mass flow rate, the species densities (as calculated with the above conservation equations; see eq 1) and velocities are then corrected to account for this effect, following the method of Kozak and Bogaerts.<sup>31</sup>

- The gas temperature is calculated self-consistently for the MW plasma in the same manner as done by Kozak and Bogerts,<sup>31</sup> and a detailed description is given in the SI. For the DBD and the GA plasma, we adopt a temperature profile, as explained below.
- A 0D model calculates the species densities as a function of time only, and neglects spatial variations. However, the time evolution can be translated into a spatial evolution (i.e., as a function of position in the plasma reactor) by means of the gas flow rate. In this way, local variations in the applied plasma power can be implemented in the model, as power pulses as a function of time (see details below).
- The conversion of CH<sub>4</sub> is calculated as

$$\chi_{\text{CH}_4}(\%) = 100\% \frac{n_{\text{CH}_4,i}(\text{cm}^{-3})v_i(\text{cm s}^{-1}) - n_{\text{CH}_4,f}(\text{cm}^{-3})v_f(\text{cm s}^{-1})}{n_{\text{CH}_4,i}(\text{cm}^{-3})v_i(\text{cm s}^{-1})} \quad (3)$$

where  $n_{\text{CH}_4,f}$  and  $n_{\text{CH}_4,i}$  are the densities of CH<sub>4</sub> at the end and the beginning of the simulation, respectively, and  $v_f$  and  $v_i$  are the corresponding velocities.

- The selectivities of the different hydrocarbons are calculated as

$$S_{\text{C}_x\text{H}_y}(\%) = 100\% \frac{x n_{\text{C}_x\text{H}_y}(\text{cm}^{-3})v_f(\text{cm s}^{-1})}{n_{\text{CH}_4,i}(\text{cm}^{-3})v_i(\text{cm s}^{-1}) - n_{\text{CH}_4,f}(\text{cm}^{-3})v_f(\text{cm s}^{-1})} \quad (4)$$

with  $n_{\text{C}_x\text{H}_y}$  the density of the hydrocarbon. Note that these selectivities are C-based. We also define the H<sub>2</sub> selectivity, which is H-based:

$$S_{\text{H}_2}(\%) = 100\% \frac{0.5 n_{\text{H}_2}(\text{cm}^{-3})v_f(\text{cm s}^{-1})}{n_{\text{CH}_4,i}(\text{cm}^{-3})v_i(\text{cm s}^{-1}) - n_{\text{CH}_4,f}(\text{cm}^{-3})v_f(\text{cm s}^{-1})} \quad (5)$$

- The specific energy input SEI deposited on the initial CH<sub>4</sub> flow is calculated as

$$\text{SEI}(\text{kJL}^{-1}) = \frac{P(\text{W})60(\text{s min}^{-1})}{\Phi(\text{sccm})} \quad (6)$$

$P$  is the deposited power in the plasma and  $\Phi$  the flow rate. This SEI value can be converted into eV molec<sup>-1</sup> as follows:<sup>6</sup>

$$\text{SEI}(\text{eV molec}^{-1}) = \frac{\text{SEI}(\text{kJ L}^{-1})6.24 \times 10^{21}(\text{eV kJ}^{-1})24.5(\text{L mol}^{-1})p_0(101325 \text{ Pa})}{6.022 \times 10^{23}(\text{molec mol}^{-1})p(\text{Pa})} \quad (7)$$

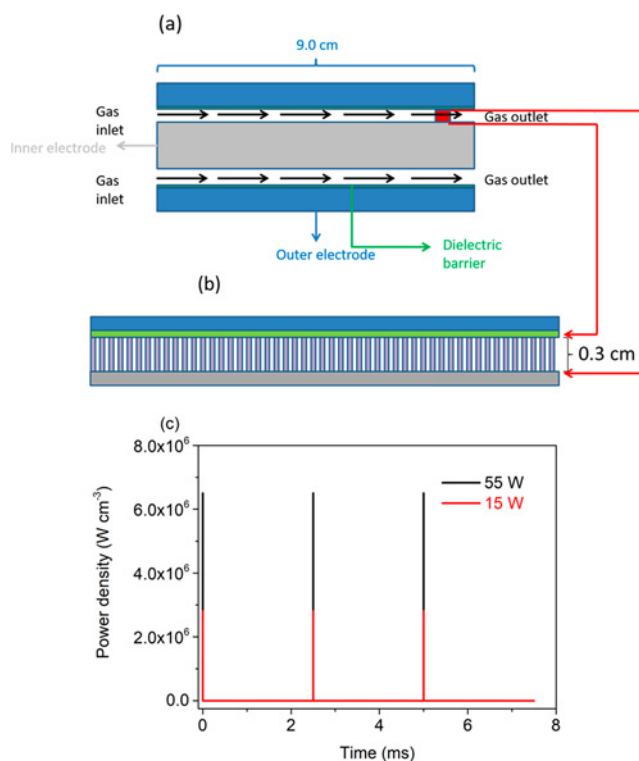
with  $p_0$  and  $p$  the atmospheric pressure and pressure inside the reactor, respectively. This allows us to calculate the energy cost for CH<sub>4</sub> conversion (either in kJ L<sup>-1</sup> or eV molec<sup>-1</sup>, depending on the unit of SEI):

$$\text{EC} = \frac{\text{SEI} \times 100\%}{\chi_{\text{CH}_4}(\%)\phi} \quad (8)$$

where  $\phi$  is the fraction of CH<sub>4</sub> present in the feed gas.

**2.2.2. Dielectric Barrier Discharge (DBD).** As mentioned in the Introduction, a DBD is created by applying an electric potential difference between two electrodes, of which at least

one is covered by a dielectric barrier. A DBD in CH<sub>4</sub> exhibits filamentary behavior, i.e., microdischarges between these electrodes. Hence, the CH<sub>4</sub> molecules will pass through several microdischarge filaments on their way throughout the reactor, which we mimic in the model as microdischarge power pulses as a function of time (cf. previous section). We applied our model to the DBD reactor of Xu and Tu<sup>10</sup> and to the micro-DBD reactor of Wang et al.,<sup>32</sup> in order to first verify our modeling results with their experiments, as a validation of our model. Indeed, these results are a good representation of other DBD reactor studies on CH<sub>4</sub> conversion, as reviewed by Scapinello et al.<sup>5</sup> Figure 1 illustrates a schematic picture of the cylindrical



**Figure 1.** Schematic illustration of a typical cylindrical DBD reactor, based on the design of Xu and Tu<sup>10</sup> (a), representation of the filaments in this reactor (b), and the corresponding power density profile as a function of time in this DBD reactor, for three pulses, at an input power of 15 and 55 W and a frequency of the applied power of 20 kHz (c).

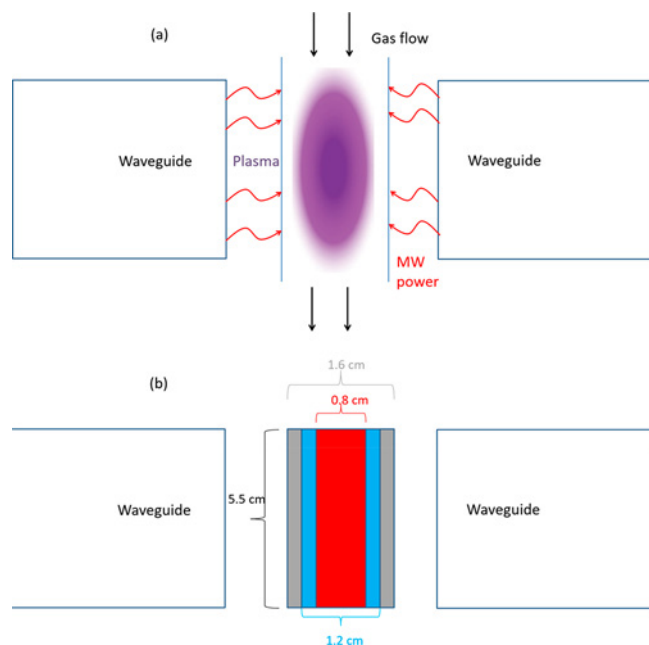
DBD reactor of Xu and Tu,<sup>10</sup> which has a length of 9 cm and a discharge gap of 0.3 cm, resulting in a discharge volume of 13.6 cm<sup>3</sup>.<sup>10</sup> The micro-DBD reactor of Wang et al.<sup>32</sup> looks similar, but with a discharge gap of 0.09 cm, a length of 20 cm, and a discharge volume of 1.4 cm<sup>3</sup>.

We assume that the plasma power is uniformly deposited in pulses (or microdischarges) with lifetimes of 11 ns for 15 W and 14 ns for 55 W, based on linear interpolation of the microdischarge lifetime as a function of power, adopted from Ozkan et al.<sup>33,34</sup> During one AC period in a DBD reactor, these authors measured approximately 400 microdischarges at 50 W and 500 microdischarges at 100 W, with an almost linear increase of the number of discharges as a function of power.<sup>33</sup> The local power deposition per pulse  $P_{\text{pulse}}$  (in W) is defined as

$$P_{\text{pulse}} = \frac{P_{\text{total}}}{N_{\text{pulse}}f_{\text{AC}}t_{\text{pulse}}} \quad (9)$$

where  $P_{\text{total}}$  (in W) is the global power input, which is varied between 15 and 55 W, based on the experiments of Xu and Tu,<sup>10</sup> and between 10 and 30 W for the experiments of Wang et al.,<sup>32</sup>  $N_{\text{pulse}}$  is the number of pulses per AC cycle,  $f_{\text{AC}}$  (in Hz) the frequency of the applied power, which is 20 kHz in our simulations, again based on Xu and Tu<sup>10</sup> and Wang et al.,<sup>32</sup> and  $t_{\text{pulse}}$  (in s) is the lifetime of the microdischarges (see above). Each of these microdischarges can be represented as a cylinder with a typical radius of  $\sim 0.13$  mm<sup>35,36</sup> and a length equal to the discharge gap. Following Snoeckx et al.,<sup>27,37</sup> we assume that every molecule passes such a microdischarge every 100 half cycles, irrespective of power deposited. Detailed information on how the microdischarges are treated in the model, including the number of pulses per AC cycle and the temperature, is given in the SI.

**2.2.3. Microwave (MW) Plasma.** According to Scapinello et al.,<sup>5</sup> the majority of results for  $\text{CH}_4$  conversion in MW plasmas were obtained by Heintze and Magureanu<sup>12</sup> at reduced pressure, and by Shen et al.<sup>14</sup> at atmospheric pressure. Both reactors are so-called surface wave MW plasmas, where microwave power is applied from the side, through a waveguide, to a cylindrical tube through which the gas flows (see schematic diagram in Figure 2).

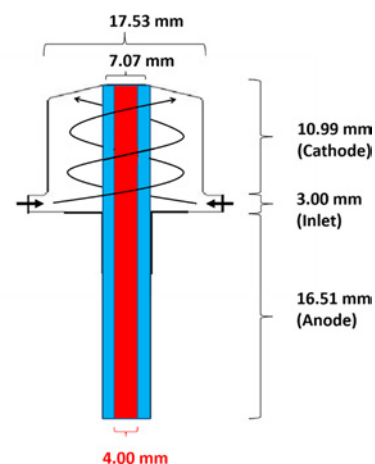


**Figure 2.** Schematic illustration of the atmospheric pressure MW plasma, based on the design of Shen et al.<sup>14</sup> (a) and its implementation in the 0D model (b). The arrows depict the direction of the gas flow and the different colors in (b) indicate the hot center (red) and cooler (blue and gray) zones (see text in SI).

Hence, we applied our model to the wide range of conditions in both studies, to validate our model. Details of both reactor configurations and discharge conditions, and the assumptions made in our model on power deposition and corresponding temperature in the plasma, are given in SI.

**2.2.4. Gliding Arc (GA) Plasma.** The results on GA performance, as reviewed by Scapinello et al.,<sup>5</sup> are quite scattered. A classical GA is formed between two flat converging electrodes, between which an electric potential difference is applied, creating an arc discharge, that glides along the electrodes under influence of the gas flow, toward rising interelectrode distance, until it extinguishes and a new arc is

formed at the shortest interelectrode distance.<sup>38</sup> However, the residence time of the gas inside the arc plasma is quite limited in classical GA discharges. For this reason, a cylindrical GA discharge, also called gliding arc plasmatron (GAP), was developed by Nunnally et al.,<sup>39,40</sup> and showed promising results for  $\text{CO}_2$  splitting<sup>39–42</sup> and dry reforming of  $\text{CH}_4$ .<sup>28</sup> Therefore, we performed experiments in this GAP for pure  $\text{CH}_4$  conversion to validate our model. A schematic picture of this GAP configuration is given in Figure 3.



**Figure 3.** Schematic illustration of the GAP, with characteristic dimensions of cathode (reactor body), inlet region (insulator), anode (outlet) and arc region, and indication of the outer vortex (solid spiral). The inner (reverse) vortex is not depicted for the sake of clarity, but it is confined in the red and blue rectangles. The red rectangle shows the arc region, and the blue region is the hot region right next to it, inside the inner vortex.

It consists of a cylindrical reactor body (at cathode potential) and a reactor outlet (at anode potential). The gas flows in through six tangential inlets, creating a vortex flow. When the anode (= outlet) diameter is smaller than the cathode (= reactor body) diameter, the incoming gas will not immediately escape the reactor through the outlet at the bottom of the reactor, as it follows a vortex flow with larger diameter, so it will be forced upward in the cathodic part of the reactor, in a so-called forward vortex flow (FVF) pattern. When the spiraling gas arrives at the top of the reactor, the rotational speed will be reduced due to friction and inertia, and it will start to move downward in a smaller vortex, toward the outlet at the bottom, i.e., in a reverse vortex flow (RVF). The latter stabilizes the arc in the center of the reactor and it minimizes heat losses toward the walls. In this way, the residence time inside the arc is longer than in classical GA discharges, with a larger plasma volume. Therefore, the performance in terms of gas conversion is generally better than in classical GA discharges.

The arc plasma in a GAP is confined within the inner vortex and is more or less uniform, allowing a straightforward description of this GA configuration with our 0D model. Moreover, the arc dimensions change little with electric current, as investigated by Trenchev et al.<sup>43,44</sup> We assume that the arc has a diameter of 4 mm, as in our earlier simulations.<sup>28,41,42,45</sup> This corresponds to an arc volume of  $383 \text{ mm}^3$ . Right next to the arc, there is still a warm zone until the edge of the inner vortex, where the temperature is still above 1000 K, and thus where thermal  $\text{CH}_4$  conversion can still take place.<sup>28</sup>

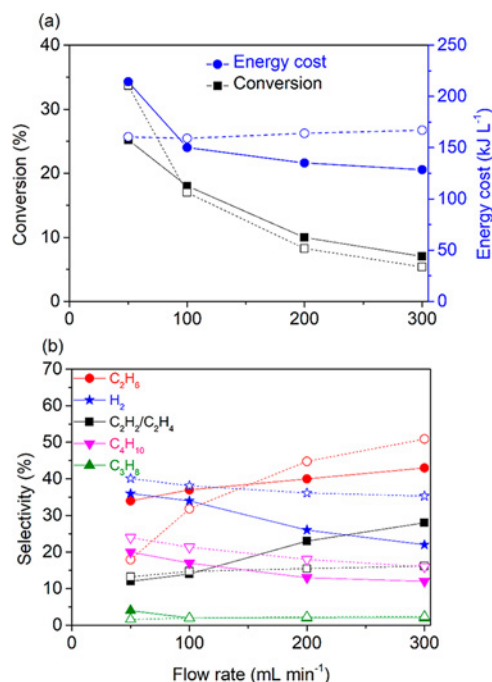
In both the experiments and simulations, we did not use pure  $\text{CH}_4$ , as the latter did not allow plasma ignition in our GAP reactor. Therefore, we added between 80% and 50%  $\text{N}_2$ , and consequently, we expanded the chemistry in our model with  $\text{N}_2$  and  $\text{CH}_4\text{-N}_2$  chemistry, as explained in the SI. The power deposited inside the plasma was 224 W and the flow rate was  $10 \text{ L min}^{-1}$ . Based on earlier 3D fluid dynamics calculations by Trenchev et al.,<sup>44</sup> this corresponds to a velocity of  $196 \text{ cm s}^{-1}$  and a residence time of 15 ms. The SEI value is  $1.3 \text{ kJ L}^{-1}$ .

### 3. RESULTS AND DISCUSSION

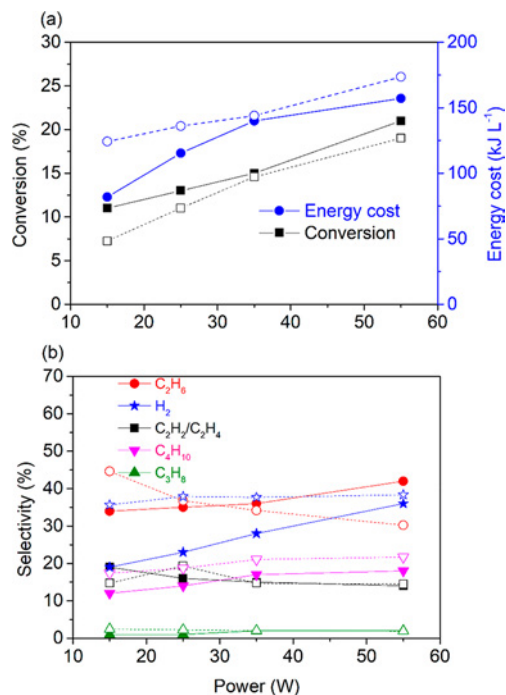
In the following sections, we will always first compare the calculated  $\text{CH}_4$  conversion and energy cost with experimental data, as well as the selectivities of the most important hydrocarbons (and  $\text{H}_2$  when available), for a wide range of conditions, to verify whether the model predicts the right chemistry in each of the plasma sources. Subsequently, we can use the model to elucidate the underlying reaction pathways for  $\text{CH}_4$  conversion into higher hydrocarbons and  $\text{H}_2$ , in DBD, MW, and GA plasmas. It should be noted that only C atom formation, but no solid carbon formation is included in our model, because we only describe the gas phase chemistry. Furthermore, it was stated in the experimental papers to be always below 10% in the DBD and MW plasma at atmospheric pressure,<sup>10,14,32</sup> while in the MW plasma at reduced pressure, it was also stated to be negligible in the pulsed mode.<sup>12</sup> In the MW plasma at reduced pressure in continuous mode and in our own GAP experiments, however, significant solid carbon formation was observed, so in the future, we should improve our model to account for it, by adding surface processes.

**3.1. DBD Plasma. 3.1.1. Comparison of Calculated and Measured  $\text{CH}_4$  Conversion, Energy Cost, and Product Selectivities.** The calculated and experimental results for  $\text{CH}_4$  conversion, energy cost, and selectivities of the most important hydrocarbons and  $\text{H}_2$  in the DBD reactor of Xu and Tu<sup>10</sup> are plotted as a function of flow rate and plasma power in Figures 4 and 5, respectively. The experimental and calculated data follow (more or less) the same trend with increasing flow rate. The largest discrepancies are seen for the selectivities of  $\text{C}_2\text{H}_6$  and  $\text{C}_2\text{H}_2/\text{C}_2\text{H}_4$ , with maximum relative discrepancies of 62% for  $\text{C}_2\text{H}_6$  at  $50 \text{ mL min}^{-1}$  and 53% for  $\text{C}_2\text{H}_4/\text{C}_2\text{H}_2$  at  $300 \text{ mL min}^{-1}$  (see Figure 4). Also the trends as a function of plasma power are in reasonable agreement, except for the  $\text{C}_2\text{H}_6$  selectivity, which decreases in our model, whereas the experiments indicate a small rise. The largest discrepancy for the  $\text{C}_2\text{H}_6$  selectivity is however still only 31% (see Figure 5). The average discrepancy between the calculated and experimental results is 25%, which is satisfactory, in view of the complex chemistry and the assumptions made in the 0D model. Hence, we believe the model is able to elucidate the most important mechanisms in this DBD discharge.

The calculated and experimental conversions, energy costs and product selectivities for the DBD reactor of Wang et al.<sup>32</sup> are plotted in Figures 6 and 7, as a function of flow rate and plasma power, respectively. The  $\text{H}_2$  selectivity was not measured as a function of flow rate, and therefore, only the calculated  $\text{H}_2$  selectivities are shown in Figure 6. Again, the conversion, energy cost, and selectivities generally follow the same trends. Note that the energy cost is rather constant in the model, while the experimental values slightly drop as a function of flow rate (see Figure 6), but this is because the measured conversion drops more slowly than the calculated values at rising flow rate (and thus lower SEI). Indeed, when the flow rate rises by a factor 3

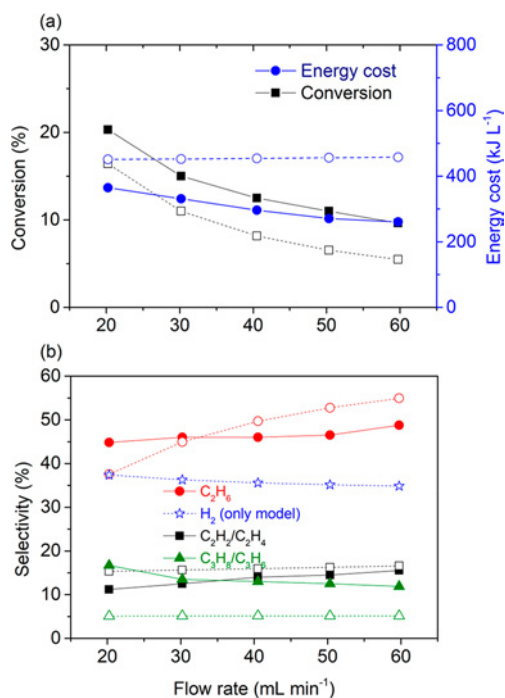


**Figure 4.** Calculated (dashed lines) and experimental (solid lines)  $\text{CH}_4$  conversions and energy costs (a), as well as selectivities of the most important hydrocarbons and  $\text{H}_2$  formed (b), as a function of flow rate, at a plasma power of 45 W in an atmospheric pressure DBD reactor. The experimental results are adopted from Xu and Tu.<sup>10</sup>

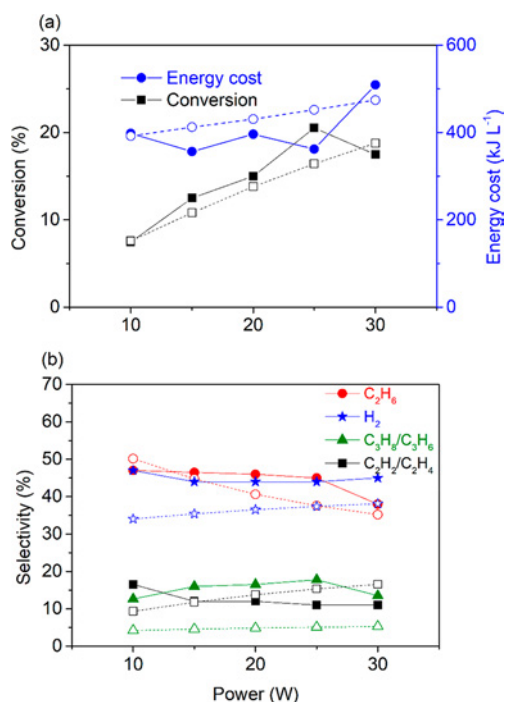


**Figure 5.** Calculated (dashed lines) and experimental (solid lines)  $\text{CH}_4$  conversions and energy costs (a), as well as selectivities of the most important hydrocarbons and  $\text{H}_2$  formed (b), as a function of plasma power, at a flow rate of  $100 \text{ mL min}^{-1}$  in an atmospheric pressure DBD reactor. The experimental results are adopted from Xu and Tu.<sup>10</sup>

(and thus, the SEI drops by a factor 3, at constant power), the calculated conversion drops by a factor 3 as well (thus explaining the constant energy cost), while the measured conversion only drops by a factor 2 (thus explaining why the energy cost slightly



**Figure 6.** Calculated (dashed lines) and experimental (solid lines) CH<sub>4</sub> conversions and energy costs (a), as well as selectivities of the most important hydrocarbons and H<sub>2</sub> formed (b), as a function of flow rate, at a plasma power of 25 W in an atmospheric pressure DBD reactor. The experimental results are adopted from Wang et al.<sup>32</sup>



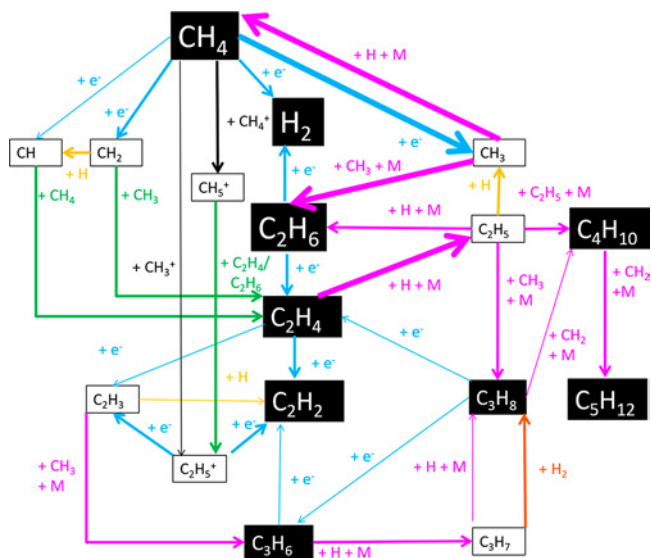
**Figure 7.** Calculated (dashed lines) and experimental (solid lines) CH<sub>4</sub> conversions and energy costs (a), as well as selectivities of the most important hydrocarbons and H<sub>2</sub> formed (b), as a function of plasma power, at a flow rate of 20.24 mL min<sup>-1</sup> in an atmospheric pressure DBD reactor. The experimental results are adopted from Wang et al.<sup>32</sup>

drops). In addition, also the C<sub>2</sub>H<sub>2</sub>/C<sub>2</sub>H<sub>4</sub> selectivities show some discrepancy, because the experimental data slightly drop and the calculation results slightly rise upon increasing plasma power

(see Figure 7). However, the maximum relative difference is about 50%, which is still reasonable, in view of the assumptions made in the OD model. Also the absolute values of the calculated and experimental results are in satisfactory agreement, except for the C<sub>3</sub>H<sub>8</sub>/C<sub>3</sub>H<sub>6</sub> selectivities, which exhibit a maximum discrepancy of 72% at a plasma power of 15 W and a flow rate of 20.2 mL min<sup>-1</sup> (see Figure 7). The average discrepancy between the calculated and experimental results is 37%, which we believe is good enough for explaining the underlying chemistry in a DBD reactor.

In both reactors, the conversions vary between 7% and 21%, decreasing with rising flow rate and increasing with power. Based on the conditions used, this corresponds to energy costs varying between 82 kJ L<sup>-1</sup> (or 19 eV molec<sup>-1</sup>) at a plasma power of 15 W and a flow rate of 100 mL min<sup>-1</sup> (i.e., SEI = 9 kJ L<sup>-1</sup>, for the conditions of Xu and Tu;<sup>10</sup> Figure 5), up to 509 kJ L<sup>-1</sup> (or 118 eV molec<sup>-1</sup>) at a plasma power of 30 W and a flow rate of 20.2 mL min<sup>-1</sup> (i.e., SEI = 89 kJ L<sup>-1</sup>, for the conditions of Wang et al.;<sup>32</sup> see Figure 7). The average energy cost for CH<sub>4</sub> conversion for all conditions studied is 259 kJ L<sup>-1</sup> (or 60 eV molec<sup>-1</sup>), which is very high. Both in the model and experiments, C<sub>2</sub>H<sub>6</sub> is by far the most important hydrocarbon, followed by C<sub>2</sub>H<sub>2</sub> and C<sub>2</sub>H<sub>4</sub>, C<sub>4</sub>H<sub>10</sub>, and finally C<sub>3</sub>H<sub>8</sub>. Other (unsaturated or higher) hydrocarbons were not reported in both papers, but according to our model, C<sub>5</sub>H<sub>12</sub> can also be formed, and further polymerization toward C<sub>6</sub> and higher hydrocarbons is also possible. In addition, H<sub>2</sub> is formed in large amounts, both in the experiments and our model.

**3.1.2. Underlying Reaction Pathways.** The most important reactions in the DBD plasma are visualized in Figure 8. The thickness of the arrow lines is a measure for the importance of the reactions, determined by the reaction rates, as calculated in the model. These calculated rates are listed in the SI (Table S.6).



**Figure 8.** Most important net reaction pathways in a DBD at atmospheric pressure. Blue, pink, yellow, green, and orange arrow lines represent electron impact reactions, three-body reactions, two-body reactions with H atoms, reactions with hydrocarbon molecules or radicals, and two-body reactions with H<sub>2</sub>, respectively. The thickness of the arrow lines is proportional to the reaction rate, while the size of the boxes is proportional to the species density, as calculated in the model. The black boxes represent stable molecules and the white boxes intermediates (radicals or ions).

CH<sub>4</sub> is mainly converted by electron impact dissociation into CH<sub>3</sub> radicals ( $e^- + \text{CH}_4 \rightarrow e^- + \text{CH}_3 + \text{H}$ ), as well as into CH<sub>2</sub> and CH radicals ( $e^- + \text{CH}_4 \rightarrow e^- + \text{CH}_2 + \text{H}_2$  and  $e^- + \text{CH}_4 \rightarrow e^- + \text{CH} + \text{H} + \text{H}_2$ ). The dissociation into CH<sub>2</sub> and H<sub>2</sub> ( $e^- + \text{CH}_4 \rightarrow e^- + \text{CH}_2 + \text{H}_2$ ) is one of the most important H<sub>2</sub> formation processes (together with  $e^- + \text{C}_2\text{H}_6 \rightarrow e^- + \text{C}_2\text{H}_4 + \text{H}_2$ ; see below).

In addition, CH<sub>4</sub> undergoes electron impact ionization and dissociative ionization ( $e^- + \text{CH}_4 \rightarrow e^- + e^- + \text{CH}_4^+$  and  $e^- + \text{CH}_4 \rightarrow e^- + e^- + \text{CH}_3^+ + \text{H}$ ). The CH<sub>4</sub><sup>+</sup> and CH<sub>3</sub><sup>+</sup> ions formed in this way are not indicated as separate species in Figure 8, as they quickly react with CH<sub>4</sub>, forming C<sub>2</sub>H<sub>5</sub><sup>+</sup> ( $\text{CH}_3^+ + \text{CH}_4 \rightarrow \text{C}_2\text{H}_5^+ + \text{H}_2$ ) or CH<sub>5</sub><sup>+</sup> ( $\text{CH}_4^+ + \text{CH}_4 \rightarrow \text{CH}_5^+ + \text{CH}_3$ ).

The CH<sub>3</sub> radicals partially recombine with H ( $\text{CH}_3 + \text{H} + \text{M} \rightarrow \text{CH}_4 + \text{M}$ ) forming again CH<sub>4</sub>, but they also recombine with another CH<sub>3</sub> radical ( $\text{CH}_3 + \text{CH}_3 + \text{M} \rightarrow \text{C}_2\text{H}_6 + \text{M}$ ) to form C<sub>2</sub>H<sub>6</sub>, which is the most important production mechanism of C<sub>2</sub>H<sub>6</sub>, and it occurs mainly in the microdischarge pulses of the DBD, where the CH<sub>3</sub> radicals as necessary building blocks are formed.

C<sub>2</sub>H<sub>6</sub> is partially converted into C<sub>2</sub>H<sub>4</sub> by electron impact dissociation ( $e^- + \text{C}_2\text{H}_6 \rightarrow e^- + \text{C}_2\text{H}_4 + \text{H}_2$ ), which is the main population mechanism of C<sub>2</sub>H<sub>4</sub> and one of the main population mechanisms of H<sub>2</sub> (cf. above). In addition, C<sub>2</sub>H<sub>4</sub> is also formed upon (radical) recombination reactions ( $\text{CH}_3 + \text{CH}_2 \rightarrow \text{C}_2\text{H}_4 + \text{H}$  and  $\text{CH}_4 + \text{CH} \rightarrow \text{C}_2\text{H}_4 + \text{H}$ ).

C<sub>2</sub>H<sub>4</sub> partially recombines with H into C<sub>2</sub>H<sub>5</sub> ( $\text{C}_2\text{H}_4 + \text{H} + \text{M} \rightarrow \text{C}_2\text{H}_5 + \text{M}$ ), and C<sub>2</sub>H<sub>5</sub> recombines further with C<sub>2</sub>H<sub>5</sub> into C<sub>4</sub>H<sub>10</sub> ( $\text{C}_2\text{H}_5 + \text{C}_2\text{H}_5 + \text{M} \rightarrow \text{C}_4\text{H}_{10} + \text{M}$ ), as well as with H ( $\text{C}_2\text{H}_5 + \text{H} \rightarrow \text{CH}_3 + \text{CH}_3$ ) forming again two CH<sub>3</sub> radicals, and with CH<sub>3</sub> ( $\text{CH}_3 + \text{C}_2\text{H}_5 + \text{M} \rightarrow \text{C}_3\text{H}_8 + \text{M}$ ) forming C<sub>3</sub>H<sub>8</sub>. The latter reaction is however less important than the other two reactions, explaining why C<sub>4</sub>H<sub>10</sub> was formed in larger amounts than C<sub>3</sub>H<sub>6</sub>/C<sub>3</sub>H<sub>8</sub> in the experiments of Xu and Tu<sup>10</sup> (see Figures 4 and 5). Moreover, C<sub>2</sub>H<sub>4</sub> also undergoes electron impact dissociation ( $e^- + \text{C}_2\text{H}_4 \rightarrow e^- + \text{C}_2\text{H}_2 + \text{H}_2$  and  $e^- + \text{C}_2\text{H}_4 \rightarrow e^- + \text{C}_2\text{H}_3 + \text{H}$ ).

In addition, C<sub>2</sub>H<sub>4</sub> and C<sub>2</sub>H<sub>6</sub> react with CH<sub>5</sub><sup>+</sup> ions, forming C<sub>2</sub>H<sub>5</sub><sup>+</sup> ( $\text{CH}_5^+ + \text{C}_2\text{H}_6 \rightarrow \text{C}_2\text{H}_5^+ + \text{H}_2 + \text{CH}_4$  and  $\text{CH}_5^+ + \text{C}_2\text{H}_4 \rightarrow \text{C}_2\text{H}_5^+ + \text{CH}_4$ ). C<sub>2</sub>H<sub>5</sub><sup>+</sup> is an important intermediate for the formation of C<sub>2</sub>H<sub>2</sub> and C<sub>2</sub>H<sub>3</sub>, by dissociative recombination with electrons ( $e^- + \text{C}_2\text{H}_5^+ \rightarrow \text{C}_2\text{H}_3 + \text{H} + \text{H}$ ,  $e^- + \text{C}_2\text{H}_5^+ \rightarrow \text{C}_2\text{H}_2 + \text{H}_2 + \text{H}$ , and  $e^- + \text{C}_2\text{H}_5^+ \rightarrow \text{C}_2\text{H}_2 + \text{H} + \text{H} + \text{H}$ ). The C<sub>2</sub>H<sub>3</sub> radicals mainly recombine with CH<sub>3</sub> radicals into C<sub>3</sub>H<sub>6</sub> ( $\text{CH}_3 + \text{C}_2\text{H}_3 + \text{M} \rightarrow \text{C}_3\text{H}_6 + \text{M}$ ), as well as with H ( $\text{C}_2\text{H}_3 + \text{H} \rightarrow \text{C}_2\text{H}_2 + \text{H}_2$ ) forming C<sub>2</sub>H<sub>2</sub>.

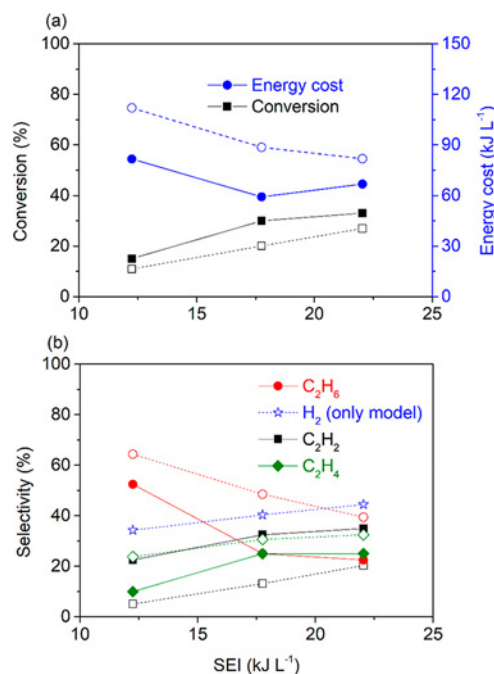
C<sub>3</sub>H<sub>6</sub> undergoes electron impact dissociation into C<sub>2</sub>H<sub>2</sub> ( $e^- + \text{C}_3\text{H}_6 \rightarrow e^- + \text{C}_2\text{H}_2 + \text{CH}_4$ ), but it mainly recombines with H, forming C<sub>3</sub>H<sub>7</sub> ( $\text{C}_3\text{H}_6 + \text{H} + \text{M} \rightarrow \text{C}_3\text{H}_7 + \text{M}$ ). The latter radical quickly forms C<sub>3</sub>H<sub>8</sub> upon reaction with H<sub>2</sub> ( $\text{C}_3\text{H}_7 + \text{H}_2 \rightarrow \text{C}_3\text{H}_8 + \text{H}$ ), as well as by three-body recombination with H ( $\text{C}_3\text{H}_7 + \text{H} + \text{M} \rightarrow \text{C}_3\text{H}_8 + \text{M}$ ).

C<sub>3</sub>H<sub>8</sub> partially creates again C<sub>3</sub>H<sub>6</sub> by electron impact dissociation ( $e^- + \text{C}_3\text{H}_8 \rightarrow e^- + \text{C}_3\text{H}_6 + \text{H}_2$ ) or it recombines with CH<sub>2</sub> into C<sub>4</sub>H<sub>10</sub> ( $\text{C}_3\text{H}_8 + \text{CH}_2 + \text{M} \rightarrow \text{C}_4\text{H}_{10} + \text{M}$ ). Finally, C<sub>4</sub>H<sub>10</sub> recombines with CH<sub>2</sub> radicals into C<sub>5</sub>H<sub>12</sub> ( $\text{C}_4\text{H}_{10} + \text{CH}_2 + \text{M} \rightarrow \text{C}_5\text{H}_{12} + \text{M}$ ), which will further react into the formation of higher hydrocarbons by the same type of recombination reaction.

Hence it is clear that in a DBD electron impact dissociation processes are predominant. They create radicals, which mainly recombine with other radicals or H atoms, due to the lower

temperatures, forming especially the saturated hydrocarbons, such as C<sub>2</sub>H<sub>6</sub>, C<sub>3</sub>H<sub>8</sub>, and C<sub>4</sub>H<sub>10</sub>.

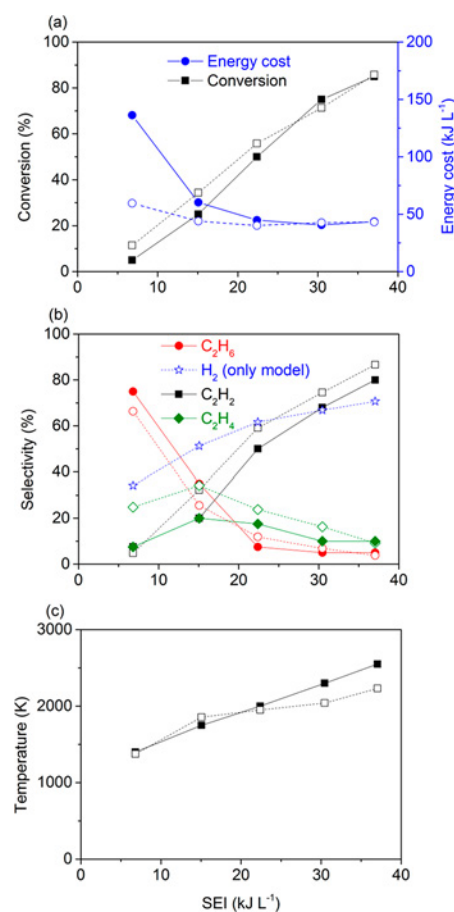
**3.2. MW Plasma. 3.2.1. Comparison of Calculated and Measured CH<sub>4</sub> Conversion, Energy Cost, and Product Selectivities.** The experimental and calculated CH<sub>4</sub> conversions, energy costs, and selectivities of the most important hydrocarbons are plotted as a function of SEI in Figures 9 and 10, for a



**Figure 9.** Calculated (dashed lines) and experimental (solid lines) CH<sub>4</sub> conversions and energy costs (a), as well as selectivities of the most important hydrocarbons and H<sub>2</sub> formed (b), as a function of SEI, in a MW plasma at a pressure of 30 mbar and flow rate of 98 sccm, operating in a continuous regime. The experimental results are adopted from Heintze and Magureanu.<sup>12</sup>

MW discharge at reduced pressure, i.e., 30 mbar, for a continuous and a pulsed discharge, respectively. Again, no H<sub>2</sub> selectivities were reported in the experiments, so only the calculated values are given. In the pulsed regime, we also compare the calculated and measured gas temperature in Figure 10. Figures 11 and 12 show the experimental and calculated CH<sub>4</sub> conversions, energy costs, and most important product selectivities in a MW discharge at atmospheric pressure, as a function of power and flow rate, respectively. Note that these experiments were performed in a CH<sub>4</sub>/H<sub>2</sub> mixture, so the H<sub>2</sub> selectivities could not be determined, since H<sub>2</sub> is also a reactant.

In general, the difference between the calculated and experimental results is higher for lower powers and reduced pressure than for higher pressures and higher powers. The C<sub>2</sub>H<sub>2</sub> selectivities in the reduced pressure MW plasma in continuous mode show the largest discrepancies, even up to almost a factor of 5 (i.e., calculated C<sub>2</sub>H<sub>2</sub> selectivity of 5% versus 23%, for an SEI value of 12 kJ L<sup>-1</sup>). The reason is probably the underestimation of the gas temperature and the assumption that the power is evenly distributed over the whole radial distance of the reactor tube. In the atmospheric pressure MW plasma the largest discrepancies are found for the C<sub>2</sub>H<sub>4</sub> selectivities, i.e., up to a factor of 6 (calculated C<sub>2</sub>H<sub>4</sub> selectivity of 3% versus 18%, at 400 W and 500 mL min<sup>-1</sup>; see Figure 11). Nevertheless, in both the reduced pressure and atmospheric pressure MW plasma the

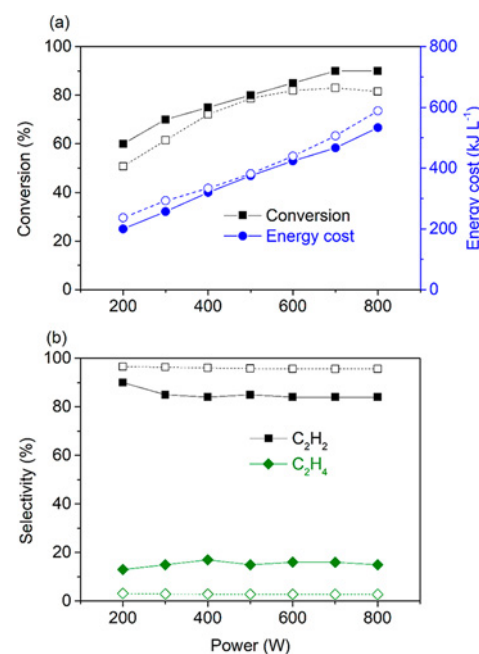


**Figure 10.** Calculated (dashed lines) and experimental (solid lines) CH<sub>4</sub> conversions and energy costs (a), as well as selectivities of the most important hydrocarbons and H<sub>2</sub> (b), and gas temperatures (c), as a function of SEI, in a MW plasma at a pressure of 30 mbar and flow rate of 98 sccm, operating in a pulsed regime. The experimental results are adopted from Heintze and Magureanu.<sup>12</sup>

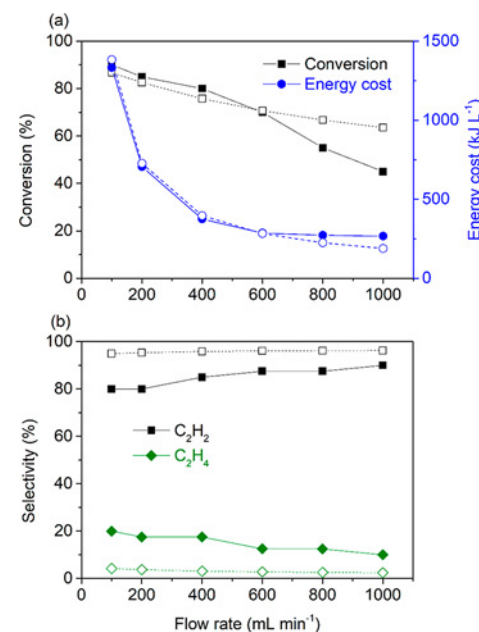
experimental and calculated results show the same trend and on average the discrepancy between calculated and experimental results is 40% for the reduced pressure MW plasma and 44% for the atmospheric pressure plasma. In addition, the difference between calculated and measured gas temperature in the pulsed reduced pressure MW plasma is less than 12%, so we believe that a qualitative description of the reaction mechanisms in MW plasmas operating in different pressure regimes is feasible with our model and will be presented in the next section.

It is clear that the CH<sub>4</sub> conversion in the MW plasma, both at reduced and atmospheric pressure, can reach values above 80%, for high power and low flow rate or high SEI values. The energy costs range from about 50 to above 100 kJ L<sup>-1</sup> at reduced pressure, which is lower than in a DBD. In the atmospheric pressure MW plasma, the energy costs vary from 200 to above 1000 kJ L<sup>-1</sup>, which is of the same order or even higher than in the DBD. However, it should be mentioned that the gas flow in this case was diluted with H<sub>2</sub>, (CH<sub>4</sub>/H<sub>2</sub> ratio of 1/4), which reacts to a large extent with the dissociation products of CH<sub>4</sub>, forming again CH<sub>4</sub>. This means that not all of the power is efficiently used for CH<sub>4</sub> conversion, explaining the higher energy cost.

For lower power and pressure, the main products formed are C<sub>2</sub>H<sub>6</sub> (with selectivities ranging between 5% and 75%), C<sub>2</sub>H<sub>4</sub> (with selectivities ranging from 8% to 20%), and C<sub>2</sub>H<sub>2</sub> (with selectivities ranging from 8% to 80%). Higher hydrocarbons,



**Figure 11.** Calculated (dashed lines) and experimental (solid lines) CH<sub>4</sub> conversions and energy costs (a), as well as selectivities of C<sub>2</sub>H<sub>4</sub> and C<sub>2</sub>H<sub>2</sub> (b), as a function of microwave power, at a flow rate of 500 mL min<sup>-1</sup> in an atmospheric pressure MW plasma, for a CH<sub>4</sub>/H<sub>2</sub> ratio of 1/4. The experimental results are adopted from Shen et al.<sup>14</sup>



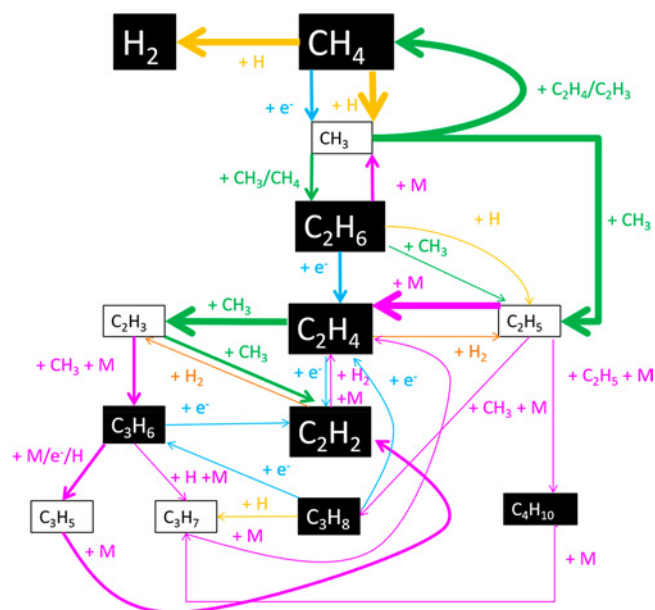
**Figure 12.** Calculated (dashed lines) and experimental (solid lines) CH<sub>4</sub> conversions and energy costs (a), as well as selectivities of C<sub>2</sub>H<sub>4</sub> and C<sub>2</sub>H<sub>2</sub> (b), as a function of flow rate, at a microwave power of 400 W in an atmospheric pressure MW plasma, for a CH<sub>4</sub>/H<sub>2</sub> ratio of 1/4. The experimental results are adopted from Shen et al.<sup>14</sup>

such as created in the DBD, were not observed in our model, and also not reported experimentally. This is attributed to the high temperatures in the MW plasma (above 1000 K), which will cause dissociation of these higher hydrocarbons back in smaller compounds. Furthermore, the higher the SEI value, the larger the shift toward C<sub>2</sub>H<sub>2</sub> and C<sub>2</sub>H<sub>4</sub>, instead of C<sub>2</sub>H<sub>6</sub>. At atmospheric pressure, CH<sub>4</sub> is mainly converted into C<sub>2</sub>H<sub>2</sub>



with a selectivity of  $\sim 85\%$ , and to  $C_2H_4$  with a selectivity of  $\sim 15\%$ . Although different conditions give different product selectivities, especially at reduced pressure, we can draw an overall picture of the most important mechanisms at reduced pressure vs atmospheric pressure, as outlined in next section.

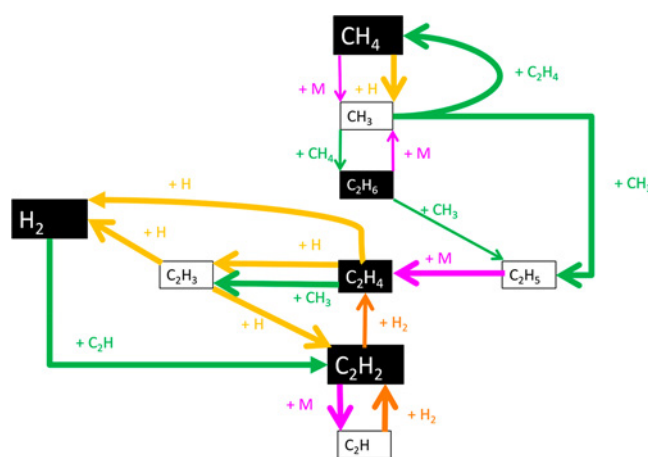
**3.2.2. Underlying Reaction Pathways.** It is clear from above that the different pressure regimes in a MW plasma show different product distributions, which are attributed to different mechanisms, as can be seen in Figures 13 and 14. Again, the



**Figure 13.** Most important net reaction pathways in a MW plasma at reduced pressure. Blue, pink, yellow, green, and orange arrow lines represent electron impact reactions, reactions involving a neutral species M in three-body reactions or neutral dissociation, two-body reactions with H atoms, two-body reactions with hydrocarbon molecules or radicals, and with  $H_2$  molecules, respectively. The thickness of the arrow lines and the size of the boxes are proportional to the reaction rate and species density, respectively, as calculated in the model. The black boxes represent stable molecules and the white boxes intermediates (radicals).

thickness of the arrow lines are a measure for the importance of the reactions, determined by the reaction rates, as calculated in the model. These calculated rates are listed in the SI (Tables S.7 and S.8, for the MW plasma at reduced and atmospheric pressure, respectively).

In a reduced pressure MW plasma,  $CH_4$  is converted into  $CH_3$  by a combination of electron impact dissociation ( $e^- + CH_4 \rightarrow e^- + CH_3 + H$ ) and reaction with H atoms ( $CH_4 + H \rightarrow CH_3 + H_2$ ). The latter reaction is possible due to the higher temperature in the MW plasma, compared to a DBD, and it is also the main population mechanism of  $H_2$ . Some of the  $CH_3$  radicals react back to  $CH_4$  by reactions with  $C_2H_4$  and  $C_2H_3$  ( $CH_3 + C_2H_4 \rightarrow CH_4 + C_2H_3$  and  $CH_3 + C_2H_3 \rightarrow CH_4 + C_2H_2$ ). In addition, the  $CH_3$  radicals react further with either  $CH_3$  ( $CH_3 + CH_3 + M \rightarrow C_2H_6 + M$ , and  $CH_3 + CH_3 \rightarrow C_2H_5 + H$ ) or  $CH_4$  ( $CH_4 + CH_3 \rightarrow C_2H_6 + H$ ), to form both  $C_2H_6$  and  $C_2H_5$ . The latter radicals, due to the higher temperature, dissociate mainly further into  $C_2H_4$  ( $C_2H_5 + M \rightarrow C_2H_4 + H + M$ ). However, a small fraction also recombines with  $CH_3$  into  $C_3H_8$  ( $CH_3 + C_2H_5 + M \rightarrow C_3H_8 + M$ ) or with  $C_2H_5$  into  $C_4H_{10}$  ( $C_2H_5 + C_2H_5 + M \rightarrow C_4H_{10} + M$ ).



**Figure 14.** Most important net reaction pathways in a MW plasma at atmospheric pressure. Pink, yellow, green, and orange arrow lines represent reactions involving dissociation with a neutral species M, two-body reactions with H atoms, two-body reactions with hydrocarbon molecules or radicals, and with  $H_2$  molecules, respectively. The thickness of the arrow lines and the size of the boxes are proportional to the reaction rate and species density, respectively as calculated in the model. The black boxes represent stable molecules and the white boxes intermediates (radicals).

$C_2H_6$  partially dissociates back into  $CH_3$  ( $C_2H_6 + M \rightarrow CH_3 + CH_3 + M$ ), which becomes more important at high SEI values, explaining why high SEI values give lower  $C_2H_6$  selectivities (see Figures 9 and 10). In addition, it also undergoes electron impact dissociation toward  $C_2H_4$  ( $e^- + C_2H_6 \rightarrow e^- + C_2H_4 + H_2$ ), and it reacts with  $CH_3$  or H radicals into  $C_2H_5$  ( $CH_3 + C_2H_6 \rightarrow CH_4 + C_2H_5$  and  $C_2H_6 + H \rightarrow C_2H_5 + H_2$ ).

$C_2H_4$ , which is mainly formed by dissociation of  $C_2H_6$  and  $C_2H_5$ , reacts mostly further with  $CH_3$  radicals into  $C_2H_3$  ( $CH_3 + C_2H_4 \rightarrow CH_4 + C_2H_3$ ), but a small fraction is also subject to electron impact dissociation, creating  $C_2H_2$  ( $e^- + C_2H_4 \rightarrow e^- + C_2H_2 + H_2$ ), or it reacts with  $H_2$ , creating again  $C_2H_5$  ( $C_2H_4 + H_2 \rightarrow C_2H_5 + H$ ).

The  $C_2H_3$  radicals react with  $CH_3$  radicals into either  $C_3H_6$  or  $C_2H_2$ , at almost equal rates ( $CH_3 + C_2H_3 + M \rightarrow C_3H_6 + M$ , and  $CH_3 + C_2H_3 \rightarrow CH_4 + C_2H_2$ ). This is the main formation process of  $C_3H_6$  at high SEI values, while at low SEI values,  $C_3H_6$  is mainly formed by electron impact dissociation of  $C_3H_8$  ( $e^- + C_3H_8 \rightarrow e^- + C_3H_6 + H_2$ ).

At low SEI values,  $C_3H_6$  dissociates mainly into  $C_2H_2$  and  $C_3H_5$  by electron impact dissociation ( $e^- + C_3H_6 \rightarrow e^- + C_2H_2 + CH_4$ , and  $e^- + C_3H_6 \rightarrow e^- + C_3H_5 + H$ ) and it forms  $C_3H_7$  upon recombination with H atoms ( $C_3H_6 + H + M \rightarrow C_3H_7 + M$ ). At high SEI values,  $C_3H_6$  mainly forms  $C_3H_5$  upon reaction with H or any other neutral molecule ( $C_3H_6 + H \rightarrow C_3H_5 + H_2$  and  $C_3H_6 + M \rightarrow C_3H_5 + H + M$ ).  $C_3H_5$  immediately dissociates further into  $C_2H_2$  ( $C_3H_5 + M \rightarrow C_2H_2 + CH_3 + M$ ).

$C_3H_8$  undergoes electron impact dissociation toward  $C_3H_6$ , as mentioned above, but also toward  $C_2H_4$  ( $e^- + C_3H_8 \rightarrow e^- + C_2H_4 + CH_4$ ), and to a smaller extent it reacts with H into  $C_3H_7$  ( $C_3H_8 + H \rightarrow C_3H_7 + H_2$ ).  $C_3H_7$  is formed by dissociation of  $C_3H_8$  and recombination of  $C_3H_6$ , as mentioned above, but it is also (and even predominantly) formed by dissociation of  $C_4H_{10}$  ( $C_4H_{10} + M \rightarrow C_3H_7 + CH_3 + M$ ). Vice versa, it dissociates into  $C_2H_4$  ( $C_3H_7 + M \rightarrow C_2H_4 + CH_3 + M$ ), thus closing the  $C_3$  and  $C_4$  loop back toward the  $C_2$  hydrocarbons, and explaining why the latter are predominantly formed in MW plasmas.

Finally,  $C_2H_2$ , which is the main product at high SEI values, is formed by various electron impact dissociation, neutral dissociation and two-body reactions with several  $C_2$  and  $C_3$  compounds, mainly  $C_2H_4$ ,  $C_2H_3$ ,  $C_3H_6$  and  $C_3H_5$ , while a small portion reacts further with  $H_2$  toward  $C_2H_3$  ( $C_2H_2 + H_2 \rightarrow C_2H_3 + H$ ), which in turn creates again  $C_3$  compounds, as described above, thus closing the whole cycle.

The chemistry in the atmospheric pressure MW plasma is much less complex, as can be seen in Figure 14. This is attributed to the higher temperature (i.e., >3000 K vs ~2000 K at 30 mbar), causing the dehydrogenation processes to be much more prominent. Like in the reduced pressure case,  $CH_4$  is converted into  $CH_3$ , by a combination of electron impact dissociation ( $e^- + CH_4 \rightarrow e^- + CH_3 + H$ ) and reaction with H atoms ( $CH_4 + H \rightarrow CH_3 + H_2$ ). These radicals partially recombine back into  $CH_4$  upon reaction with  $C_2H_4$  ( $CH_3 + C_2H_4 \rightarrow CH_4 + C_2H_3$ ). In addition, they react with  $CH_4$  to produce  $C_2H_6$  ( $CH_4 + CH_3 \rightarrow C_2H_6 + H$ ), which however immediately dissociates back into  $CH_3$  ( $C_2H_6 + M \rightarrow CH_3 + CH_3 + M$ ) or reacts with  $CH_3$  into the formation of  $C_2H_5$  ( $CH_3 + C_2H_6 \rightarrow CH_4 + C_2H_5$ ). Furthermore, two  $CH_3$  radicals also recombine to produce  $C_2H_5$  ( $CH_3 + CH_3 \rightarrow C_2H_5 + H$ ), which immediately dissociates into  $C_2H_4$  ( $C_2H_5 + M \rightarrow C_2H_4 + H + M$ ).

$C_2H_4$  in turn reacts with  $CH_3$  and H atoms, forming  $C_2H_3$  ( $CH_3 + C_2H_4 \rightarrow CH_4 + C_2H_3$  and  $C_2H_4 + H \rightarrow C_2H_3 + H_2$ ), which directly reacts further with H into  $C_2H_2$  ( $C_2H_3 + H \rightarrow C_2H_2 + H_2$ ). Due to the high temperature,  $C_2H_2$  dissociates into  $C_2H$  ( $C_2H_2 + M \rightarrow C_2H + H + M$ ), which returns immediately back into  $C_2H_2$  ( $C_2H + H_2 \rightarrow C_2H_2 + H$ ). Finally, a small portion of  $C_2H_2$  also recombines back with  $H_2$  into the formation of  $C_2H_4$  ( $C_2H_2 + H_2 + M \rightarrow C_2H_4 + M$ ), closing the loop. Although  $H_2$  is a reactant, it is immediately formed again by the dehydrogenation processes, forming ultimately  $C_2H_2$ .

The reaction pathways in Figures 13 and 14 mainly exhibit thermal reactions, with some contribution of electron impact dissociation at reduced pressure (Figure 13). This is of course due to the high temperature, enabling these thermal reactions, in contrast with the DBD, where electron impact dissociation and also ionization were much more predominant (Figure 8). Lower pressures and lower powers furthermore favor recombination processes, resulting in the formation of  $C_3$  compounds. Higher pressures and higher powers induce dehydrogenation reactions, resulting in more unsaturated hydrocarbons, and thus explaining the high  $C_2H_2$  selectivity in Figures 10–12.

In addition, we investigated the role of vibrational-induced dissociation of  $CH_4$  in the MW plasma, as this process is important in the case of  $CO_2$  splitting and  $N_2$  fixation,<sup>46–49</sup> especially in low pressure MW plasmas, where there is a pronounced vibrational–translational nonequilibrium. For this purpose, we calculated the vibrational temperature, from the four vibrational levels included in our model:

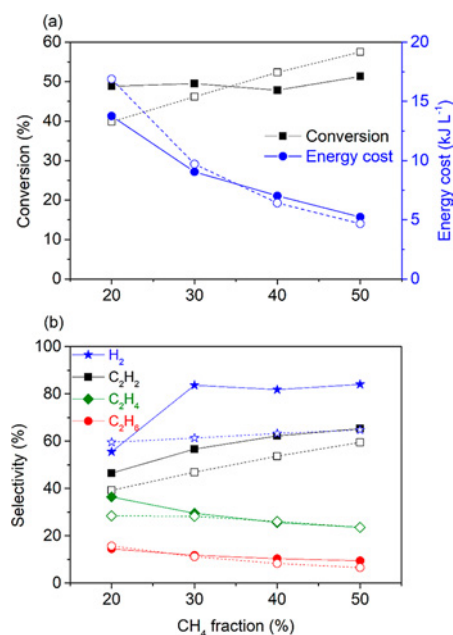
$$T_v = \frac{1}{4} \sum_{i=1}^4 \frac{E_i}{\log\left(\frac{n_i}{g_i n_o}\right)} \quad (10)$$

with  $E_i$  the energy of the first level of vibrational mode  $\nu_i$  of  $CH_4$  (in K),  $g_i$  its degeneracy and  $n_i$  its density (in  $cm^{-3}$ ).  $n_o$  is the density of ground state  $CH_4$ .

We found that, for the MW plasma conditions in this study, the vibrational temperature of  $CH_4$  is almost equal to the gas temperature, indicating that the vibration–translational nonequilibrium in  $CH_4$  MW plasma is negligible, even at reduced

pressure (see Figures S.7 and S.8 in the Supporting Information). This finding is supported by measurements of Butterworth et al.<sup>50</sup>

**3.3. GAP. 3.3.1. Comparison of Calculated and Measured  $CH_4$  Conversion, Energy Costs, and Product Selectivities.** The experimental and calculated  $CH_4$  conversions, energy costs and selectivities of the most important hydrocarbons and  $H_2$  are plotted in Figure 15 as a function of  $CH_4$  fraction in the  $CH_4/N_2$



**Figure 15.** Calculated (dashed lines) and experimental (solid lines)  $CH_4$  conversions and energy costs (a), as well as selectivities of the most important hydrocarbons and  $H_2$  formed (b), in the GAP, as a function of  $CH_4$  fraction in the  $CH_4/N_2$  mixture, for an input power of 224 W and a flow rate of  $10 L min^{-1}$ .

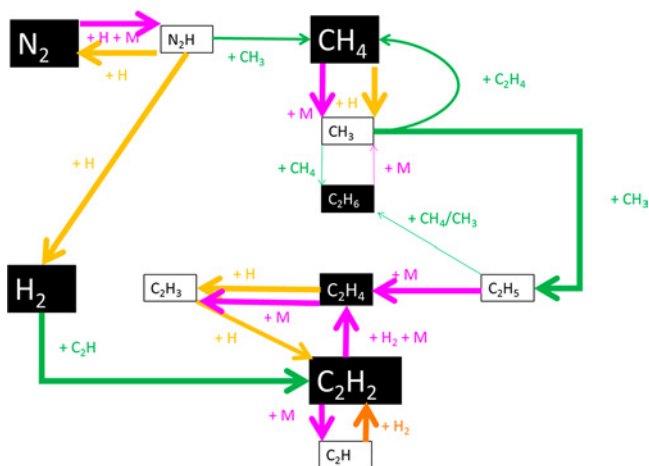
mixture, at a power of 224 W and a flow rate of  $10 L min^{-1}$ . The agreement is very reasonable, with a maximum discrepancy between the experimental and calculated results of 36% for the  $C_2H_6$  selectivity (at a  $CH_4$  fraction of 50%) and an average discrepancy of 15%. In addition, both experimental and calculated results follow the same trends as a function of  $CH_4$  fraction. Therefore, we believe our model can provide a reasonable description of the chemistry inside the GAP, operating in  $CH_4/N_2$  at various mixing ratios.

The conversion is around 50%, and the energy cost is between 5 and  $15 kJ L^{-1}$ , decreasing for higher  $CH_4$  fraction in the mixture. This is significantly lower than the energy costs obtained in the DBD and in the MW plasma, both at reduced and atmospheric pressure. The fact that the energy cost is much lower than in a DBD is not surprising, as this is also the case for other gas conversion processes, such as  $CO_2$  splitting, dry reforming of methane, and  $N_2$  fixation.<sup>6,51</sup> However, the fact that it is also clearly lower than the MW plasma is quite striking, as both plasma sources operate at similar temperature (>3000 K) and power (>200 W). On the other hand, the flow rate in the GAP ( $10 L min^{-1}$ ) is much higher than in the MW plasma ( $100–1000 mL min^{-1}$ ), so the SEI in the GAP is much lower, demonstrating the superior performance in terms of energy cost.

The most important product formed is  $C_2H_2$  (with selectivities ranging between 46% and 65%), followed by

$C_2H_4$  (with selectivities between 24% and 36%) and finally  $C_2H_6$  (with selectivities between 9% and 15%).

3.3.2. *Underlying Reaction Pathways.* The underlying reaction mechanisms in the GAP are presented in Figure 16.



**Figure 16.** Most important net reaction pathways in the GAP at atmospheric pressure. Pink, yellow, green, and orange arrow lines represent reactions involving a neutral species  $M$  in three-body reactions or neutral dissociation, two-body reactions with  $H$  atoms, two-body reactions with hydrocarbon molecules or radicals, and with  $H_2$  molecules, respectively. The thickness of the arrow lines and the size of the boxes are proportional to the reaction rate and species density, respectively, as calculated by the model. The black boxes represent stable molecules and the white boxes intermediates (radicals).

They are similar as in the MW plasma at atmospheric pressure, which is logical, because both plasma types operate at similar temperatures and powers, as mentioned above. The calculated rates of the reactions in this figure are listed in the SI (Table S.9).

Just as in the MW plasma at atmospheric pressure,  $CH_4$  is converted into  $CH_3$  radicals upon both neutral dissociation ( $CH_4 + M \rightarrow CH_3 + H + M$ ) and reaction with  $H$  atoms ( $CH_4 + H \rightarrow CH_3 + H_2$ ). The  $CH_3$  radicals partially react with  $C_2H_4$  to form  $CH_4$  again ( $CH_3 + C_2H_4 \rightarrow CH_4 + C_2H_3$ ) but also with  $N_2H$  ( $CH_3 + N_2H \rightarrow CH_4 + N_2$ ), the latter being formed by  $N_2$  reacting with  $H$  atoms ( $N_2 + H + M \rightarrow N_2H + M$ ). Finally, some  $CH_3$  radicals also form  $C_2H_6$  ( $CH_4 + CH_3 \rightarrow C_2H_6 + H$ ), which however immediately dissociates back into  $CH_3$  ( $C_2H_6 + M \rightarrow CH_3 + CH_3 + M$ ) or reacts with  $CH_3$  into the formation of  $C_2H_5$  ( $CH_3 + C_2H_6 \rightarrow CH_4 + C_2H_5$ ).

The rest of the pathways is identical to the atmospheric MW plasma, with the exception that  $C_2H_5$  partially reacts back to  $C_2H_6$  ( $CH_3 + C_2H_5 \rightarrow C_2H_6 + CH_2$ , and  $CH_4 + C_2H_5 \rightarrow CH_3 + C_2H_6$ ) and  $C_2H_4$  also dissociates in  $C_2H_3$  using neutral dissociation ( $C_2H_4 + M \rightarrow C_2H_3 + H + M$ ) due to the higher temperatures in the GAP, especially in the beginning of the arc discharge near the cathode spot.

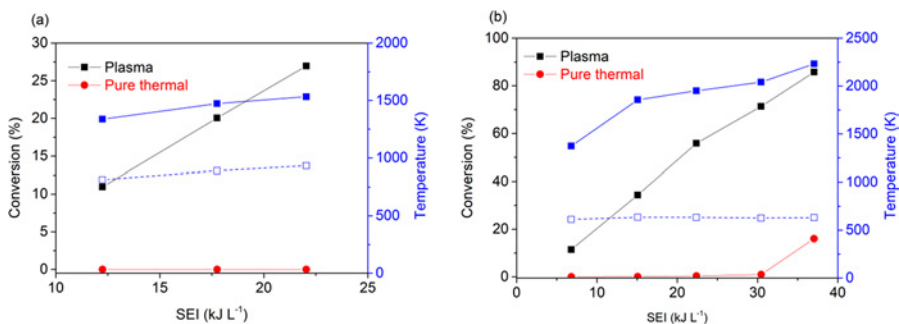
Thus, dehydrogenation and neutral dissociation reactions of the produced hydrocarbons are the most important processes in the GAP, resulting especially in the formation of  $C_2H_2$ .

The fact that the majority of  $CH_4$  dissociates in the GAP, even at the high flow rate of  $10 \text{ L min}^{-1}$  (which is at least a factor 10 higher than in the MW plasma at atmospheric pressure, cf. Figure 12; and even up to 3 orders of magnitude higher than in the DBD; cf. Figures 4–7), point toward the high efficiency of the GAP for  $CH_4$  conversion, compared to the MW and DBD plasmas. This is attributed to the high temperature of the GAP, favoring thermal  $CH_4$  dissociation.

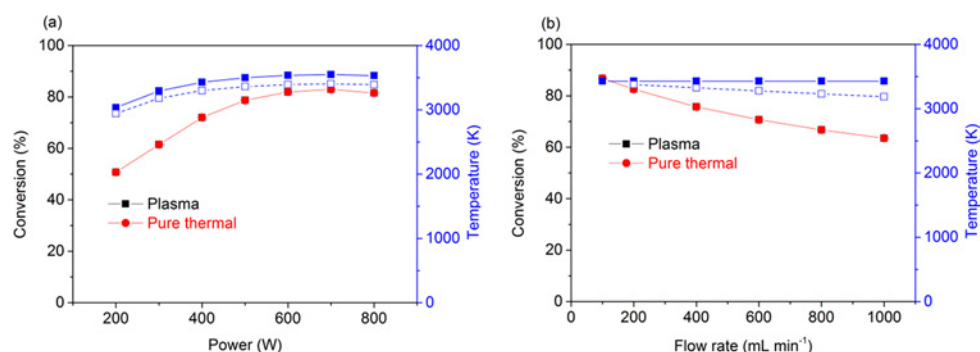
In terms of energy cost, we can conclude that sufficiently high temperatures to induce thermal dissociation, together with a high flow rate, are needed for  $CH_4$  conversion at low energy cost. Indeed, our model predicts that also in the GAP, vibration-induced dissociation of  $CH_4$  is negligible, and there is no vibrational–translational nonequilibrium. In addition, mainly  $C_2H_2$  and  $H_2$  are formed, next to  $C_2H_4$ . It would be even more beneficial if the selectivity toward  $C_2H_4$  could be enhanced, to make plasma technology of interest for the production of this important chemical compound, and thus for electrification of the chemical industry.<sup>52</sup> Note that the  $C_2H_4$  selectivity could be enhanced by introducing a catalyst after the plasma reactor, to convert the produced  $C_2H_2$  into  $C_2H_4$ , as demonstrated by Delikonstantis et al.<sup>53</sup>

**3.4. Plasma vs Thermal Conversion.** It is clear from previous sections that the higher temperature of MW and GA plasma leads to higher conversion and more selective production of unsaturated hydrocarbons. To investigate whether the conversion in these plasmas is purely thermal or due to (additional) plasma effects, we make a distinction between the plasma effects and the thermal effects for the same range of conditions as investigated in sections 3.2 and 3.3.

Figure 17 shows the  $CH_4$  conversions for the MW plasma at reduced pressure (30 mbar), obtained in the plasma and by pure thermal conversion at the same temperature (i.e., without electron impact reactions, which are specific plasma-based reactions), as a function of SEI, for the continuous (a) and pulsed (b) regime. The corresponding gas temperature is



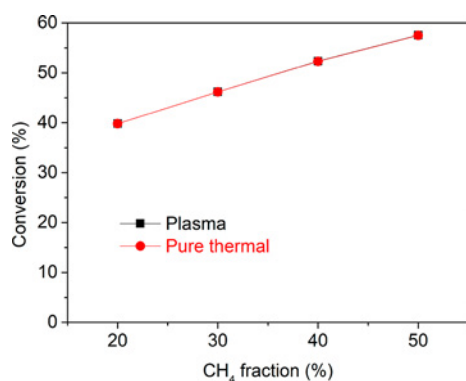
**Figure 17.** Calculated conversion by the plasma and by pure thermal conversion (i.e., without electron impact reactions; left y-axis), as well as calculated maximum gas temperature inside the plasma/pulses (solid line) and averaged over the whole residence time in the reactor (dashed line; right y-axis), as a function of SEI, in a MW plasma at a pressure of 30 mbar and flow rate of 98 sccm, operating in a continuous (a) and pulsed (b) regime.



**Figure 18.** Calculated conversion by the plasma and by pure thermal conversion (i.e., without electron impact reactions) (left y-axis), as well as calculated maximum gas temperature (solid line) and averaged over the whole residence time in the reactor (dashed line) (right y-axis), as a function of microwave power, at a flow rate of 500 mL min<sup>-1</sup> (a), and as a function of flow rate, at a microwave power of 400 W (b), in an atmospheric pressure MW plasma, for a CH<sub>4</sub>/H<sub>2</sub> ratio of 1/4. Note that the plasma conversion and pure thermal conversion perfectly overlap.

plotted in blue color (right y-axis). Both the maximum temperature and averaged temperature (obtained by averaging over the whole residence time) are plotted. At this reduced pressure, almost all conversion is due to plasma effects. Indeed, despite the fact that the maximum temperatures obtained in both the continuous and pulsed mode can reach 1500 K and more, which is in principle sufficient to induce significant thermal conversion, this temperature is only reached for a short time, even in the continuous mode, due to the triangular power profile, as explained in section 1.7 in the SI ( $\sim 30 \mu\text{s}$  in the pulsed mode and  $\sim 100 \mu\text{s}$  in the continuous mode), causing the average temperature in the MW plasma to be too low for thermal conversion. During the short plasma time, however, enough reactive species are created, which, due to the higher local temperatures, react further in neutral reactions. These reactive species are mainly CH<sub>3</sub> and H, as can be seen in Figure 13, and are mainly created by electron impact dissociation of CH<sub>4</sub> or neutral dissociation of higher hydrocarbons, as illustrated in Figures S.12 and S.13 in the SI.

However, in the atmospheric pressure MW plasma and in the GAP discharge, the conversions obtained with and without electron impact reactions are virtually the same, as is clear from Figures 18 and 19, indicating that the conversion is purely thermal at the high temperatures of 3000–3500 K. However, plasmas can still be beneficial above classical thermal conversion,

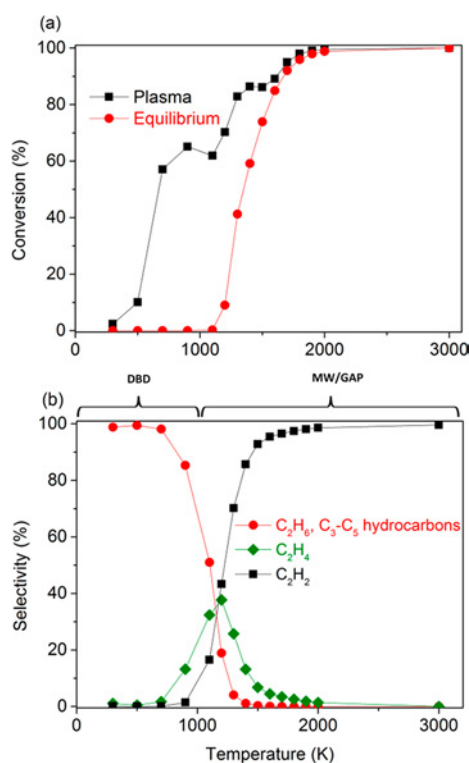


**Figure 19.** Calculated conversion by the plasma and by pure thermal conversion (i.e., without electron impact reactions) in the GAP, as a function of CH<sub>4</sub> fraction in the CH<sub>4</sub>/N<sub>2</sub> mixture, for an input power of 224 W and a flow rate of 10 L min<sup>-1</sup>. The plasma conversion and pure thermal conversion perfectly overlap. The used temperature profile for all conditions studied can be seen in Figure S.1 in the SI.

as high temperatures (3000–3500 K) can be reached by applying electric power (of interest for electrification of chemical reactions) and without damaging the reactor. Indeed, the arc in the GAP can be easily contained in the reactor center due to the reverse vortex flow, which isolates the hot plasma from the reactor walls<sup>54</sup> and in MW plasmas at atmospheric pressure, gas contraction takes place, also focusing the plasma in the center, and thus also protecting the reactor walls.<sup>55,56</sup> Finally, plasmas can be switched on and off quite fast, with ignition times equal to several 100 ms in plasma torches,<sup>57</sup> making them compatible with fluctuating renewable electricity.

Besides the gas temperature, also the electron density is completely different in the three different plasma types. In the DBD plasma the electron densities are calculated to be between  $5 \times 10^{13} \text{ cm}^{-3}$  and  $2 \times 10^{14} \text{ cm}^{-3}$ . In the MW plasma at reduced pressure, the electron densities range between  $1.6 \times 10^{12}$  and  $2.4 \times 10^{13} \text{ cm}^{-3}$ , while in the MW plasma at atmospheric pressure, the electron densities vary between  $6.0 \times 10^{11}$  and  $1.4 \times 10^{12} \text{ cm}^{-3}$ . Finally, in the GAP the electron density is calculated to be  $\sim 6.0 \times 10^{11} \text{ cm}^{-3}$ . Thus, the calculated electron density is the highest in the DBD, more specifically inside the filaments. Combined with the low gas temperature ( $< 500 \text{ K}$ ), it is logical that electron impact reactions, next to three-body recombinations, are dominant. Since a 0D model cannot capture spatial nonuniformities, such as plasma contraction, local higher power densities may be underestimated, which might result in lower electron densities. Nevertheless, since the gas temperatures are around 3000 K or higher in the (atmospheric pressure) MW plasma and the GAP, CH<sub>4</sub> dissociates very fast at these temperatures, so we are confident that our conclusion about the importance of thermal conversion is valid, even if the electron densities would be somewhat underestimated.

To assess whether temperature controls the overall chemical behavior, we plot in Figure 20a,b the CH<sub>4</sub> conversion and product selectivities for a generic type of plasma, at 400 W and a flow rate of 500 mL min<sup>-1</sup>, as a function of gas temperature. It is clear that the temperature indeed plays a determining role in steering the conversion and the product selectivities. Gas temperatures below 1000 K favor radical recombination processes, resulting in more saturated hydrocarbons (C<sub>2</sub>H<sub>6</sub> and higher C<sub>3</sub>–C<sub>5</sub> hydrocarbons), as demonstrated in section 3.1.2 for DBD plasmas. Higher temperatures favor neutral dissociation and dehydrogenation, explaining why C<sub>2</sub>H<sub>4</sub> and especially C<sub>2</sub>H<sub>2</sub> are the dominant products in the MW plasma and the GAP.



**Figure 20.** Calculated conversion (a) and most important hydrocarbon selectivities (b) inside a generic plasma type at atmospheric pressure, a power of 400 W and a flow rate of 500 mL min<sup>-1</sup> for pure CH<sub>4</sub>, as a function of gas temperature. In (a) both the plasma conversion and thermal equilibrium conversion are plotted, indicating a clear difference up to 2000 K.

In Figure 20a we also compare the plasma conversion and conversion at thermal equilibrium, demonstrating that up to a temperature of 2000 K, there is still a significant difference. Hence, the plasma effect can still be important in warm plasmas at atmospheric pressure, when the temperature would be below 2000 K. However, for the atmospheric pressure MW plasma and GAP studied in sections 3.2 and 3.3 above, the gas temperature is around 3000 K or above, and the conversion occurs by thermal processes.

#### 4. CONCLUSIONS

CH<sub>4</sub> conversion into higher hydrocarbons and H<sub>2</sub> by plasma technology is gaining increasing interest as more sustainable alternative to conventional steam reforming. However, different plasma types yield a different performance in terms of conversion, energy cost and selectivity toward different hydrocarbons, and the underlying mechanisms are not yet fully understood. Therefore, we developed a chemical kinetics model to elucidate the main conversion mechanisms of CH<sub>4</sub> into the most important hydrocarbons, especially C<sub>2</sub>H<sub>2</sub>, C<sub>2</sub>H<sub>4</sub> and C<sub>2</sub>H<sub>6</sub>, as well as into H<sub>2</sub>, in the three most commonly used plasma reactors, i.e., a DBD, MW, and GAP reactor. We first compared the calculated conversions, energy costs and product selectivities with experimental results in different reactor configurations and in a wide range of operating conditions. The calculation results are in satisfactory agreement with the experiments, which indicates that our model can provide a realistic picture of the underlying chemistry in CH<sub>4</sub> plasmas and even CH<sub>4</sub>-H<sub>2</sub>-N<sub>2</sub> mixtures, and can be used to elucidate the

underlying mechanisms of CH<sub>4</sub> conversion into various hydrocarbons and H<sub>2</sub> in the different plasma reactors.

The CH<sub>4</sub> conversion is around 20% in the DBD, as well as in the MW plasma at reduced pressure, but it rises to values above 80% in the pulsed MW plasma, as well as at atmospheric pressure, both upon rising SEI. In the GAP, conversions around 50% were obtained, even at high flow rates of 10 L min<sup>-1</sup>. Because of this high flow rate, the GAP operates at much lower SEI than the other plasma sources, i.e., around 1.3 kJ L<sup>-1</sup>, vs 9–54 kJ L<sup>-1</sup> for the DBD, 7–37 kJ L<sup>-1</sup> for the reduced pressure MW plasma, and 24–240 kJ L<sup>-1</sup> for the atmospheric pressure MW plasma. Therefore, the corresponding energy cost is by far the lowest for the GAP (between 5 and 15 kJ/L, decreasing upon higher CH<sub>4</sub> fraction in the mixture), while it is around 40–140 kJ L<sup>-1</sup> in the reduced pressure MW plasma, from 200 until above 1000 kJ L<sup>-1</sup> in the atmospheric pressure MW plasma, and around 125–510 kJ L<sup>-1</sup> in the DBD. As the GAP operates at the highest temperatures, this illustrates that thermal CH<sub>4</sub> conversion is important, and most efficient. Indeed, our model predicts that vibrational–translational nonequilibrium is negligible in all these CH<sub>4</sub> plasmas.

We can conclude that higher temperatures, especially in the GAP but also in atmospheric pressure MW plasmas, result in more CH<sub>4</sub> conversion, and in neutral dissociation and dehydrogenation processes of the hydrocarbons created, forming especially C<sub>2</sub>H<sub>2</sub> and H<sub>2</sub>, and (some) C<sub>2</sub>H<sub>4</sub>. Low temperature plasmas, such as DBD and reduced pressure MW plasmas, result in more electron impact dissociation and three-body recombination processes, creating more saturated compounds, i.e., mainly C<sub>2</sub>H<sub>6</sub>, but also higher hydrocarbons, such as C<sub>3</sub>H<sub>8</sub> and C<sub>4</sub>H<sub>10</sub>.

Thus, high temperature plasmas, and especially the GAP, which operates at high flow rates, are clearly beneficial, for both higher and more energy-efficient CH<sub>4</sub> conversion, as well as more selective production of C<sub>2</sub>H<sub>2</sub> and (to a lower extent) C<sub>2</sub>H<sub>4</sub>. It would even be better if C<sub>2</sub>H<sub>4</sub> would be the major product. To realize this, it is possible to add a catalyst after the plasma reactor, to convert C<sub>2</sub>H<sub>2</sub> into C<sub>2</sub>H<sub>4</sub>, as demonstrated by Delikonstantis et al. for a nanosecond pulsed plasma.<sup>53</sup> This will be the subject of our future work.

#### ■ ASSOCIATED CONTENT

##### Supporting Information

The Supporting Information is available free of charge at <https://pubs.acs.org/doi/10.1021/acs.jpcc.0c00082>.

Full description of the 0D model, including the vibrational and rotational kinetics of CH<sub>4</sub> and the vibrational kinetics of H<sub>2</sub>, and a list of all reactions included in the model for the CH<sub>4</sub> and CH<sub>4</sub>-N<sub>2</sub> chemistry. In addition, details are given on the assumptions made to describe the DBD, MW plasma and GAP, as well as about the experiments performed in the GAP. We also present additional calculation results, i.e., the vibrational and gas temperature in the different plasma sources, to demonstrate that the various CH<sub>4</sub> plasmas investigated are close to vibrational–translational equilibrium. Finally, we present the calculated rates of the most important reactions in the various plasma sources, to identify the reaction pathways plotted in Figures 8, 13, 14 and 16 and the net contribution of the most important formation mechanisms of H and CH<sub>3</sub> in the reduced pressure MW discharge. (PDF)

## ■ AUTHOR INFORMATION

## Corresponding Authors

**Stijn Heijkers** – Research group PLASMANT, Department of Chemistry, University of Antwerp BE-2610 Wilrijk-Antwerp, Belgium; [orcid.org/0000-0001-7142-9697](https://orcid.org/0000-0001-7142-9697);

Phone: +3232652369; Email: [stijn.heijkers@uantwerpen.be](mailto:stijn.heijkers@uantwerpen.be)

**Annemie Bogaerts** – Research group PLASMANT, Department of Chemistry, University of Antwerp BE-2610 Wilrijk-Antwerp, Belgium; [orcid.org/0000-0001-9875-6460](https://orcid.org/0000-0001-9875-6460);

Phone: +3232652377; Email: [annemie.bogaerts@uantwerpen.be](mailto:annemie.bogaerts@uantwerpen.be)

## Author

**Maryam Aghaei** – Research group PLASMANT, Department of Chemistry, University of Antwerp BE-2610 Wilrijk-Antwerp, Belgium; [orcid.org/0000-0003-4995-8773](https://orcid.org/0000-0003-4995-8773)

Complete contact information is available at:

<https://pubs.acs.org/10.1021/acs.jpcc.0c00082>

## Notes

The authors declare no competing financial interest.

## ■ ACKNOWLEDGMENTS

We acknowledge financial support from the Fund for Scientific Research, Flanders (FWO; Grant No. G.0383.16N), the Methusalem Grant, and the European Research Council (ERC) under the European Union's Horizon 2020 research and innovation programme (Grant Agreement No. 810182 – SCOPE ERC Synergy project). This work was carried out in part using the Turing HPC infrastructure at the CalcUA core facility of the Universiteit Antwerpen, a division of the Flemish Supercomputer Center VSC, funded by the Hercules Foundation, the Flemish Government (department EWI) and the University of Antwerp.

## ■ REFERENCES

- (1) Van Geem, K. M.; Galvita, V. V.; Marin, G. B. Making Chemicals with Electricity. *Science (Washington, DC, U. S.)* **2019**, *364*, 734–735.
- (2) Bellussi, G.; Pollesel, P. Industrial Applications of Zeolite Catalysis: Production and Uses of Light Olefins. *Stud. Surf. Sci. Catal.* **2005**, *158*, 1201–1212.
- (3) Hoveyda, A. H.; Zhugralin, A. R. The Remarkable Metal-Catalysed Olefin Metathesis Reaction. *Nature* **2007**, *450*, 243–251.
- (4) Holmen, A.; Olsvik, O.; Rokstad, O. A. Pyrolysis of Natural Gas: Chemistry and Process Concepts. *Fuel Process. Technol.* **1995**, *42*, 249–267.
- (5) Scapinello, M.; Delikonstantis, E.; Stefanidis, G. D. The Panorama of Plasma-Assisted Non-Oxidative Methane Reforming. *Chem. Eng. Process.* **2017**, *117*, 120–140.
- (6) Snoeckx, R.; Bogaerts, A. Plasma Technology—a Novel Solution for CO<sub>2</sub> Conversion? *Chem. Soc. Rev.* **2017**, *46*, 5805–5863.
- (7) Kasinathan, P.; Park, S.; Choi, W. C.; Hwang, Y. K.; Chang, J. S.; Park, Y. K. Plasma-Enhanced Methane Direct Conversion over Particle-Size Adjusted MO<sub>x</sub>/Al<sub>2</sub>O<sub>3</sub> (M = Ti and Mg) Catalysts. *Plasma Chem. Plasma Process.* **2014**, *34*, 1317–1330.
- (8) Lü, J.; Li, Z. Conversion of Natural Gas to C<sub>2</sub> Hydrocarbons via Cold Plasma Technology. *J. Nat. Gas Chem.* **2010**, *19*, 375–379.
- (9) Li, X. S.; Zhu, A. M.; Wang, K. J.; Xu, Y.; Song, Z. M. Methane Conversion to C<sub>2</sub> Hydrocarbons and Hydrogen in Atmospheric Non-Thermal Plasmas Generated by Different Electric Discharge Techniques. *Catal. Today* **2004**, *98*, 617–624.
- (10) Xu, C.; Tu, X. Plasma-Assisted Methane Conversion in an Atmospheric Pressure Dielectric Barrier Discharge Reactor. *J. Energy Chem.* **2013**, *22*, 420–425.

(11) Zhang, H.; Du, C.; Wu, A.; Bo, Z.; Yan, J.; Li, X. Rotating Gliding Arc Assisted Methane Decomposition in Nitrogen for Hydrogen Production. *Int. J. Hydrogen Energy* **2014**, *39*, 12620–12635.

(12) Heintze, M.; Magureanu, M. Methane Conversion into Acetylene in a Microwave Plasma: Optimization of the Operating Parameters. *J. Appl. Phys.* **2002**, *92* (5), 2276–2283.

(13) Cho, W.; Kim, Y. C.; Kim, S. S. Conversion of Natural Gas to C<sub>2</sub> Product, Hydrogen and Carbon Black Using a Catalytic Plasma Reaction. *J. Ind. Eng. Chem.* **2010**, *16*, 20–26.

(14) Shen, C.; Sun, D.; Yang, H. Methane Coupling in Microwave Plasma under Atmospheric Pressure. *J. Nat. Gas Chem.* **2011**, *20*, 449–456.

(15) Młotek, M.; Sentek, J.; Krawczyk, K.; Schmidt-Szałowski, K. The Hybrid Plasma-Catalytic Process for Non-Oxidative Methane Coupling to Ethylene and Ethane. *Appl. Catal., A* **2009**, *366*, 232–241.

(16) Yuhan, Z. Methane Pyrolysis to Acetylene in Gliding Arc Plasma Driven by Magnetism. *Proc. - Int. Conf. Comput. Distrib. Control Intell. Environ. Monit. CDCIEM 2011* **2011**, *2*, 894–896.

(17) Lee, H.; Sekiguchi, H. Plasma-Catalytic Hybrid System Using Spouted Bed with a Gliding Arc Discharge: CH<sub>4</sub> Reforming as a Model Reaction. *J. Phys. D: Appl. Phys.* **2011**, *44*, 274008.

(18) Polak, L. S. Low-Temperature Plasma in Petroleum Chemistry. *Pet. Chem. U.S.S.R* **1967**, *7*, 136–152.

(19) Indarto, A.; Coowanitwong, N.; Choi, J. W.; Lee, H.; Song, H. K. Kinetic Modeling of Plasma Methane Conversion in a Dielectric Barrier Discharge. *Fuel Process. Technol.* **2008**, *89*, 214–219.

(20) De Bie, C.; Verheyde, B.; Martens, T.; Van Dijk, J.; Paulussen, S.; Bogaerts, A. Fluid Modeling of the Conversion of Methane into Higher Hydrocarbons in an Atmospheric Pressure Dielectric Barrier Discharge. *Plasma Processes Polym.* **2011**, *8*, 1033–1058.

(21) Istadi, I.; Amin, N. A. S. Modelling and Optimization of Catalytic-Dielectric Barrier Discharge Plasma Reactor for Methane and Carbon Dioxide Conversion Using Hybrid Artificial Neural Network-Genetic Algorithm Technique. *Chem. Eng. Sci.* **2007**, *62* (23), 6568–6581.

(22) Yang, Y. Direct Non-Oxidative Methane Conversion by Non-Thermal Plasma: Modeling Study. *Plasma Chem. Plasma Process.* **2003**, *23*, 327–346.

(23) Dors, M.; Nowakowska, H.; Jasiński, M.; Mizeraczyk, J. Chemical Kinetics of Methane Pyrolysis in Microwave Plasma at Atmospheric Pressure. *Plasma Chem. Plasma Process.* **2014**, *34*, 313–326.

(24) Indarto, A.; Choi, J. W.; Lee, H.; Song, H. K. Kinetic Modeling of Plasma Methane Conversion Using Gliding Arc. *J. Nat. Gas Chem.* **2005**, *14*, 13–21.

(25) Hassouni, K.; Duten, X.; Rousseau, A.; Gicquel, A. Investigation of Chemical Kinetics and Energy Transfer in a Pulsed Microwave H<sub>2</sub>/CH<sub>4</sub> Plasma. *Plasma Sources Sci. Technol.* **2001**, *10*, 61–75.

(26) Lombardi, G.; Hassouni, K.; Stancu, G. D.; Mechold, L.; Röpcke, J.; Gicquel, A. Study of an H<sub>2</sub>/CH<sub>4</sub> Moderate Pressure Microwave Plasma Used for Diamond Deposition: Modelling and IR Tuneable Diode Laser Diagnostic. *Plasma Sources Sci. Technol.* **2005**, *14*, 440–450.

(27) Snoeckx, R.; Aerts, R.; Tu, X.; Bogaerts, A. Plasma-Based Dry Reforming: A Computational Study Ranging from the Nanoseconds to Seconds Time Scale. *J. Phys. Chem. C* **2013**, *117*, 4957–4970.

(28) Cleiren, E.; Heijkers, S.; Ramakers, M.; Bogaerts, A. Dry Reforming of Methane in a Gliding Arc Plasmatron: Towards a Better Understanding of the Plasma Chemistry. *ChemSusChem* **2017**, *10*, 4025–4036.

(29) Pancheshnyi, S.; Eismann, B.; Hagelaar, G. J. M.; Pitchford, L. C. *ZDPlasKin: A New Tool for Plasmachemical Simulations*; University of Toulouse, LAPLACE, CNRS-UPS-INP: Toulouse, France, 2008.

(30) Hagelaar, G. J. M.; Pitchford, L. C. Solving the Boltzmann Equation to Obtain Electron Transport Coefficients and Rate Coefficients for Fluid Models. *Plasma Sources Sci. Technol.* **2005**, *14*, 722–733.

(31) Kozak, T.; Bogaerts, A. Evaluation of the Energy Efficiency of CO<sub>2</sub> Conversion in Microwave Discharges Using a Reaction Kinetics Model. *Plasma Sources Sci. Technol.* **2015**, *24*, 015024.

- (32) Wang, B.; Yan, W.; Ge, W.; Duan, X. Methane Conversion into Higher Hydrocarbons with Dielectric Barrier Discharge Micro-Plasma Reactor. *J. Energy Chem.* **2013**, *22*, 876–882.
- (33) Ozkan, A.; Dufour, T.; Silva, T.; Britun, N.; Snyders, R.; Reniers, F.; Bogaerts, A. DBD in Burst Mode : Solution for More Efficient CO<sub>2</sub> Conversion? *Plasma Sources Sci. Technol.* **2016**, *25*, 055005.
- (34) Ozkan, A.; Dufour, T.; Bogaerts, A.; Reniers, F. How Do the Barrier Thickness and Dielectric Material Influence the Filamentary Mode and CO<sub>2</sub> Conversion in a Flowing DBD? *Plasma Sources Sci. Technol.* **2016**, *25*, 045016.
- (35) Fridman, A. *Plasma Chemistry*; Cambridge University Press: New York, 2008.
- (36) Papageorghiou, L.; Panousis, E.; Loiseau, J. F.; Spyrou, N.; Held, B. Two-Dimensional Modelling of a Nitrogen Dielectric Barrier Discharge (DBD) at Atmospheric Pressure: Filament Dynamics with the Dielectric Barrier on the Cathode. *J. Phys. D: Appl. Phys.* **2009**, *42*, 105201.
- (37) Snoeckx, R.; Heijkers, S.; Van Wesenbeeck, K.; Lenaerts, S.; Bogaerts, A. CO<sub>2</sub> Conversion in a Dielectric Barrier Discharge Plasma: N<sub>2</sub> in the Mix as a Helping Hand or Problematic Impurity? *Energy Environ. Sci.* **2016**, *9*, 30–39.
- (38) Kuznetsova, I. V.; Kalashnikov, N. Y.; Gutsol, a. F.; Fridman, a. a.; Kennedy, L. a. Effect of “Overshooting” in the Transitional Regimes of the Low-Current Gliding Arc Discharge. *J. Appl. Phys.* **2002**, *92* (8), 4231–4237.
- (39) Nunnally, T. P. *Application of Low Current Gliding Arc Plasma Discharges for Hydrogen Sulfide Decomposition and Carbon Dioxide Emission Reduction*. Ph.D. Dissertation; Drexel University, 2011.
- (40) Nunnally, T.; Gutsol, K.; Rabinovich, A.; Fridman, A.; Gutsol, A.; Kemoun, A. Dissociation of CO<sub>2</sub> in a Low Current Gliding Arc Plasmatron. *J. Phys. D: Appl. Phys.* **2011**, *44*, 274009.
- (41) Ramakers, M.; Trenchev, G.; Heijkers, S.; Wang, W.; Bogaerts, A. Gliding Arc Plasmatron: Providing a Novel Method for Carbon Dioxide Conversion. *ChemSusChem* **2017**, *10*, 2642–2652.
- (42) Ramakers, M.; Heijkers, S.; Tytgat, T.; Lenaerts, S.; Bogaerts, A. Combining CO<sub>2</sub> Conversion and N<sub>2</sub> Fixation in a Gliding Arc Plasmatron. *J. CO<sub>2</sub> Util.* **2019**, *33*, 121–130.
- (43) Trenchev, G.; Kolev, S.; Bogaerts, A. A 3D Model of a Reverse Vortex Flow Gliding Arc Reactor. *Plasma Sources Sci. Technol.* **2016**, *25* (3), 035014.
- (44) Trenchev, G.; Kolev, S.; Wang, W.; Ramakers, M.; Bogaerts, A. CO<sub>2</sub> Conversion in a Gliding Arc Plasmatron: Multidimensional Modeling for Improved Efficiency. *J. Phys. Chem. C* **2017**, *121* (44), 24470–24479.
- (45) Heijkers, S.; Bogaerts, A. CO<sub>2</sub> Conversion in a Gliding Arc Plasmatron: Elucidating the Chemistry through Kinetic Modeling. *J. Phys. Chem. C* **2017**, *121*, 22644–22655.
- (46) Kozák, T.; Bogaerts, A. Splitting of CO<sub>2</sub> by Vibrational Excitation in Non-Equilibrium Plasmas: A Reaction Kinetics Model. *Plasma Sources Sci. Technol.* **2014**, *23*, 045004.
- (47) Berthelot, A.; Bogaerts, A. Modeling of CO<sub>2</sub> Splitting in a Microwave Plasma: How to Improve the Conversion and Energy Efficiency. *J. Phys. Chem. C* **2017**, *121* (15), 8236–8251.
- (48) Vermeiren, V.; Bogaerts, A. Supersonic Microwave Plasma: Potential and Limitations for Energy-Efficient CO<sub>2</sub> Conversion. *J. Phys. Chem. C* **2018**, *122*, 25869–25881.
- (49) Van Alphen, S.; Vermeiren, V.; Butterworth, T.; Van Den Bekerom, D. C. M.; Van Rooij, G. J.; Bogaerts, A. Power Pulsing to Maximize Vibrational Excitation Efficiency in N<sub>2</sub> Microwave Plasma: A Combined Experimental and Computational Study. *J. Phys. Chem. C* **2020**, *124*, 1765.
- (50) Butterworth, T. D.; Amyay, B.; Bekerom, D. V.D.; Steeg, A. V.D.; Minea, T.; Gatti, N.; Ong, Q.; Richard, C.; van Kruijsdijk, C.; Smits, J. T.; et al. Quantifying Methane Vibrational and Rotational Temperature with Raman Scattering. *J. Quant. Spectrosc. Radiat. Transfer* **2019**, *236*, 106562.
- (51) Bogaerts, A.; Neyts, E. C. Plasma Technology: An Emerging Technology for Energy Storage. *ACS Energy Lett.* **2018**, *3*, 1013–1027.
- (52) Schiffer, Z. J.; Manthiram, K. Electrification and Decarbonization of the Chemical Industry. *Joule* **2017**, *1*, 10–14.
- (53) Delikonstantis, E.; Scapinello, M.; Stefanidis, G. D. Low Energy Cost Conversion of Methane to Ethylene in a Hybrid Plasma-Catalytic Reactor System. *Fuel Process. Technol.* **2018**, *176*, 33–42.
- (54) Kalra, C. S.; Cho, Y. I.; Gutsol, A.; Fridman, A.; Rufael, T. S. Gliding Arc in Tornado Using a Reverse Vortex Flow. *Rev. Sci. Instrum.* **2005**, *76* (2), 025110.
- (55) Kabouzi, Y.; Calzada, M. D.; Moisan, M.; Tran, K. C.; Trassy, C. Radial Contraction of Microwave-Sustained Plasma Columns at Atmospheric Pressure. *J. Appl. Phys.* **2002**, *91*, 1008–1019.
- (56) den Harder, N.; van den Bekerom, D. C. M.; Al, R. S.; Graswinckel, M. F.; Palomares, J. M.; Peeters, F. J. J.; Ponduri, S.; Minea, T.; Bongers, W. A.; van de Sanden, M. C. M.; et al. Homogeneous CO<sub>2</sub> Conversion by Microwave Plasma: Wave Propagation and Diagnostics. *Plasma Process. Polym.* **2017**, *14*, e1600120.
- (57) Cao, X.; Yu, D.; Xiang, Y.; Li, C.; Jiang, H.; Yao, J. Study on the Ignition Process of a Segmented Plasma Torch. *Plasma Sci. Technol.* **2017**, *19*, 075404.