

*Plasma-based N<sub>2</sub> fixation into NO<sub>x</sub>:*

*Insights from modeling toward optimum yields and energy  
costs in a gliding arc plasmatron*

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Figure S.7 Calculated number densities of NO, NO<sub>2</sub>, O and N (a), and net rates of the main reactions as function of the residence time (b), for an 80/20 N<sub>2</sub>/O<sub>2</sub> mixture at 1.25 bar, 10 L min<sup>-1</sup> and 415 W.

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## 1. Comparison with different plasma sources applied for NO<sub>x</sub> formation

Table S.1 Yield and energy cost for NO<sub>x</sub> formation in different plasma sources. They all operate at atmospheric pressure, unless mentioned otherwise. The HB process for NH<sub>3</sub> synthesis is also added, as benchmark.

Reactor	Yield [%]	Energy cost [MJ/mol]	Ref.
GAP	1.5 % NO <sub>x</sub>	3.6 MJ/mol NO <sub>x</sub>	This work
Electric arc (Birkeland – Eyde)	1 – 2 % NO	2.41 MJ/mol NO	2
Electric arc with water injection	2.41 % NO	3.5 MJ/mol NO	3
MW at reduced pressure with MoO <sub>3</sub> catalyst	6 % NO	0.84 MJ/mol NO	4
Pulsed MW at reduced pressure	6 % NO	0.60 MJ/mol NO	5
MW with magnetic field at reduced pressure	14 % NO	0.30 MJ/mol NO	6
DBD with γ – Al <sub>2</sub> O <sub>3</sub> catalyst	0.5 % NO <sub>x</sub>	18 MJ/mol NO <sub>x</sub>	7
Shielded sliding discharge	0.1 % NO <sub>x</sub>	15.4 MJ/mol NO <sub>x</sub>	8
Pulsed milliscale GA	2 % NO <sub>x</sub>	2.8 MJ/mol NO <sub>x</sub>	9
Haber – Bosch	10 – 20 % NH <sub>3</sub> <sup>a</sup>	0.48 MJ/mol <sup>a</sup>	10

- a. Yield after one pass, depending on the specific plant, and energy cost of the whole process.

## 2. Details on the experimental setup

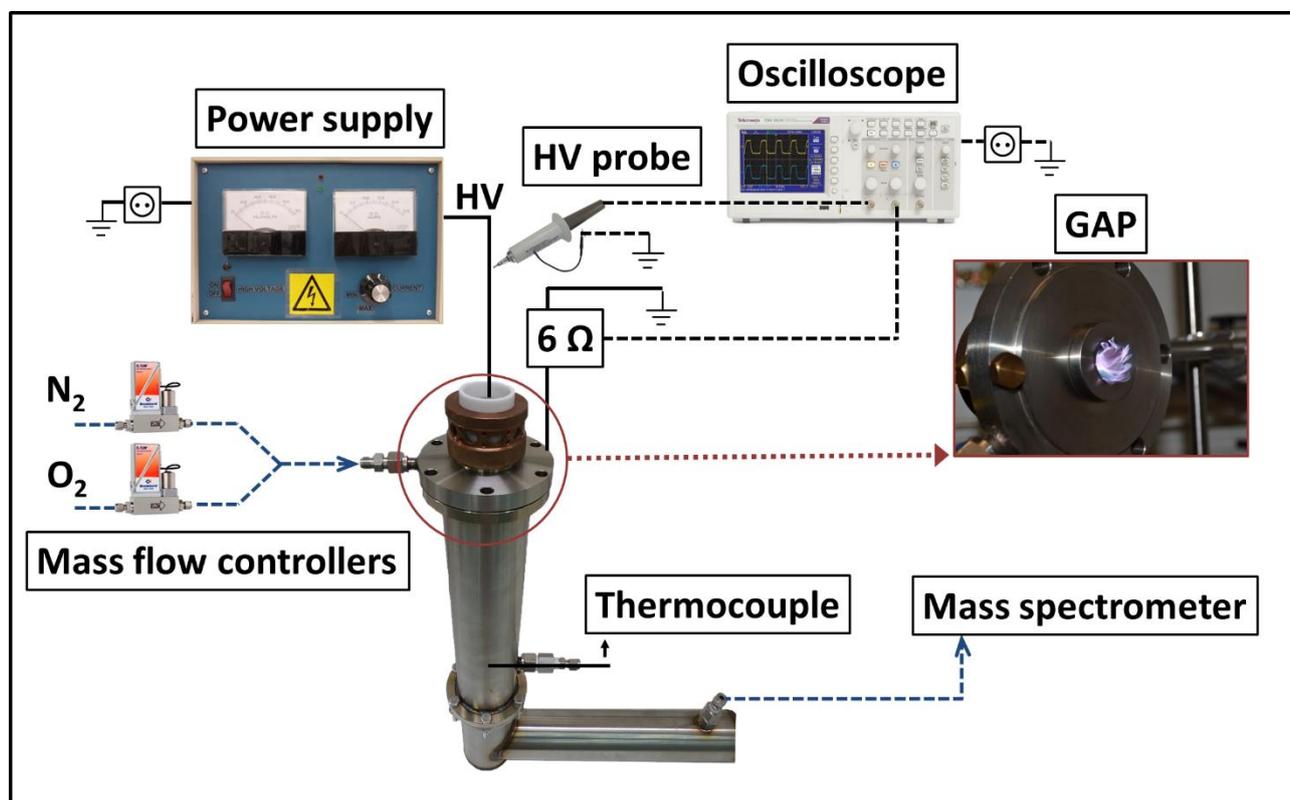


Figure S.1 Schematics of the entire experimental system used for the experimental procedure that was explained in the main paper.

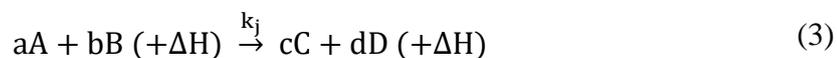
For safety and environmental concerns, we have NO and NO<sub>2</sub> sensors in the lab to detect any probable leak. In addition, the whole experimental setup is placed in a separated fume hood, connected to special air filters to avoid introducing the exhaust gas to the open air and harming the environment.

## 3. 0D model description

A zero-dimensional (0D) chemical kinetics model was developed to solve a set of continuity equations (Eq. 2) for all individual species included in the model (see Table S.2), in order to obtain the species densities as a function of time:

$$\frac{dn_i}{dt} = \sum_j \left[ (a_{ij}^R - a_{ij}^L) k_j \prod_l n_l^L \right] \quad (2)$$

$n_i$  is the density of species  $i$ ,  $a_{ij}^R$  and  $a_{ij}^L$  are the right and left stoichiometric coefficients for the following general reaction:



With species  $i$  for reaction  $j$ . Here,  $A$ ,  $B$ ,  $C$  and  $D$  are the different species and  $a$ ,  $b$ ,  $c$  and  $d$  are their respective stoichiometric coefficients.  $\Delta H$  represents the enthalpy of reaction  $j$ . The reaction rate coefficient,  $k_j$ , of the heavy particle reactions are either constant or dependent on the gas temperature and are expressed in  $\text{cm}^3 \text{s}^{-1}$  or  $\text{cm}^6 \text{s}^{-1}$  for two-body or three-body reactions, respectively. The rate coefficients of the electron impact reactions can depend on the electron temperature  $T_e$  (or the reduced electric field  $E/N$ , i.e., the electric field  $E$  divided by the number density of all neutral species  $N$ , usually expressed in  $\text{Td} = 10^{-21} \frac{\text{V}}{\text{m}^2}$ ). Most rate coefficients of electron impact reactions are calculated according to the following equation:

$$k_i = \int_{\varepsilon_{\text{th}}}^{\infty} \sigma_i(\varepsilon) v(\varepsilon) f(\varepsilon) d\varepsilon \quad (4)$$

$\varepsilon$  is the electron energy (usually in eV),  $\varepsilon_{\text{th}}$  is the minimum threshold energy needed to induce the reaction,  $v(\varepsilon)$  the velocity of the electrons,  $\sigma_i(\varepsilon)$  is the cross section of collision  $i$ , and  $f(\varepsilon)$  is the electron energy distribution function (EEDF). We use the ZDPlasKin<sup>11</sup> code to solve the balance equations (Eq. 2) for all species, which has a built-in Boltzmann solver, BOLSIG+<sup>12</sup>, to calculate the EEDF and the rate coefficients of the electron impact reactions based on a set of cross sections, the plasma composition, the gas temperature and the reduced electric field ( $E/N$ ). The electric field ( $E$ ) is calculated from a given power density, using the so-called local field approximation<sup>13</sup>:

$$E = \sqrt{\frac{P}{\sigma}} \quad (5)$$

$P$  is the input power density ( $\text{W m}^{-3}$ ) and  $\sigma$  is the plasma conductivity ( $\text{A V}^{-1} \text{m}^{-1}$ ). The plasma conductivity is<sup>13</sup>

$$\sigma = e n_e \mu_e \quad (6)$$

$n_e$  is the electron number density and  $\mu_e$  is the electron mobility.

The model is applied to the GAP reactor at exactly the same dimensions and operating conditions as in the experiments. A schematic diagram of the GAP, including the dimensions, is presented in Figure S.2. The arc plasma column inside the GAP is illustrated by the red rectangle. Because the gas enters the GAP reactor by tangential inlets, it follows a vortex flow pattern. As the outlet (anode) diameter is smaller than the reactor body (cathode part) (see Figure S.2a), the gas will first move upwards in a so-called forward vortex flow (indicated in Figure S.2a by the solid spiral). When the gas arrives at the top of the reactor, it will have lost most of its speed by friction and inertia. The gas will then travel downwards in a smaller so-called reverse vortex flow, which is more or less captured by the arc column (see dashed spiral in Figure S.2a).

The reverse vortex flow results in the stabilization of the arc column in the centre of the GAP, as was previously predicted by 3D fluid dynamics simulations.<sup>14,15</sup> The vast majority of the plasma conversion thus takes place in the column-shaped centre of the reactor. Since the plasma is confined

in the inner vortex of the gas flow, the plasma can be considered uniform and we can assume a constant power density applied to the gas during its residence time in the plasma. This is convenient for the 0D model, which does not include spatial variations or transport. However, the calculated temporal dependence of the species densities can be transformed into a spatial dependence through the reactor by means of the gas flow rate<sup>16,17</sup> (see Figure S.2b). The arc plasma column is thus considered as a plug flow reactor, where the plasma characteristics vary as a function of distance travelled by the gas within a certain residence time, in the same way as they would vary as a function of time in a batch reactor. 2D fluid dynamics simulation results of Trenchev et al. for a GAP in argon<sup>14,15</sup> revealed that the arc radius is typically around 1 mm. However, the temperature just outside this arc region is still high enough to induce plasma, especially in a molecular plasma where vibration-translation (VT) relaxation causes gas heating. Therefore, we assumed an arc radius of 2 mm in our simulations. Combined with the length of the cathode (10.20 mm) and anode (16.30 mm) and the inlet of 3 mm (see Figure S.1), this yields a plasma volume of 0.37 cm<sup>3</sup>. These input data were also successfully used in<sup>18–20</sup>.

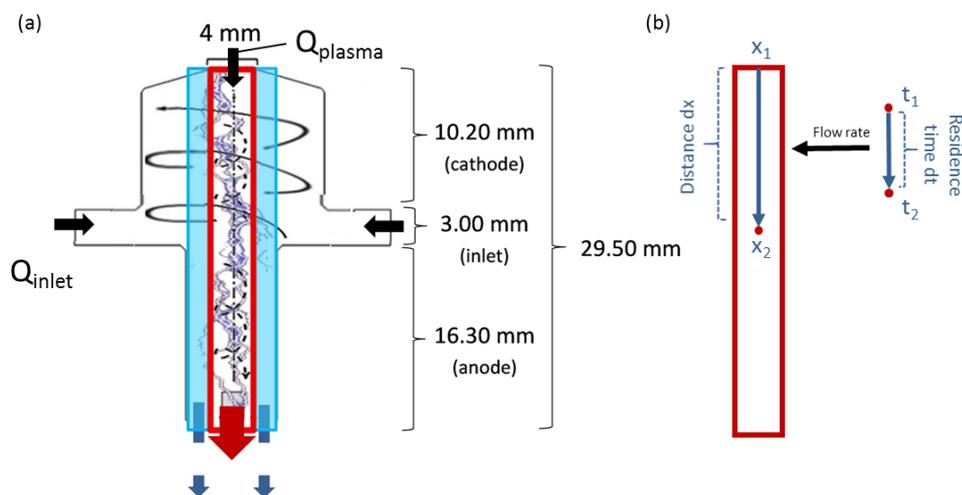


Figure S.2 (a) Schematic illustration of the GAP, indicating its dimensions as well as the outer vortex (solid spiral) and the inner (reverse) vortex (dashed spiral). The red frame indicates the plasma arc column, while the blue part indicates the region where the gas leaves the reactor without being treated. (b) Schematic of the 0D modeling approach in which the time dependency is translated into a spatial dependency by means of the gas flow rate.

We assume a constant temperature of 3000 K as input in our model, based on 3D fluid dynamics simulations<sup>14,15</sup>. Note that the calculated value was obtained for CO<sub>2</sub>, and the experimental value for pure N<sub>2</sub>, but not for N<sub>2</sub>/O<sub>2</sub> gas mixtures. We expect the temperature profiles to be similar as they are all molecular gasses, as they experience the same mechanisms causing gas heating. We can also safely assume that the gas is already heated up to 3000 K when it enters the inner vortex, where the majority of the conversion takes place, so this is why the temperature profile starts at 3000 K and is kept constant. Gröger et al. have measured a gas temperature of 5000 K in our GAP operating in pure N<sub>2</sub>.<sup>21</sup> This high temperature, however, likely originates from the hot cathode spot, so we think that 3000 K is a better estimate of the gas temperature inside the arc.

As initial conditions in the plasma, we start with a fixed electron density of  $10^{10} \text{ cm}^{-3}$ , considering only  $\text{N}_2$  and  $\text{O}_2$  molecules, including their vibrationally excited equivalents,  $\text{N}_2^+$  and  $\text{O}_2^+$  ions and electrons. We assume quasi-neutrality by setting the electron density equal to the sum of the densities of the  $\text{N}_2^+$  and  $\text{O}_2^+$  ions, according to their fraction in the inlet mixture. In addition, we assume a Boltzmann distribution for all vibrationally excited species, at a temperature of 3000 K. The sum of the initial densities of  $\text{N}_2$ ,  $\text{N}_2(v_x)$  and  $\text{N}_2^+$  ions amounts to the total density that  $\text{N}_2$  would have according to its initial fraction in the feed. Similarly, the sum of the initial densities of  $\text{O}_2$ ,  $\text{O}_2(v_x)$  and  $\text{O}_2^+$  ions is according to the  $\text{O}_2$  fraction in the feed.

Vibrational excitation of  $\text{N}_2$  is promoted in the GAP and is advantageous for more energy-efficient dissociation of  $\text{N}_2$ , because it can help to overcome the reaction energy barrier of the Zeldovich mechanism.<sup>22,23</sup> Therefore, special attention is given to the vibrational levels: 24 vibrational levels for  $\text{N}_2$  and 15 levels for  $\text{O}_2$  were implemented in the model. The species taken into account in the model are listed in Table S.2. This includes neutral molecules in the ground, vibrationally and electronically excited states, various radicals, positive and negative ions, and electrons. In total, 1195 different electron impact, 435 neutral-neutral, 523 ion-neutral and 48 ion-ion chemical reactions are included, as well as 2478 vibrational-vibrational (VV) exchanges and vibrational-translational (VT) relaxations between  $\text{N}_2 - \text{N}_2$ ,  $\text{O}_2 - \text{O}_2$ , and  $\text{N}_2 - \text{O}_2$ , and between  $\text{O}_2 - \text{O}_2$ ,  $\text{N}_2 - \text{N}_2$ ,  $\text{N}_2 - \text{N}$  and  $\text{O}_2 - \text{O}$ , for all vibrational levels. The reaction set of in reference<sup>24</sup> was revised and used, but with the addition of  $\text{N}_2 - \text{O}_2$  VV exchanges and  $\text{N}_2 - \text{N}$  and  $\text{O}_2 - \text{O}$  VT relaxations. The latter processes do not significantly influence the  $\text{NO}_x$  formation at the conditions under study, but were included for the sake of completeness. The  $\text{N}_2 - \text{O}_2$  VV exchanges are demonstrated to be very important (cf. Figure 6 in the main paper). The vibrational levels of  $\text{NO}$  and  $\text{NO}_2$  are not included, because of lack of data on their vibrational kinetics in literature. All reactions are listed under section 9.

Table S.2 Species included in the model

<b><math>\text{N}_2</math> species</b>	
Neutral ground state molecules	$\text{N}_2$
Ions	$\text{N}^+, \text{N}_2^+, \text{N}_3^+, \text{N}_4^+$
Vibrationally excited molecules	$\text{N}_2(v_1 - v_{24})$
Electronically excited molecules or atoms	$\text{N}_2(\text{A}^3\Sigma_u^+), \text{N}_2(\text{B}^3\Pi_g), \text{N}_2(\text{C}^3\Pi_u)$ and $\text{N}_2(\text{a}^1\Sigma_u^-), \text{N}(2D), \text{N}(2P)$
Radicals	$\text{N}$
<b><math>\text{N}_x\text{O}_y</math> species</b>	
$\text{NO}, \text{N}_2\text{O}, \text{NO}_2, \text{NO}_3, \text{N}_2\text{O}_5, \text{N}_2\text{O}_3, \text{N}_2\text{O}_4, \text{NO}^+, \text{N}_2\text{O}^+, \text{NO}_2^+, \text{NO}^-, \text{N}_2\text{O}^-, \text{NO}_2^-, \text{NO}_3^-, \text{O}_2^+\text{N}_2$	
<b><math>\text{O}_2</math> species</b>	

Neutral ground state molecules	$O_2, O_3$
Ions	$O^-, O_2^-, O_3^-, O_4^-, O^+, O_2^+, O_4^+$
Vibrationally excited molecules	$O_2 (v_1 - v_{15})$
Electronically excited molecules or atoms	$O (1D), O (1S), O_2(a^1\Delta), O_2(b^1\Sigma^+)$ and a combination of three states, i.e. $O_2(A^3\Sigma^+, C^3\Delta, c^1\Sigma^-)$ at a threshold energy of 4.5 eV.
radicals	$O$

The product yield, also reported in the main paper, is defined as:

$$Y_x = Y_{x,arc} \cdot f \quad (7)$$

where  $f$  is the fraction of gas passing through the plasma arc and is defined as:

$$f = \frac{Q_{plasma}}{Q_{inlet}} \quad (8)$$

where  $Q_{inlet}$  is the flow rate at the inlet of the reactor and  $Q_{plasma}$  is the flow rate of the gas in the plasma region (red frame in Figure S.1(a)). In a GAP operating at atmospheric pressure, only 14.8% of the gas flows through the plasma region and the remaining 85.2% is assumed in this model to leave the reactor without being treated.  $Y_{x,arc}$  corresponds to the product yield in the plasma arc region and is defined as:

$$Y_{x,arc} = \frac{n_x}{n_0} \cdot 100\% \quad (9)$$

where  $n_x$  is the density ( $\text{cm}^{-3}$ ) of species  $x$ , for example NO or  $\text{NO}_2$  and  $n_0$  is the initial gas density.

## 4. Detailed experimental results

The experimental procedure consists of stabilizing the plasma for 15 minutes, followed by online continuous mass spectrometry measurements, and at the same time recording the plasma voltage and current in order to calculate the plasma power, and finally a cool down and flush period of 30 minutes with the next gas mixture. Each condition is repeated for three times and the results shown below are, thus, the average of these three measurements.

### 4.1 Plasma power measurement

To calculate the plasma power, we measured the voltage and current passing through the arc. For this purpose, an oscilloscope (Tektronix TDS2012C) was used. The voltage was measured using a high voltage probe (Testec) connected to the cathode, the ground wire and channel 1 of the oscilloscope. The current was measured over an external resistor box by a wire connection to the second channel of the oscilloscope, using  $I = V/R$  with the resistance of the resistor box being 6 Ohm. The potential and current over a certain period of time were used to calculate the plasma power with the following formula:

$$P_{\text{plasma}} = \frac{1}{T} \int_0^{t=T} V_{\text{plasma}} \cdot I_{\text{plasma}} dt \quad (1)$$

Also, several pressure sensors were placed along the gas circuit to monitor the correct working of the setup during the experiments. Table S.3 shows the average plasma power measured by the oscilloscope, as well as the specific energy input (SEI) for each N<sub>2</sub>/O<sub>2</sub> ratio with a total flow rate of 10 L/min. The error values are also indicated in Table S.3.

*Table S.3 Average plasma power for different N<sub>2</sub>/O<sub>2</sub> ratios and different flow rates.*

<b>N<sub>2</sub>/O<sub>2</sub> ratio</b>	<b>Total flow rate [L/min]</b>	<b>Flow rate-error</b>	<b>Average plasma power [W]</b>	<b>Power-error</b>	<b>SEI [J/L]</b>	<b>SEI-error</b>
9/1	10.00	0.07	365	9	2190	57
8/2	10.00	0.07	369	28	2214	171
7/3	10.00	0.07	379	11	2274	69
6/4	10.00	0.07	409	25	2454	151
5/5	10.00	0.07	415	11	2492	71
4/6	10.00	0.07	434	23	2606	139
3/7	10.00	0.07	437	13	2624	83
2/8	10.00	0.07	458	12	2748	75
1/9	10.00	0.07	381	33	2289	201
8/2	8.000	5.01	490	5	3679	48
8/2	12.000	17.84	390	18	1951	90
8/2	14.000	32.08	428	16	1837	70
8/2	16.000	25.56	548	26	2057	97
8/2	18.000	29.70	390	30	1299	99
8/2	20.000	11.12	490	11	1471	34
8/2	22.000	33.85	364	34	993	92
8/2	25.000	11.55	476	12	1144	28
8/2	30.000	12.89	375	13	750	26

## 4.2 Gas analysis and product concentrations

The output gas composition was analyzed online by a mass spectrometer (Hiden Analytical Limited, QGA Pro v1.6). The mass spectrometer was calibrated separately with a mixture of 867 ppm NO<sub>2</sub> in He and 976 ppm NO in He. For both NO and NO<sub>2</sub>, a response factor was calculated and used to determine the concentration of the detected products, which is 1696 for NO and 313 for NO<sub>2</sub>. Table S.2 shows the NO and NO<sub>2</sub> concentrations (ppm) before calibration, the calibrated concentrations (ppm), as well as the product selectivity for different N<sub>2</sub> and O<sub>2</sub> gas mixtures.

Table S.4 NO and NO<sub>2</sub> concentrations (ppm) before calibration, calibrated concentrations (ppm) and product selectivity. We also checked for N<sub>2</sub>O and N<sub>2</sub>O<sub>4</sub> but their concentrations were below the detection limit.

N <sub>2</sub> /O <sub>2</sub> ratio	NO concentration [a.u.]	Calibrated-NO [ppm]	NO <sub>2</sub> concentration	Calibrated-NO <sub>2</sub> (ppm)	NO selectivity [%]	NO <sub>2</sub> selectivity [%]
9/1	7.61x10 <sup>-8</sup>	1.29x10 <sup>-4</sup>	1.73x10 <sup>-8</sup>	5.41x10 <sup>-6</sup>	95.97	4.03
8/2	8.04x10 <sup>-8</sup>	1.36x10 <sup>-4</sup>	4.26x10 <sup>-8</sup>	1.33x10 <sup>-5</sup>	91.09	8.91
7/3	7.90x10 <sup>-8</sup>	1.34x10 <sup>-4</sup>	6.04x10 <sup>-8</sup>	1.89x10 <sup>-5</sup>	87.63	12.37
6/4	7.61x10 <sup>-8</sup>	1.29x10 <sup>-4</sup>	8.03x10 <sup>-8</sup>	2.51x10 <sup>-5</sup>	83.70	16.30
5/5	7.24x10 <sup>-8</sup>	1.23x10 <sup>-4</sup>	8.43x10 <sup>-8</sup>	2.64x10 <sup>-5</sup>	82.31	17.69
4/6	6.57x10 <sup>-8</sup>	1.11x10 <sup>-4</sup>	8.17x10 <sup>-8</sup>	2.56x10 <sup>-5</sup>	81.33	18.67
3/7	6.20x10 <sup>-8</sup>	1.05x10 <sup>-4</sup>	7.90x10 <sup>-8</sup>	2.47x10 <sup>-5</sup>	80.96	19.04
2/8	5.45x10 <sup>-8</sup>	9.24x10 <sup>-5</sup>	7.03x10 <sup>-8</sup>	2.20x10 <sup>-5</sup>	80.77	19.23
1/9	4.04x10 <sup>-8</sup>	6.85x10 <sup>-5</sup>	4.52x10 <sup>-8</sup>	1.41x10 <sup>-5</sup>	82.89	17.11

### 4.3 Energy measurements

Table S.5 Measured energy cost (EC) with the corresponding error values for different N<sub>2</sub>/O<sub>2</sub> ratios.

N <sub>2</sub> /O <sub>2</sub> ratio	EC	EC-error
9/1	3.99x10 <sup>6</sup>	0.10x10 <sup>6</sup>
8/2	3.62x10 <sup>6</sup>	0.28x10 <sup>6</sup>
7/3	3.64x10 <sup>6</sup>	0.11x10 <sup>6</sup>
6/4	3.90x10 <sup>6</sup>	0.24x10 <sup>6</sup>
5/5	4.09x10 <sup>6</sup>	0.12x10 <sup>6</sup>
4/6	4.66x10 <sup>6</sup>	0.25x10 <sup>6</sup>
3/7	4.95x10 <sup>6</sup>	0.16x10 <sup>6</sup>
2/8	5.88x10 <sup>6</sup>	0.16x10 <sup>6</sup>
1/9	6.78x10 <sup>6</sup>	0.59x10 <sup>6</sup>

## 5. Raw data from the model

Table S.6 Calculated yield of NO and NO<sub>2</sub> and energy consumption (EC) as a function of N<sub>2</sub> fraction in the feed gas, for a gas flow rate of 10 L min<sup>-1</sup>, a pressure of 1.25 bar and a power ranging from 365 to 458 W (slightly varying for different gas composition; see Table S.3).

N <sub>2</sub> [%]	NO [%]	NO <sub>2</sub> [%]	EC [MJ/mol]
10	0.48	0.06	11.44
20	0.76	0.08	7.98
30	1.01	0.10	5.77

40	1.30	0.12	4.49
50	1.44	0.12	3.91
60	1.49	0.11	3.75
70	1.44	0.10	3.63
80	1.35	0.07	3.81
90	1.11	0.04	4.66

Table S.7 Calculated density of  $N_2O$ ,  $N_2O_4$ ,  $NO_3$ ,  $N_2O_5$  and  $N_2O_3$  as a function of  $N_2$  fraction in the feed gas, for a gas flow rate of  $10 \text{ L min}^{-1}$ , a pressure of 1.25 bar and a power ranging from 365 to 458 W (slightly varying for different gas compositions; see Table S.3).

$N_2$ [%]	$N_2O$ [ $\text{cm}^{-3}$ ]	$N_2O_4$ [ $\text{cm}^{-3}$ ]	$NO_3$ [ $\text{cm}^{-3}$ ]	$N_2O_5$ [ $\text{cm}^{-3}$ ]	$N_2O_3$ [ $\text{cm}^{-3}$ ]
10	$6.81 \times 10^{12}$	$1.16 \times 10^5$	$5.22 \times 10^{13}$	$1.02 \times 10^5$	$8.62 \times 10^7$
20	$1.66 \times 10^{13}$	$2.53 \times 10^5$	$8.11 \times 10^{13}$	$2.34 \times 10^5$	$2.04 \times 10^8$
30	$2.81 \times 10^{13}$	$3.76 \times 10^5$	$9.62 \times 10^{13}$	$3.39 \times 10^5$	$3.31 \times 10^8$
40	$4.58 \times 10^{13}$	$5.29 \times 10^5$	$1.10 \times 10^{14}$	$4.59 \times 10^5$	$5.05 \times 10^8$
50	$5.75 \times 10^{13}$	$5.47 \times 10^5$	$1.04 \times 10^{14}$	$4.44 \times 10^5$	$5.68 \times 10^8$
60	$6.54 \times 10^{13}$	$4.86 \times 10^5$	$9.04 \times 10^{13}$	$3.62 \times 10^5$	$5.55 \times 10^8$
70	$6.58 \times 10^{13}$	$3.49 \times 10^5$	$6.78 \times 10^{13}$	$2.30 \times 10^5$	$4.55 \times 10^8$
80	$6.49 \times 10^{13}$	$2.11 \times 10^5$	$4.40 \times 10^{13}$	$1.16 \times 10^5$	$3.31 \times 10^8$
90	$5.37 \times 10^{13}$	$6.86 \times 10^4$	$1.75 \times 10^{13}$	$2.64 \times 10^4$	$1.55 \times 10^8$

## 6. Benchmarking the energy cost of our GAP reactor: Chi parameter

The various plasma sources listed in Table S.6 are all different in structure, geometry and excitation modes, and they potentially have different chemical reaction pathways for  $NO_x$  production. Therefore, Pei et al. proposed a dimensionless parameter ( $\chi$ ) to compare different plasma set-ups<sup>1</sup>:

$$\chi = \frac{\bar{E} \cdot \bar{T}}{\bar{E}_r \cdot \bar{T}_r} \quad (4)$$

Where  $\bar{E}$  and  $\bar{T}$  are the average electric field and average gas temperature of a specific plasma type, and  $\bar{E}_r$  and  $\bar{T}_r$  are reference values chosen to normalize these parameters at 1.43 kV/cm and 1800 K, respectively.

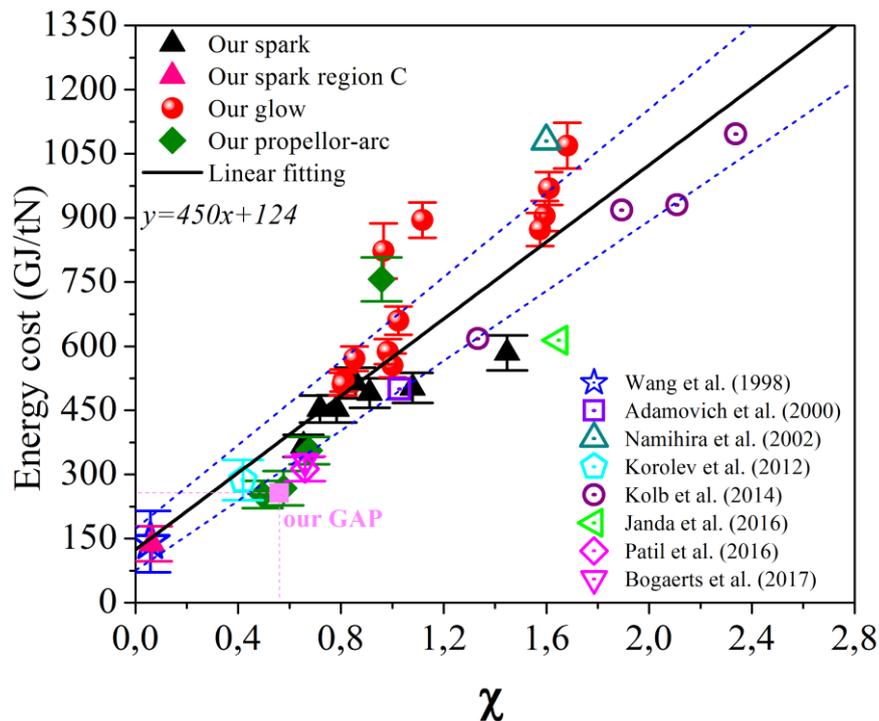


Figure S.3 Energy cost for  $\text{NO}_x$  production as a function of the  $\chi$  parameter, compared to the reported works from literature and the results of Pei et al. using different plasma sources. The figure is adapted from ref.<sup>1</sup> with the permission from the authors. The  $\chi$  parameter of our GAP is plotted in pink (for the conditions described in the section below).

They observed that the energy cost (reported per unit of reactive N, expressed in units of GJ/tN) increases linearly with  $\chi$  for different plasma types evaluated, and thus they concluded that  $\chi$  can give a good indication of the energy cost performance of a specific plasma set-up for  $\text{NO}_x$  production. Based on the calculated gas number density of  $3.02 \times 10^{18} \text{ cm}^{-3}$  and an average reduced electric field of 16 Td, we estimate for our GAP an average electric field of 0.48 kV/cm, while the average gas temperature in the arc should be around 3000 K<sup>15</sup>. This yields a  $\chi$  value of 0.56. The minimum energy cost in GJ/tN in our GAP is 257 GJ/tN. If we would add this data point to the figure in ref.<sup>25</sup> (see pink square on Figure S.3), our EC is in the range of what is predicted by the linear dependency between EC and  $\chi$ .

## 7. Reaction analysis

The net rates for the production or loss of NO and  $\text{NO}_2$ , discussed in the main paper, are plotted as a function of the  $\text{N}_2$  fraction in the feed gas in Figure S.4. As  $\text{NO}_2$  is always formed from NO, the main processes for the formation and loss of  $\text{NO}_2$  are also included in this figure, though formulated as an NO loss instead of an  $\text{NO}_2$  formation process. For the sake of clarity, we have plotted processes N1 and N5 on the right y-axis, which is 10 times larger than the left y-axis, so that the evolution of the rates of the Zeldovich processes (N2 and N3) is clearly visible. The Zeldovich mechanism (N2 and N3) as a function of the  $\text{N}_2$  fraction in the feed is discussed in section 3.4 of the main paper. As seen in Figure S.4, N1 is the dominant NO formation reaction at  $\text{N}_2$  fractions below 60 %. At higher  $\text{N}_2$  fractions, reaction N2 becomes more important, as there is less  $\text{O}_2$  available. NO is rapidly converted

into  $\text{NO}_2$  through N4 (pink curve in Figure S.4). Its rate drops with increasing  $\text{N}_2$  fraction, as this process requires atomic O. Next,  $\text{NO}_2$  is converted back to  $\text{NO}$  through N1 (red curve) and N4 (purple curve), which are the two main loss channels for  $\text{NO}_2$ .

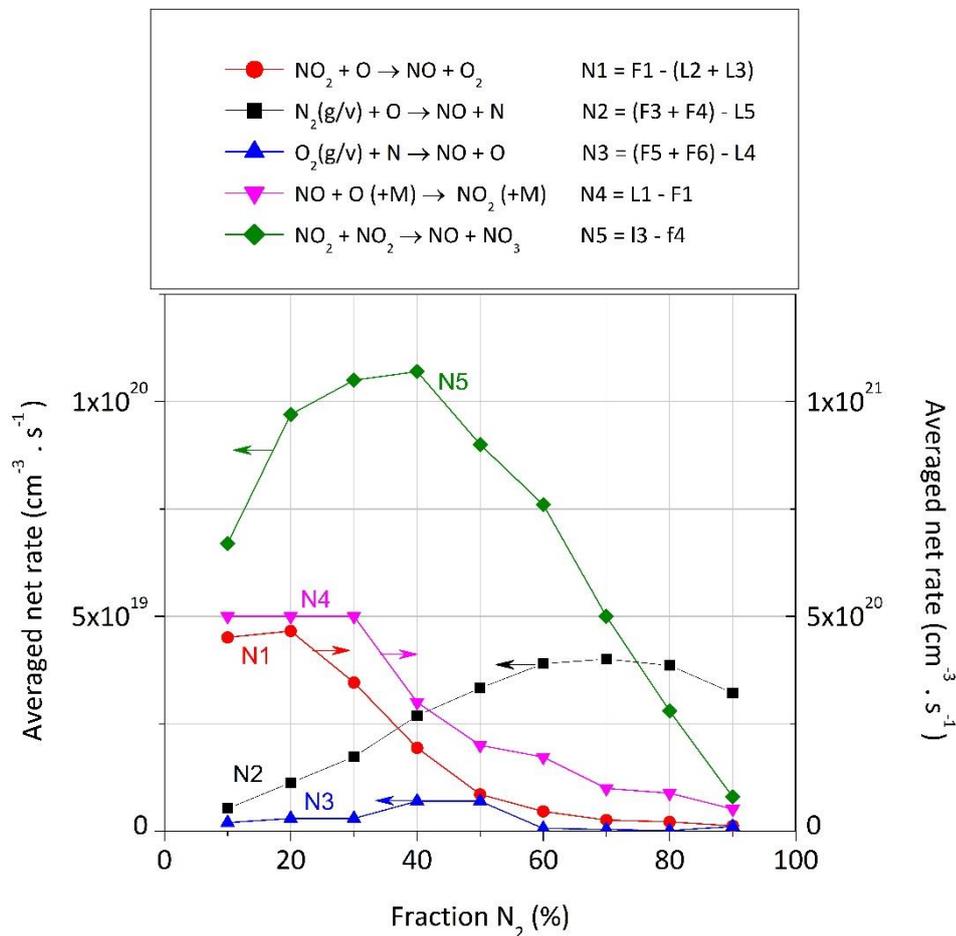


Figure S.4 Net rates of the most important formation and loss process of  $\text{NO}$  (and  $\text{NO}_2$ ) as a function of the  $\text{N}_2$  fraction in the feed gas, at the same condition as in Figure 1 in the main paper.

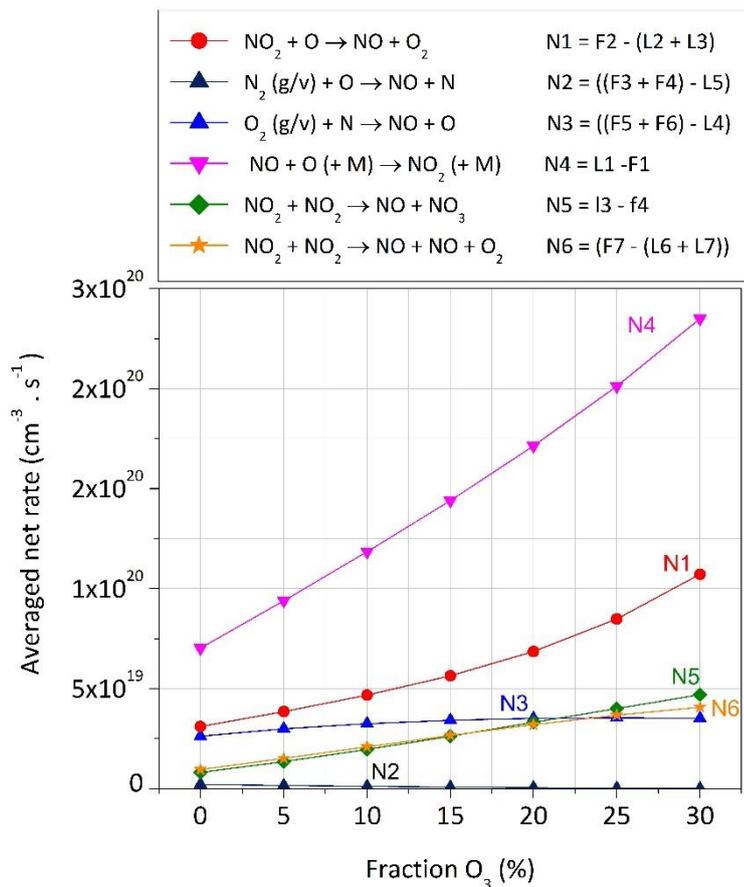


Figure S.5 Net rates of the most important formation and loss processes of NO as a function of the O<sub>3</sub> fraction in the feed gas at a N<sub>2</sub>/O<sub>2</sub> ratio of 80/20, flow rate of 10 L min<sup>-1</sup> and a power of 400 W.

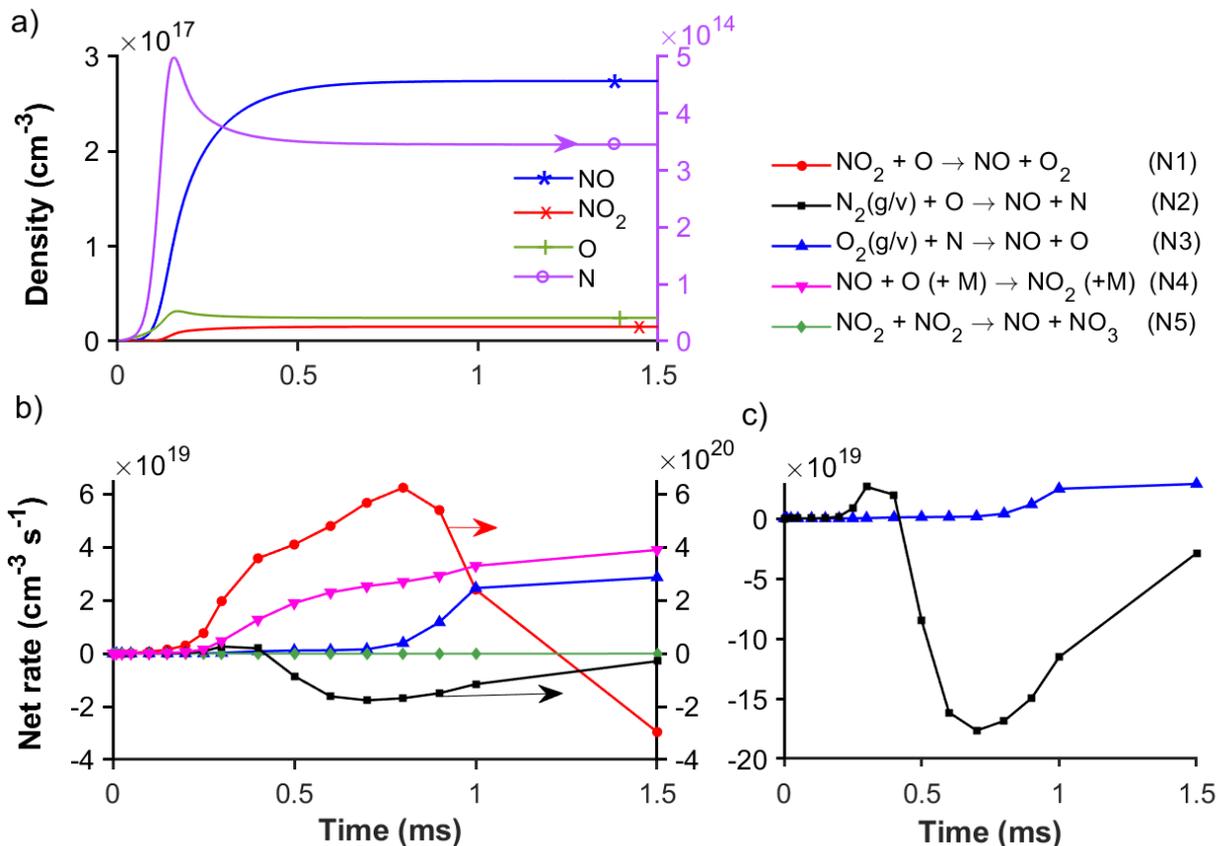


Figure S.6: Calculated number densities of NO, NO<sub>2</sub>, O and N (a), and net rates of the main reactions as function of residence time until steady state (b), for an 80/20 N<sub>2</sub>/O<sub>2</sub> mixture at 1.25 bar, 10 L min<sup>-1</sup> and 415 W. The same figure for the full residence time (15 ms) can be found in Figure S.7. Panel (c) shows reactions N2 and N3 in detail.

The NO, NO<sub>2</sub>, N and O densities reach steady state already in the first 0.5 ms, which can be explained as follows. First, the N atoms are predominantly (99.98 %) formed through electron impact dissociation of N<sub>2</sub>(g/v) (see peak in Figure S.6a: purple curve). The N atoms are partially consumed in the Zeldovich mechanism (Figure S.6b and c: blue curve, N3) with the formation of NO. Similarly, the O atoms are formed through direct electron impact dissociation and collision with electronically excited N<sub>2</sub> molecules (as discussed of the main paper) and partially consumed through the second step of the Zeldovich mechanism (Figure S.6b and c: black curve, N2). Once NO is formed, it is either (1) converted into NO<sub>2</sub> (Figure S.6b: pink curve, N4), or (2) destroyed through the backward reaction of N2. Indeed, the rate of N2 becomes negative around 0.5 ms (see Figure S.6b and c: black curve). In case it had been converted into NO<sub>2</sub> it is partially converted back into NO (Figure S.6b: red curve, N1). Under these conditions the backward reaction of N3 is not promoted, and the net reaction rate is in favor of NO production throughout the entire residence time. On the other hand, the net rate of N2 is in favor of NO production before 0.5 ms, but decreases after 0.5 ms in favor of NO destruction. This limits the NO production.“

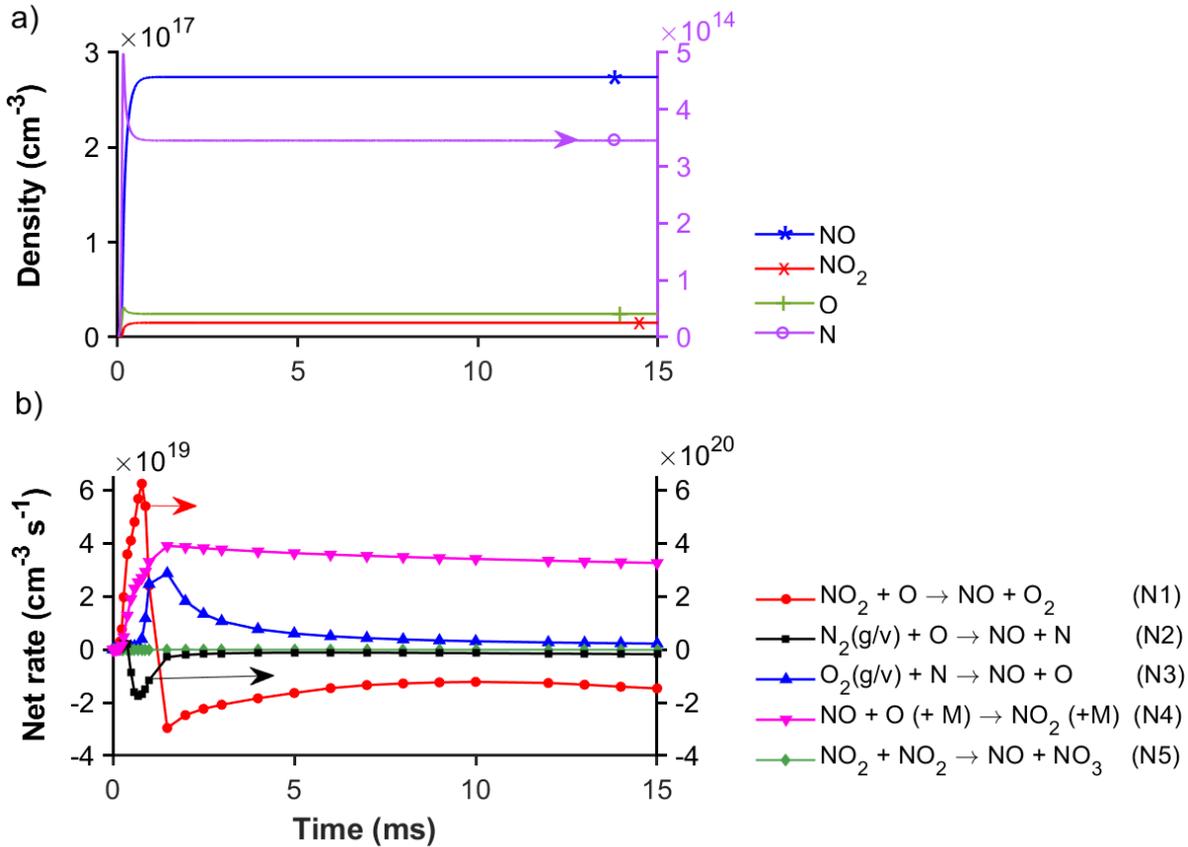


Figure S.7 Calculated number densities of NO, NO<sub>2</sub>, O and N (a), and net rates of the main reactions as function of the residence time (b), for an 80/20 N<sub>2</sub>/O<sub>2</sub> mixture at 1.25 bar, 10 L min<sup>-1</sup> and 415 W.

## 8. VDFs of N<sub>2</sub> and O<sub>2</sub>

In this section we give a more elaborate description and discussion of the VDF of N<sub>2</sub> and O<sub>2</sub> to support our discussion in the main paper.

The chemistry set we developed for this model includes an extensive description of the vibrational kinetics of both N<sub>2</sub> and O<sub>2</sub>. A simple measure of the degree of vibrational excitation is the vibrational temperature, calculated according to:

$$T_v = \frac{1}{m} \sum_{i=1}^m \frac{(E_i - E_{i-1})}{\ln\left(\frac{n_i}{n_{i-1}}\right)} \quad (5)$$

With  $m$  being an integer corresponding to the number of vibrational levels taken into account in the calculation of the vibrational temperature,  $E_i$  is the vibrational energy of the  $i^{\text{th}}$  level and  $n_i$  is the density of the molecule at the  $i^{\text{th}}$  level. The vibrational temperature, based on the 24 vibrational levels of N<sub>2</sub> included in the model, is calculated to be 3325 K. This is slightly higher than the gas temperature in the arc, which is expected to be around 3000 K, based on 2D fluid dynamics modeling<sup>15</sup>, and taken as constant in our model (see section 4 above). The vibrational temperature of O<sub>2</sub> is calculated to be 2632 K, based on the 15 vibrational levels of O<sub>2</sub> taken into account in the model. Hence, this is somewhat lower than the vibrational temperature of N<sub>2</sub>. Indeed, even though the reaction rate

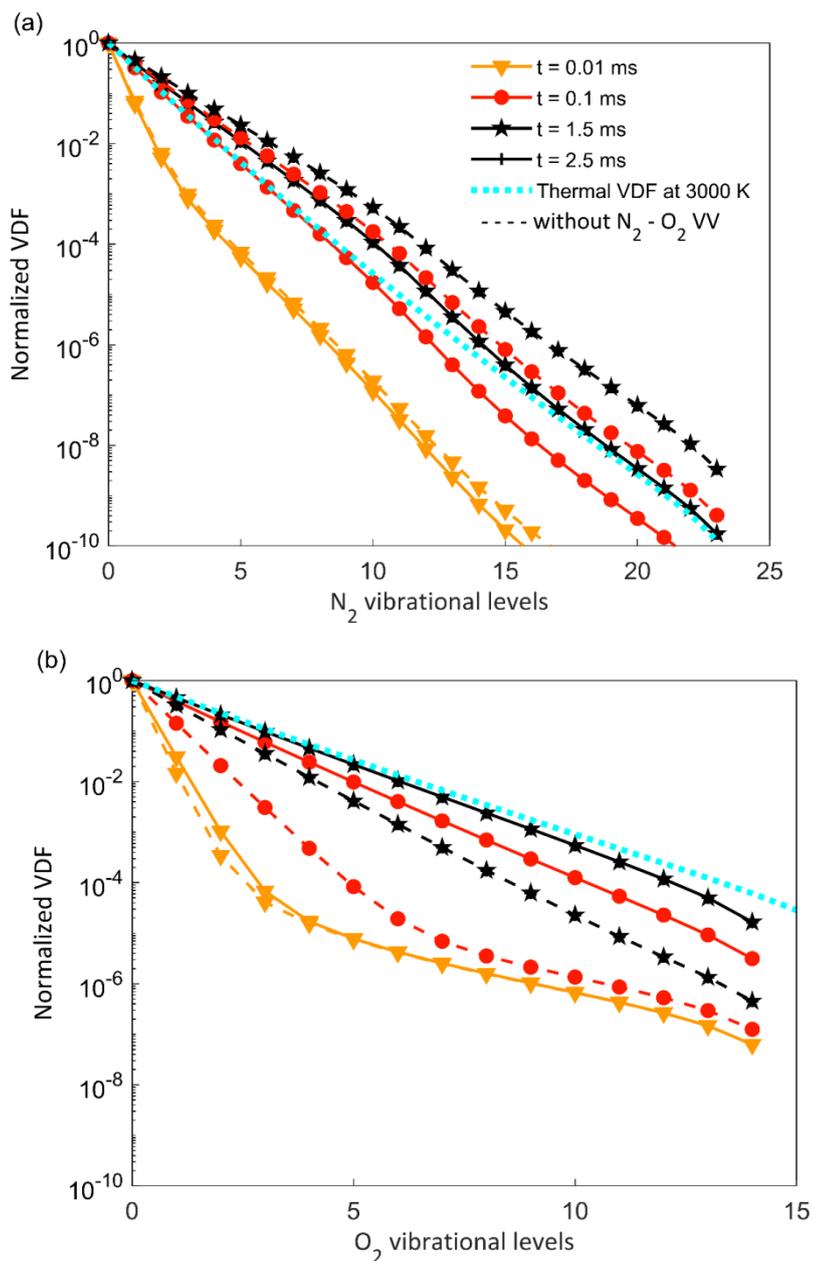


Figure S.8 Normalized vibrational distribution function (VDF) of  $N_2$  (a) and  $O_2$  (b) at different times in the plasma for a 50/50  $N_2/O_2$  plasma, and at the same conditions as in Figure 1. The solid and dashed curves represent the VDFs of a chemistry set that includes and excludes  $N_2-O_2$  VV exchanges, respectively (see next section). The black full lines (representing  $t = 1.5$  and  $2.5$  ms) are on top of one another, as well as the black dashed lines, indicating that the VDFs of  $N_2$  and  $O_2$  reach steady state already after  $1.5$  ms. For comparison, the thermal VDF at  $3000$  K is also plotted as a dotted blue curve.

constants of  $N_2-N_2$  vibrational ladder climbing (by vibrational-vibrational (VV) exchanges) are five times lower than for  $O_2-O_2$  vibrational ladder climbing, the reaction rate constants of the different depopulation mechanisms of the  $O_2$  vibrational levels (i.e., by vibrational-translational (VT) exchanges:  $O_2-O$  VT,  $O_2-N_2$  VT and  $O_2-O_2$  VT) are higher than the rate constants of the same

mechanisms for the  $\text{N}_2$  vibrational levels, resulting in easier depopulation of the  $\text{O}_2$  vibrational levels. In Figure S.8, we plot the vibrational distribution function (VDF), i.e., normalized density of the vibrational levels, of  $\text{N}_2$  (panel a, solid lines) and  $\text{O}_2$  (panel b, solid lines), at different times in the plasma, as well as the thermal distribution of  $\text{N}_2$  and  $\text{O}_2$  at 3000 K (dotted, light blue curves). The VDF of  $\text{N}_2$  is in thermal equilibrium for the majority of the residence time. At short residence time ( $t = 0.01$  ms), the vibrational temperature is much lower than 3000 K, but the population quickly builds up, to a vibrational temperature above 3000 K at 1.5 ms. The VDF of  $\text{O}_2$  shows an overpopulation of the higher vibrational levels at short residence times ( $t = 0.01$  ms), but after 1.5 ms, the VDF also becomes in equilibrium, with a temperature slightly below the gas temperature of 3000 K. Both VDFs reach a quasi-steady state after 1.5 ms. Although the VDFs are thermal, the higher vibrational levels are nevertheless sufficiently populated to facilitate dissociation, as illustrated in Figure 3 and Table 1 in the main paper. Moreover, the vibrational levels in our GAP are more populated than in other set-ups, like a classical GA, where the VDF drops significantly for the higher vibrational levels.<sup>24</sup>

## 9. Chemistry set

The chemistry set used in this model is based on the work done by Wang et al.<sup>24</sup>, but revised and updated. For instance, the set contains a more elaborate description of the vibrational kinetics of N<sub>2</sub> and O<sub>2</sub> (i.e. N<sub>2</sub>–O<sub>2</sub> vibrational-vibrational (VV) exchanges and N<sub>2</sub>–N and O<sub>2</sub>–O vibrational-translational (VT) relaxations, see Table S.13). 24 vibrational levels for N<sub>2</sub> and 15 levels for O<sub>2</sub> were implemented in the model. The species taken into account in the model are listed in Table S.5 above. This includes neutral molecules in the ground state, vibrationally and electronically excited states, various radicals, positive and negative ions, and electrons. Table S.7 lists all electron impact reactions. Most of these reactions are treated by energy-dependent cross sections. Table S.8 lists the neutral-neutral reactions and the corresponding rate-coefficient expressions. For certain reactions, the rate coefficients of the vibrationally excited species are determined according to the Fridman-Macheret model in which the activation energy is lowered by  $\alpha E_v$ , where  $\alpha$  is the vibrational efficiency to lower the activation barrier and  $E_v$  is the vibrational energy. For those reactions, the  $\alpha$  parameter is given in the last column of Table S.8. Tables S.9 to S.11 list the electron-ion recombination, the ion-neutral and the ion-ion reactions and the corresponding rate coefficients, respectively. Table S.12 displays the optical transitions

*Table S.8 Electron impact reactions implemented in the model for atomic and molecular nitrogen and oxygen species as well as NO<sub>x</sub> species. The list includes vibrational excitation and de-excitation, electronic excitation and de-excitation, direct and dissociative ionization, dissociation, as well as direct and dissociative attachment reactions. These reactions are treated by energy-dependent cross sections when the rate coefficient is not specified. When indicated, rate coefficients are expressed in cm<sup>3</sup> s<sup>-1</sup> or cm<sup>6</sup> s<sup>-1</sup> for binary or ternary reactions, respectively.*

Reaction	Rate Coefficient	Ref.	Note
$e^- + N_2 \leftrightarrow e^- + N_2(v)$		26	
$e^- + N_2(v) \leftrightarrow e^- + N_2(v')$		26	
$e^- + N_2(g, v) \rightarrow e^- + N_2(E_x)$		27	a, b, c
$e^- + N_2(E_x) \rightarrow e^- + N_2$		27	b
$e^- + N_2(g, v) \rightarrow 2e^- + N_2^+$		28	a
$e^- + N_2(E_x) \rightarrow 2e^- + N_2^+$		28	b
$e^- + N \rightarrow 2e^- + N^+$		27	
$e^- + N_2(g, v) \rightarrow 2e^- + N^+ + N$		29	a
$e^- + N_2(g, v) \rightarrow e^- + N + N$		27	a, c
$e^- + N_2(E_x) \rightarrow e^- + N + N$		27	b
$e^- + N \rightarrow e^- + N(E_x)$		27	d
$e^- + O_2 \leftrightarrow e^- + O_2(v)$		26	
$e^- + O_2(v) \leftrightarrow e^- + O_2(v')$		30	

$e^- + O_2(g, v) \rightarrow e^- + O_2(E_x)$		27	a, c, e
$e^- + O_2(E_x) \rightarrow e^- + O_2$		27	e
$e^- + O_2(g, v) \rightarrow 2e^- + O_2^+$		28	a, c
$e^- + O_2(E_x) \rightarrow 2e^- + O_2^+$		31	e
$e^- + O \rightarrow 2e^- + O^+$		27	
$e^- + O_2(g, v) \rightarrow 2e^- + O + O^+$		32	a, c
$e^- + O_2(E_x) \rightarrow 2e^- + O + O^+$		32	e
$e^- + O_3 \rightarrow 2e^- + O + O_2^+$		33	
$e^- + O_3 \rightarrow e^- + O^+ + O^- + O$		27	
$e^- + O_2(g, v) \rightarrow e^- + O + O$		27	a
$e^- + O_3 \rightarrow e^- + O_2 + O$		33	
$e^- + O_2(g, v) \rightarrow O + O^-$		27	a, c
$e^- + O_2(g, v) + M \rightarrow O_2^- + M$		34	a, c, f
$e^- + O_3 \rightarrow O^- + O_2$		28	
$e^- + O_3 \rightarrow O + O_2^-$		28	
$e^- + O_3 + M \rightarrow O_3^- + M$	$5 \times 10^{-31}$	35	f
$e^- + O + M \rightarrow O^- + M$	$1 \times 10^{-31}$	36	f
$e^- + NO \rightarrow 2e^- + NO^+$		37	
$e^- + NO_2 \rightarrow 2e^- + NO_2^+$		38	
$e^- + N_2O \rightarrow 2e^- + N_2O^+$		39	
$e^- + N_2O \rightarrow e^- + N_2 + O$		40	
$e^- + N_2O \rightarrow e^- + N_2 + O(1D)$		40	
$e^- + N_2O \rightarrow e^- + NO + N$		40	
$e^- + NO \rightarrow O^- + N$		37	
$e^- + N_2O \rightarrow N_2 + O^-$		39	
$e^- + NO_2 \rightarrow NO_2^-$	$1 \times 10^{-11}$	41	
$e^- + NO_2 \rightarrow O^- + NO$	$1 \times 10^{-11}$	42	
$e^- + NO + M \rightarrow NO^- + M$	$8 \times 10^{-31}$	42	f
$e^- + N_2O + M \rightarrow N_2O^- + M$	$6 \times 10^{-33}$	42	f

<sup>a</sup> For any species indicated with (g, v), g and v stand for its ground and vibrationally excited state, respectively.

<sup>b</sup>  $N_2(E_x)$  represents the electronically excited states:  $N_2(A^3\Sigma_u^+)$ ,  $N_2(B^3\Pi_g)$ ,  $N_2(C^3\Pi_u)$  and  $N_2(a'^1\Sigma_u^-)$ .

<sup>c</sup> The cross sections of the reactions involving excited species on the left hand side are shifted over the difference in the threshold energies.

<sup>d</sup>  $N(E_x)$  represents the electronically excited states of atomic N:  $N(2D)$  and  $N(2P)$ .

<sup>e</sup>  $O_2(E_x)$  represents the electronically excited states:  $O_2(a^1\Delta)$ ,  $O_2(b^1\Sigma^+)$  and a combination of three states, i.e.  $O_2(A^3\Sigma^+, C^3\Delta, c^1\Sigma^-)$  at a threshold energy of 4.5 eV.

<sup>f</sup> M represents any neutral species.

Table S.9 Neutral-neutral reactions included in the model and the corresponding rate coefficient expressions.  $T_g$  is the gas temperature in K. The rate coefficients are expressed in  $\text{cm}^3 \text{s}^{-1}$  or  $\text{cm}^6 \text{s}^{-1}$  for binary or ternary reactions, respectively. For certain reactions, the rate coefficients of the vibrationally excited species are determined according to the Fridman-Macheret model in which the activation energy is lowered by  $\alpha E_v$ , where  $\alpha$  is the vibrational efficiency to lower the activation barrier and  $E_v$  is the vibrational energy. For those reactions, the  $\alpha$  parameter is given in the last column.

Reaction	Rate coefficient	Ref.	Note
$\text{N}_2(\text{g}, \nu) + \text{M} \rightarrow \text{N} + \text{N} + \text{M}$	$8.37 \times 10^{-4} \times \left(\frac{T_g}{298}\right)^{-3.5} \times \exp\left(-\frac{113710}{T_g}\right)$	43	a, b $\alpha = 1$
$\text{N} + \text{N} + \text{M} \rightarrow \text{N}_2 + \text{M}$	$1.38 \times 10^{-33} \times \exp\left(\frac{502.978}{T_g}\right)$	44	b
$\text{N} + \text{N} \rightarrow \text{N}_2^+ + \text{e}^-$	$2.7 \times 10^{-11} \times \exp\left(-\frac{6.74 \times 10^4}{T_g}\right)$	42	
$\text{N} + \text{N} + \text{N} \rightarrow \text{N}_2(\text{A}^3\Sigma_u^+) + \text{N}$	$1.0 \times 10^{-32}$	42	
$\text{N} + \text{N} + \text{N} \rightarrow \text{N}_2(\text{B}^3\Pi_g) + \text{N}$	$1.4 \times 10^{-32}$	42	
$\text{N} + \text{N} + \text{N}_2 \rightarrow \text{N}_2(\text{A}^3\Sigma_u^+) + \text{N}_2$	$1.7 \times 10^{-33}$	42	
$\text{N} + \text{N} + \text{N}_2 \rightarrow \text{N}_2(\text{B}^3\Pi_g) + \text{N}_2$	$2.4 \times 10^{-33}$	42	
$\text{N}(2\text{D}) + \text{M} \rightarrow \text{N} + \text{M}$	$2.4 \times 10^{-14}$	45	b
$\text{N}(2\text{P}) + \text{N} \rightarrow \text{N}(2\text{D}) + \text{N}$	$1.8 \times 10^{-12}$	42	
$\text{N}(2\text{P}) + \text{N}_2 \rightarrow \text{N} + \text{N}_2$	$2.0 \times 10^{-18}$	42	
$\text{N}_2(\text{a}^1\Sigma_u^-) + \text{N} \rightarrow \text{N}_2 + \text{N}$	$2.0 \times 10^{-11}$	46	
$\text{N}_2(\text{a}^1\Sigma_u^-) + \text{N}_2 \rightarrow \text{N}_2 + \text{N}_2$	$3.7 \times 10^{-16}$	46	
$\text{N}_2(\text{a}^1\Sigma_u^-) + \text{N}_2 \rightarrow \text{N}_2(\text{B}^3\Pi_g) + \text{N}_2$	$1.9 \times 10^{-13}$	42	
$\text{N}_2(\text{a}^1\Sigma_u^-) + \text{N}_2(\text{a}^1\Sigma_u^-) \rightarrow \text{N}_2^+ + \text{N}_2 + \text{e}^-$	$5.0 \times 10^{-13}$	46	
$\text{N}_2(\text{a}^1\Sigma_u^-) + \text{N}_2(\text{a}^1\Sigma_u^-) \rightarrow \text{N}_4^+ + \text{e}^-$	$1.0 \times 10^{-11}$	42	
$\text{N}_2(\text{a}^1\Sigma_u^-) + \text{N}_2(\text{A}^3\Sigma_u^+) \rightarrow \text{N}_4^+ + \text{e}^-$	$4.0 \times 10^{-12}$	42	
$\text{N}_2(\text{A}^3\Sigma_u^+) + \text{N} \rightarrow \text{N}_2 + \text{N}(2\text{P})$	$4.0 \times 10^{-11} \times \left(\frac{300}{T_g}\right)^{0.667}$	42	
$\text{N}_2(\text{A}^3\Sigma_u^+) + \text{N} \rightarrow \text{N}_2 + \text{N}$	$2.0 \times 10^{-12}$	42	
$\text{N}_2(\text{A}^3\Sigma_u^+) + \text{N}_2 \rightarrow \text{N}_2 + \text{N}_2$	$3.0 \times 10^{-16}$	42	

$N_2(A^3\Sigma_u^+) + N_2(a^1\Sigma_u^-) \rightarrow N_2^+ + N_2 + e^-$	$1.0 \times 10^{-12}$	46	
$N_2(A^3\Sigma_u^+) + N_2(A^3\Sigma_u^+) \rightarrow N_2 + N_2(A^3\Sigma_u^+)$	$2.0 \times 10^{-12}$	46	
$N_2(A^3\Sigma_u^+) + N_2(A^3\Sigma_u^+) \rightarrow N_2 + N_2(B^3\Pi_g)$	$3.0 \times 10^{-10}$	42	
$N_2(A^3\Sigma_u^+) + N_2(A^3\Sigma_u^+) \rightarrow N_2 + N_2(C^3\Pi_u)$	$1.5 \times 10^{-10}$	42	
$N_2(B^3\Pi_g) + N_2 \rightarrow N_2 + N_2$	$2.0 \times 10^{-12}$	42	
$N_2(B^3\Pi_g) + N_2 \rightarrow N_2(A^3\Sigma_u^+) + N_2$	$3 \times 10^{-11}$	42	
$N_2(C^3\Pi_u) + N_2 \rightarrow N_2 + (a^1\Sigma_u^-)$	$1.0 \times 10^{-11}$	42	
$O_2(g, v) + M \rightarrow O + O + M$	$\left(\frac{3.0 \times 10^{-6}}{T_g}\right) \times \exp\left(\frac{-59380}{T_g}\right)$		a $\alpha = 1$
$O + O + M \rightarrow O_2 + M$	$5.21 \times 10^{-35} \times \exp\left(\frac{900}{T_g}\right)$	47	b
$O + O_3 \rightarrow O_2 + O_2$	$8.0 \times 10^{-12} \times \exp\left(-\frac{2056}{T_g}\right)$	48	
$O + O_2(g, v) + M \rightarrow O_3 + M$	$1.34 \times 10^{-34} \times \left(\frac{T_g}{298}\right)^{-1.0}$	49	a, b
$O_3 + M \rightarrow O_2 + O + M$	$7.16 \times 10^{-10} \times \exp\left(-\frac{98120}{R_g T_g}\right)$	50	b, c
$O + O_2(E_x) + M \rightarrow O_3 + M$	$1.34 \times 10^{-34} \times \left(\frac{T_g}{298}\right)^{-1.0}$	49	b, d, e
$O + O_3 \rightarrow O_2 + O_2(a^1\Delta)$	$2.0 \times 10^{-11} \times \exp\left(-\frac{2280}{T_g}\right)$	42	
$O_2(a^1\Delta) + O \rightarrow O_2 + O$	$7.0 \times 10^{-16}$	42	
$O_2(a^1\Delta) + O_2 \rightarrow O_2 + O_2$	$3.8 \times 10^{-18} \times \exp\left(-\frac{205}{T_g}\right)$	42	
$O_2(b^1\Sigma^+) + O \rightarrow O_2(a^1\Delta) + O$	$8.1 \times 10^{-14}$	42	
$O_2(b^1\Sigma^+) + O \rightarrow O_2 + O(1D)$	$3.4 \times 10^{-11} \times \left(\frac{T_g}{300}\right)^{-0.1} \times \exp\left(-\frac{4200}{T_g}\right)$	42	
$O_2(b^1\Sigma^+) + O_2 \rightarrow O_2 + O_2(a^1\Delta)$	$4.3 \times 10^{-22} \times (T_g)^{2.4} \times \exp\left(-\frac{281}{T_g}\right)$	42	
$O_2(b^1\Sigma^+) + O_3 \rightarrow O_2 + O_2 + O$	$2.2 \times 10^{-11}$	42	
$O_2(a^1\Delta) + O_3 \rightarrow O_2 + O_2 + O(1D)$	$5.2 \times 10^{-11} \times \exp\left(-\frac{2840}{T_g}\right)$	42	
$O_2(a^1\Delta) + O_2(a^1\Delta) \rightarrow O_2 + O_2(b^1\Sigma^+)$	$7.0 \times 10^{-28} \times (T_g)^{3.8} \times \exp\left(\frac{700}{T_g}\right)$	42	

$O(1D) + O \rightarrow O + O$	$8.0 \times 10^{-12}$	42	
$O(1D) + O_2 \rightarrow O + O_2$	$6.4 \times 10^{-12} \times \exp\left(-\frac{67}{T_g}\right)$	42	
$O(1S) + O \rightarrow O(1D) + O(1D)$	$5.0 \times 10^{-11} \times \exp\left(-\frac{300}{T_g}\right)$	42	
$O(1S) + O_2 \rightarrow O + O_2$	$1.3 \times 10^{-12} \times \exp\left(-\frac{850}{T_g}\right)$	42	
$O(1S) + O_2 \rightarrow O + O + O$	$3.0 \times 10^{-12}$	42	
$O(1S) + O_2(a^1\Delta) \rightarrow O + O + O$	$3.2 \times 10^{-11}$	42	
$O(1S) + O_2(a^1\Delta) \rightarrow O(1D) + O_2(b^1\Sigma^+)$	$2.9 \times 10^{-11}$	42	
$O(1S) + O_2 \rightarrow O + O_2(A^3\Sigma^+, C^3\Delta, c^1\Sigma^-)$	$3.0 \times 10^{-12} \times \exp\left(-\frac{850}{T_g}\right)$	42	f
$N + O_2(g, v) \rightarrow O + NO$	$2.36 \times 10^{-11} \times \exp\left(-\frac{44230}{R_g T_g}\right)$	51	a, c $\alpha = 0.24$
$O + N_2(g, v) \rightarrow N + NO$	$3.01 \times 10^{-10} \times \exp\left(-\frac{318000}{R_g T_g}\right)$	52	a, c $\alpha = 1$
$O_3 + N \rightarrow NO + O_2$	$5.0 \times 10^{-12} \times \exp\left(-\frac{650}{T_g}\right)$	48	
$O_3 + NO \rightarrow O_2 + NO_2$	$2.5 \times 10^{-13} \times \exp\left(-\frac{765}{T_g}\right)$	42	
$O_3 + NO_2 \rightarrow O_2 + NO_3$	$1.2 \times 10^{-13} \times \exp\left(-\frac{2450}{T_g}\right)$	41	
$NO_3 + O_3 \rightarrow NO_2 + O_2 + O_2$	$1.0 \times 10^{-17}$	53	
$N + NO \rightarrow O + N_2$	$1.66 \times 10^{-11}$	54	
$N + NO_2 \rightarrow O + O + N_2$	$9.1 \times 10^{-13}$	42	
$N + NO_2 \rightarrow O + N_2O$	$3.0 \times 10^{-12}$	42	
$N + NO_2 \rightarrow N_2 + O_2$	$7.0 \times 10^{-13}$	42	
$N + NO_2 \rightarrow NO + NO$	$2.3 \times 10^{-12}$	42	
$O + NO \rightarrow N + O_2$	$7.5 \times 10^{-12} \times \left(\frac{T_g}{300}\right) \times \exp\left(-\frac{19500}{T_g}\right)$	42	
$O + NO_2 \rightarrow NO + O_2$	$9.05 \times 10^{-12} \times \left(\frac{T_g}{298}\right)^{-0.52}$	55	
$O + N_2O \rightarrow NO + NO$	$1.5 \times 10^{-10} \times \exp\left(-\frac{14090}{T_g}\right)$	42	
$O + N_2O \rightarrow N_2 + O_2$	$8.3 \times 10^{-12} \times \exp\left(-\frac{14000}{T_g}\right)$	42	
$O + NO_3 \rightarrow O_2 + N_2$	$1.0 \times 10^{-11}$	42	

$\text{NO} + \text{NO} \rightarrow \text{N} + \text{NO}_2$	$3.3 \times 10^{-16} \times \left(\frac{300}{T_g}\right)^{0.5} \times \exp\left(-\frac{39200}{T_g}\right)$	42	
$\text{NO} + \text{NO} \rightarrow \text{O} + \text{N}_2\text{O}$	$2.2 \times 10^{-12} \times \exp\left(-\frac{32100}{T_g}\right)$	42	
$\text{NO} + \text{NO} \rightarrow \text{N}_2 + \text{O}_2$	$5.1 \times 10^{-13} \times \exp\left(-\frac{33660}{T_g}\right)$	42	
$\text{NO} + \text{N}_2\text{O} \rightarrow \text{N}_2 + \text{NO}_2$	$4.6 \times 10^{-10} \times \exp\left(-\frac{25170}{T_g}\right)$	42	
$\text{NO} + \text{NO}_3 \rightarrow \text{NO}_2 + \text{NO}_2$	$1.7 \times 10^{-11}$	42	
$\text{NO}_2 + \text{NO}_2 \rightarrow \text{NO} + \text{NO}_3$	$4.5 \times 10^{-10} \times \exp\left(-\frac{18500}{T_g}\right)$	42	
$\text{NO}_2 + \text{NO}_2 \rightarrow \text{NO} + \text{NO} + \text{O}_2$	$3.3 \times 10^{-12} \times \exp\left(-\frac{13500}{T_g}\right)$	42	
$\text{NO}_2 + \text{NO}_3 \rightarrow \text{NO} + \text{NO}_2 + \text{O}_2$	$2.3 \times 10^{-13} \times \exp\left(-\frac{1600}{T_g}\right)$	42	
$\text{NO}_3 + \text{NO}_3 \rightarrow \text{O}_2 + \text{NO}_2 + \text{NO}_2$	$4.3 \times 10^{-12} \times \exp\left(-\frac{3850}{T_g}\right)$	42	
$\text{NO} + \text{O}_2(\text{g}, \text{v}) \rightarrow \text{O} + \text{NO}_2$	$2.8 \times 10^{-12} \times \exp\left(-\frac{23400}{T_g}\right)$	42	a $\alpha = 1$
$\text{NO} + \text{NO} + \text{O}_2(\text{g}, \text{v}) \rightarrow \text{NO}_2 + \text{NO}_2$	$3.3 \times 10^{-39} \times \exp\left(-\frac{4410}{R_g T_g}\right)$	56	a, c $\alpha = 0.2$
$\text{NO}_2 + \text{O}_2(\text{g}, \text{v}) \rightarrow \text{NO} + \text{O}_3$	$2.8 \times 10^{-12} \times \exp\left(-\frac{25400}{T_g}\right)$	42	a $\alpha = 0.2$
$\text{NO}_3 + \text{O}_2(\text{g}, \text{v}) \rightarrow \text{O}_3 + \text{NO}_2$	$1.5 \times 10^{-12} \times \exp\left(-\frac{15020}{T_g}\right)$	42	a $\alpha = 0.8$
$\text{NO} + \text{O} \rightarrow \text{NO}_2$	$3.01 \times 10^{-11} \times \left(\frac{T_g}{300}\right)^{-0.75}$	57	
$\text{NO}_2 + \text{NO} + \text{M} \rightarrow \text{N}_2\text{O}_3 + \text{M}$	$3.09 \times 10^{-34} \times \left(\frac{T_g}{300}\right)^{-7.70}$	48	b
$\text{NO}_2 + \text{NO}_2 + \text{M} \rightarrow \text{N}_2\text{O}_4 + \text{M}$	$1.4 \times 10^{-33} \times \left(\frac{T_g}{300}\right)^{-3.8}$	48	b
$\text{NO}_2 + \text{NO}_3 + \text{M} \rightarrow \text{N}_2\text{O}_5 + \text{M}$	$3.7 \times 10^{-30} \times \left(\frac{300}{T_g}\right)^{4.10}$	56	b
$\text{N} + \text{O} + \text{M} \rightarrow \text{NO} + \text{M}$	$1.0 \times 10^{-32} \times \left(\frac{300}{T_g}\right)^{0.5}$	42	b
$\text{N}_2(\text{g}, \text{v}) + \text{O} + \text{M} \rightarrow \text{N}_2\text{O} + \text{M}$	$3.9 \times 10^{-35} \times \exp\left(-\frac{10400}{T_g}\right)$	42	b
$\text{N}_2\text{O} + \text{M} \rightarrow \text{N}_2 + \text{O} + \text{M}$	$1.20 \times 10^{-9} \times \exp\left(-\frac{240000}{R_g T_g}\right)$	42	b, c

$\text{NO}_2 + \text{M} \rightarrow \text{NO} + \text{O} + \text{M}$	$9.4 \times 10^{-5} \times \left(\frac{T_g}{298}\right)^{-2.66} \times \exp\left(-\frac{311000}{R_g T_g}\right)$	57	b, c
$\text{NO}_3 + \text{M} \rightarrow \text{NO} + \text{O}_2 + \text{M}$	$2.51 \times 10^{-14} \times \exp\left(-\frac{10230}{R_g T_g}\right)$	58	b, c
$\text{NO} + \text{M} \rightarrow \text{N} + \text{O} + \text{M}$	$8.7 \times 10^{-9} \times \exp\left(-\frac{75994}{T_g}\right)$	42	b
$\text{N}_2\text{O}_3 + \text{M} \rightarrow \text{NO} + \text{NO}_2 + \text{M}$	$1.91 \times 10^{-7} \times \left(\frac{T_g}{298}\right)^{-8.7} \times \exp\left(-\frac{40570}{R_g T_g}\right)$	48	b, c
$\text{N}_2\text{O}_4 + \text{M} \rightarrow \text{NO}_2 + \text{NO}_3 + \text{M}$	$1.3 \times 10^{-5} \times \left(\frac{T_g}{298}\right)^{-3.8} \times \exp\left(-\frac{53210}{R_g T_g}\right)$	48	b, c
$\text{N}_2\text{O}_5 + \text{M} \rightarrow \text{NO}_2 + \text{NO}_3 + \text{M}$	$2.1 \times 10^{-11} \times \left(\frac{300}{T_g}\right)^{-3.5} \times \exp\left(-\frac{91460}{R_g T_g}\right)$	42	b, c
$\text{NO} + \text{O}_2(\text{g}, \nu) + \text{M} \rightarrow \text{NO}_3 + \text{M}$	$5.65 \times 10^{-41} \times \exp\left(-\frac{1750}{R_g T_g}\right)$	59	a, b, c
$\text{NO} + \text{O}_2(\text{E}_x) + \text{M} \rightarrow \text{NO}_3 + \text{M}$	$5.65 \times 10^{-41} \times \exp\left(-\frac{1750}{R_g T_g}\right)$	59	b, d
$\text{N} + \text{N} + \text{NO} \rightarrow \text{N}_2(\text{A}^3\Sigma_u^+) + \text{NO}$	$1.7 \times 10^{-33}$	42	
$\text{N} + \text{N} + \text{NO} \rightarrow \text{N}_2(\text{B}^3\Pi_g) + \text{NO}$	$2.4 \times 10^{-33}$	42	
$\text{N} + \text{N} + \text{O} \rightarrow \text{N}_2(\text{A}^3\Sigma_u^+) + \text{O}$	$1.0 \times 10^{-32}$	42	
$\text{N} + \text{N} + \text{O} \rightarrow \text{N}_2(\text{B}^3\Pi_g) + \text{O}$	$1.4 \times 10^{-32}$	42	
$\text{N} + \text{N} + \text{O}_2 \rightarrow \text{N}_2(\text{A}^3\Sigma_u^+) + \text{O}_2$	$1.7 \times 10^{-33}$	42	
$\text{N} + \text{N} + \text{O}_2 \rightarrow \text{N}_2(\text{B}^3\Pi_g) + \text{O}_2$	$2.4 \times 10^{-33}$	42	
$\text{N}(2\text{D}) + \text{N}_2\text{O} \rightarrow \text{NO} + \text{N}_2$	$3.5 \times 10^{-12}$	42	
$\text{N}(2\text{D}) + \text{NO} \rightarrow \text{N}_2 + \text{O}$	$1.8 \times 10^{-10}$	42	
$\text{N}(2\text{D}) + \text{O} \rightarrow \text{N} + \text{O}(1\text{D})$	$4.0 \times 10^{-13}$	42	
$\text{N}(2\text{D}) + \text{O}_2(\text{g}, \nu) \rightarrow \text{NO} + \text{O}$	$5.2 \times 10^{-12}$	42	a
$\text{N}(2\text{P}) + \text{NO} \rightarrow \text{N}_2(\text{A}^3\Sigma_u^+) + \text{O}$	$3.0 \times 10^{-11}$	42	
$\text{N}(2\text{P}) + \text{O} \rightarrow \text{N} + \text{O}$	$1.0 \times 10^{-12}$	42	
$\text{N}(2\text{P}) + \text{O}_2(\text{g}, \nu) \rightarrow \text{NO} + \text{O}$	$2.6 \times 10^{-15}$	42	a
$\text{N}_2(\text{a}^1\Sigma_u^-) + \text{NO} \rightarrow \text{N}_2 + \text{N} + \text{O}$	$3.6 \times 10^{-10}$	42	
$\text{N}_2(\text{a}^1\Sigma_u^-) + \text{O} \rightarrow \text{NO} + \text{N}$	$3.0 \times 10^{-10}$	52	
$\text{N}_2(\text{a}^1\Sigma_u^-) + \text{O}_2(\text{g}, \nu) \rightarrow \text{N}_2 + \text{O} + \text{O}$	$2.8 \times 10^{-11}$	42	a
$\text{N}_2(\text{A}^3\Sigma_u^+) + \text{N}_2\text{O} \rightarrow \text{N}_2 + \text{N} + \text{NO}$	$1.0 \times 10^{-11}$	42	

$N_2(A^3\Sigma_u^+) + NO \rightarrow N_2 + NO$	$6.9 \times 10^{-11}$	42	
$N_2(A^3\Sigma_u^+) + NO_2 \rightarrow N_2 + O + NO$	$1.0 \times 10^{-12}$	42	
$N_2(A^3\Sigma_u^+) + O \rightarrow N_2 + O(1S)$	$2.1 \times 10^{-11}$	42	
$N_2(A^3\Sigma_u^+) + O \rightarrow NO + N(2D)$	$7.0 \times 10^{-12}$	42	
$N_2(A^3\Sigma_u^+) + O_2(g, v) \rightarrow N_2 + O + O$	$2.0 \times 10^{-12} \times \left(\frac{T_g}{300}\right)^{0.55}$	42	a
$N_2(A^3\Sigma_u^+) + O_2 \rightarrow N_2 + O_2(a^1\Delta)$	$2.0 \times 10^{-13} \times \left(\frac{T_g}{300}\right)^{0.55}$	42	
$N_2(A^3\Sigma_u^+) + O_2 \rightarrow N_2 + O_2$	$2.54 \times 10^{-12}$	42	
$N_2(A^3\Sigma_u^+) + O_2(g, v) \rightarrow N_2O + O$	$2.0 \times 10^{-14} \times \left(\frac{T_g}{300}\right)^{0.55}$	42	a
$N_2(B^3\Pi_g) + N_2O \rightarrow N_2 + N + NO$	$0.58 \times 10^{-10}$	60	
$N_2(B^3\Pi_g) + N_2O \rightarrow N_2 + N_2 + O$	$0.58 \times 10^{-10}$	60	
$N_2(B^3\Pi_g) + O \rightarrow NO + N$	$3.0 \times 10^{-10}$	52	
$N_2(C^3\Pi_u) + O \rightarrow NO + N$	$3.0 \times 10^{-10}$	52	
$N_2(C^3\Pi_u) + O_2(g, v) \rightarrow N_2 + O + O$	$3.0 \times 10^{-10}$	42	a
$NO + O_2(E_x) \rightarrow O + NO_2$	$2.8 \times 10^{-12} \times \exp\left(-\frac{23400}{T_g}\right)$	42	d, g
$NO_3 + O_2(E_x) \rightarrow O_3 + NO_2$	$1.5 \times 10^{-12} \times \exp\left(-\frac{15020}{T_g}\right)$	42	d, h
$O(1D) + N_2 \rightarrow N_2 + O$	$2.3 \times 10^{-11}$	42	
$O(1S) + N \rightarrow O + N$	$1.0 \times 10^{-12}$	42	
$O(1S) + N_2(g, v) \rightarrow O + N_2(g, v)$	$1.0 \times 10^{-17}$	42	
$O_2(a^1\Delta) + N \rightarrow NO + O$	$2.0 \times 10^{-14} \times \exp\left(-\frac{600}{T_g}\right)$	42	
$O_2(a^1\Delta) + N_2(g, v) \rightarrow O_2 + N_2(g, v)$	$3.0 \times 10^{-21}$	42	
$O_2(a^1\Delta) + NO \rightarrow O_2 + NO$	$2.5 \times 10^{-11}$	42	
$O_2(b^1\Sigma^+) + N_2 \rightarrow O_2(a^1\Delta) + N_2$	$1.7 \times 10^{-15} \times \left(\frac{T_g}{300}\right)^{1.0}$	42	
$N_2(B^3\Pi_g) + NO \rightarrow N_2(A^3\Sigma_u^+) + NO$	$2.4 \times 10^{-10}$	42	
$N_2(B^3\Pi_g) + O_2(g, v) \rightarrow N_2 + O + O$	$3.0 \times 10^{-10}$	42	a

<sup>a</sup> For any species indicated with (g, v), g and v stand for its ground and vibrationally excited state, respectively.

<sup>b</sup> M represents any neutral species.

<sup>c</sup>  $R_g = 8.3144598 \text{ J} \cdot \text{K}^{-1} \cdot \text{mol}^{-1}$  is the universal gas constant.

<sup>d</sup>  $O_2(E_x)$  represents the two electronically excited states:  $O_2(a^1\Delta)$  and  $O_2(b^1\Sigma^+)$ .

<sup>e</sup> The rate coefficient is assumed to be equal to the rate of  $O + O_2 + M \rightarrow O_3 + M$ .

<sup>f</sup>  $O_2(A^3\Sigma^+, C^3\Delta, c^1\Sigma^-)$  is a combination of three electronic excited states at a threshold energy of 4.5 eV.

<sup>g</sup> The rate coefficient is assumed to be equal to the rate of  $NO + O_2 \rightarrow O + NO_2$ .

<sup>h</sup> The rate coefficient is assumed to be equal to the rate of  $\text{NO}_3 + \text{O}_2 \rightarrow \text{O}_3 + \text{NO}_2$ .

Table S.10 Electron-ion recombination reactions included in the model and the corresponding rate coefficient expressions.  $T_e$  is the electron temperature in K and  $T_g$  is the gas temperature in K. The rate coefficients are expressed in  $\text{cm}^3 \text{s}^{-1}$  or  $\text{cm}^6 \text{s}^{-1}$  for binary or ternary reactions, respectively.

Reaction	Rate coefficient	Ref.	Note
$e^- + \text{N}_2^+ \rightarrow \text{N} + \text{N}(\text{g}, E_x)$	$R \times 1.8 \times 10^{-7} \times \left(\frac{300}{T_e}\right)^{0.39}$	42	a
$e^- + \text{N}_3^+ \rightarrow \text{N}_2 + \text{N}$	$2 \times 10^{-7} \times \left(\frac{300}{T_e}\right)^{0.5}$	61	
$e^- + \text{N}_3^+ \rightarrow \text{N}_2(E_x) + \text{N}$	$6.91 \times 10^{-8} \times \left(\frac{T_e}{11604.5}\right)^{-0.5}$	61	c
$e^- + \text{N}_4^+ \rightarrow \text{N}_2 + \text{N}_2$	$2.3 \times 10^{-6} \times \left(\frac{300}{T_e}\right)^{0.53}$	42	
$e^- + \text{N}_4^+ \rightarrow \text{N}_2 + \text{N} + \text{N}$	$3.13 \times 10^{-7} \times \left(\frac{T_e}{11604.5}\right)^{-0.41}$	61	
$e^- + \text{N}^+ + e^- \rightarrow e^- + \text{N}$	$7 \times 10^{-20} \times \left(\frac{300}{T_e}\right)^{4.5}$	61	
$e^- + \text{N}^+ + \text{M} \rightarrow \text{N} + \text{M}$	$6 \times 10^{-27} \times \left(\frac{300}{T_e}\right)^{1.5}$	62	b
$e^- + \text{N}_2^+ + e^- \rightarrow e^- + \text{N}_2$	$1 \times 10^{-19} \times \left(\frac{T_e}{300}\right)^{-4.5}$	61	
$e^- + \text{N}_2^+ + \text{M} \rightarrow \text{N}_2 + \text{M}$	$2.49 \times 10^{-29} \times \left(\frac{T_e}{11604.5}\right)^{-1.5}$	61	b
$e^- + \text{O}^+ + \text{O}_2 \rightarrow \text{O} + \text{O}_2$	$6 \times 10^{-27} \times \left(\frac{300}{T_e}\right)^{1.5}$	62	
$e^- + \text{O}^+ + e^- \rightarrow e^- + \text{O}$	$7 \cdot 10^{-20} \cdot \left(\frac{300}{T_e}\right)^{4.5}$	42	
$e^- + \text{O}_2^+ + \text{M} \rightarrow \text{O}_2 + \text{M}$	$1 \times 10^{-26}$	36	b
$e^- + \text{O}_2^+ + e^- \rightarrow e^- + \text{O}_2$	$1 \times 10^{-19} \times \left(\frac{T_e}{300}\right)^{-4.5}$	62	
$e^- + \text{O}_2^+ \rightarrow \text{O} + \text{O}$	$6.46 \times 10^{-5} \times T_e^{-0.5} \times T_g^{-0.5}$	63	
$e^- + \text{O}_2^+ \rightarrow \text{O} + \text{O}(1D)$	$1.08 \times 10^{-7} \left(\frac{T_e}{300}\right)^{-0.7}$	42	
$e^- + \text{O}_2^+ \rightarrow \text{O} + \text{O}(1S)$	$0.14 \times 10^{-7} \left(\frac{T_e}{300}\right)^{-0.7}$	42	
$e^- + \text{O}_4^+ \rightarrow \text{O}_2 + \text{O}_2$	$1.4 \times 10^{-6} \times \left(\frac{300}{T_e}\right)^{0.5}$	42	
$e^- + \text{NO}^+ + e^- \rightarrow e^- + \text{NO}$	$1.0 \times 10^{-19} \left(\frac{T_e}{300}\right)^{-4.5}$	62	
$e^- + \text{NO}^+ + \text{M} \rightarrow \text{NO} + \text{M}$	$2.49 \times 10^{-29} \times \left(\frac{T_e}{11604.5}\right)^{-1.5}$	61	b

$e^- + NO^+ \rightarrow O + N(g, E_x)$	$R \times 4.2 \times 10^{-7} \times \left(\frac{300}{T_e}\right)^{0.85}$	42	d
$e^- + N_2O^+ \rightarrow N_2 + O$	$2.0 \times 10^{-7} \times \left(\frac{300}{T_e}\right)^{0.5}$	42	
$e^- + NO_2^+ \rightarrow NO + O$	$2.0 \times 10^{-7} \times \left(\frac{300}{T_e}\right)^{0.5}$	42	
$e^- + O_2^+ N_2 \rightarrow O_2 + N_2$	$1.3 \times 10^{-6} \times \left(\frac{300}{T_e}\right)^{0.5}$	42	

<sup>a</sup> In  $N(g, E_x)$ , g stands for the ground state of atomic N and  $E_x$  represents two of its electronically excited states: N(2D) and N(2P); R is equal to 0.5, 0.45 and 0.05 for N, N(2D) and N(2P), respectively.

<sup>b</sup> M represents any neutral species.

<sup>c</sup>  $N_2(E_x)$  represents  $N_2(A^3\Sigma_u^+)$  and  $N_2(B^3\Pi_g)$ .

<sup>d</sup> In  $N(g, E_x)$ , g stands for the ground state of atomic N and  $E_x$  represents the electronic excited state N(2D); R is equal to 0.2 and 0.8 for N and N(2D), respectively.

*Table S.11 Ion-neutral reactions included in the model and the corresponding rate coefficient expressions.  $T_g$  is the gas temperature in K. For certain reactions,  $T_{ion}$  is the effective temperature of the reacting ion in K [26]. The rate coefficients are expressed in  $cm^3 s^{-1}$  or  $cm^6 s^{-1}$  for binary or ternary reactions, respectively.*

Reaction	Rate coefficient	Ref.	Note
$N_2^+ + N \rightarrow N^+ + N_2$	$7.2 \times 10^{-13} \times \left(\frac{T_{ion}}{300}\right)$	42	
$N_2^+ + N + N_2 \rightarrow N_3^+ + N_2$	$9.0 \times 10^{-30} \times \left(\frac{400}{T_{ion}}\right)$	42	
$N_4^+ + N_2 \rightarrow N_2^+ + N_2 + N_2$	$2.1 \times 10^{-16} \times \left(\frac{T_{ion}}{121}\right)$	42	
$N^+ + N_2 + N_2 \rightarrow N_3^+ + N_2$	$1.7 \times 10^{-29} \times \left(\frac{300}{T_{ion}}\right)^{2.1}$	42	
$N_2^+ + N_2 + N_2 \rightarrow N_4^+ + N_2$	$5.2 \times 10^{-29} \times \left(\frac{300}{T_{ion}}\right)^{2.2}$	42	
$N^+ + N + N_2 \rightarrow N_2^+ + N_2$	$1.0 \times 10^{-29}$	42	
$N^+ + N \rightarrow N_2^+$	$1.0 \times 10^{-29}$	64	
$N_3^+ + N \rightarrow N_2^+ + N_2$	$6.6 \times 10^{-11}$	42	
$N_4^+ + N \rightarrow N^+ + N_2 + N_2$	$1.0 \times 10^{-11}$	42	
$N_2^+ + N_2(A^3\Sigma_u^+) \rightarrow N_3^+ + N$	$3.0 \times 10^{-10}$	41	
$O^- + M \rightarrow O + M + e^-$	$4.0 \times 10^{-12}$	41	a
$O^- + O \rightarrow O_2 + e^-$	$2.3 \times 10^{-10}$	65	
$O^- + O_2(g, v) + M \rightarrow O_3^- + M$	$1.1 \times 10^{-30} \times \exp\left(\frac{300}{T_g}\right)$	65	a, b

$O^- + O_2(g, v) \rightarrow O_3 + e^-$	$5.0 \times 10^{-15}$	42	b
$O^- + O_3 \rightarrow O_2 + O_2 + e^-$	$3.0 \times 10^{-10}$	66	
$O^- + O_3 \rightarrow O_3^- + O$	$5.3 \times 10^{-10}$	67	
$O^+ + O + M \rightarrow O_2^+ + M$	$1.0 \times 10^{-29}$	62	a
$O^+ + O_2(g, v) \rightarrow O + O_2^+$	$1.9 \times 10^{-11} \times \left(\frac{T_g}{300}\right)^{-0.5}$	68	b
$O^+ + O_3 \rightarrow O_2^+ + O_2$	$1.0 \times 10^{-10}$	62	
$O_2^- + M \rightarrow O_2 + M + e^-$	$2.7 \times 10^{-10} \times \left(\frac{T_g}{300}\right)^{0.5} \times \exp\left(-\frac{5590}{T_g}\right)$	68	a
$O_2^- + O \rightarrow O_2 + O^-$	$3.31 \times 10^{-10}$	65	
$O_2^- + O_2(g, v) + M \rightarrow O_4^- + M$	$3.5 \times 10^{-31} \times \left(\frac{T_g}{300}\right)^{-1.0}$	62,65,67	a, b
$O_2^- + O_2 \rightarrow O_2 + O_2 + e^-$	$2.18 \times 10^{-18}$	69	
$O_2^- + O_3 \rightarrow O_3^- + O_2$	$4.0 \times 10^{-10}$	65	
$O_2^+ + O_2(g, v) + M \rightarrow O_4^+ + M$	$2.4 \times 10^{-30} \times \left(\frac{T_g}{300}\right)^{-3.2}$	62	a, b
$O_3^- + M \rightarrow O_3 + M + e^-$	$2.3 \times 10^{-11}$	68	a
$O_3^- + O \rightarrow O_2 + O_2 + e^-$	$1.0 \times 10^{-13}$	67	
$O_3^- + O \rightarrow O_2^- + O_2$	$2.5 \times 10^{-10}$	35	
$O_3^- + O \rightarrow O_3 + O^-$	$1.0 \times 10^{-13}$	65	
$O_3^- + O_3 \rightarrow O_2 + O_2 + O_2 + e^-$	$3.0 \times 10^{-10}$	67	
$O_4^- + O \rightarrow O^- + O_2 + O_2$	$3.0 \times 10^{-10}$	62	
$O_4^- + O \rightarrow O_3^- + O_2$	$4.0 \times 10^{-10}$	62	
$O_4^- + O_2 \rightarrow O_2^- + O_2 + O_2$	$1.0 \times 10^{-10} \times \exp\left(-\frac{1044}{T_g}\right)$	42	
$O_4^+ + O \rightarrow O_2^+ + O_3$	$3.0 \times 10^{-10}$	62	
$O_4^+ + O_2 \rightarrow O_2^+ + O_2 + O_2$	$3.3 \times 10^{-6} \times \left(\frac{300}{T_g}\right)^{4.0} \times \exp\left(-\frac{5030}{T_g}\right)$	62	
$O^- + O_2(a^1\Delta) \rightarrow O_3 + e^-$	$3.0 \times 10^{-10}$	42	
$O_2^- + O_2(a^1\Delta) \rightarrow O_2 + O_2 + e^-$	$2.0 \times 10^{-10}$	42	
$O_2^- + O_2(b^1\Sigma^+) \rightarrow O_2 + O_2 + e^-$	$3.6 \times 10^{-10}$	42	
$O_2^+ + O_2(E_x) + M \rightarrow O_4^+ + M$	$2.4 \times 10^{-30} \times \left(\frac{T_g}{300}\right)^{-3.2}$	42	a, c, d
$O_4^+ + O_2(a^1\Delta) \rightarrow O_2^+ + O_2 + O_2$	$1.0 \times 10^{-10}$	42	
$O_4^- + O_2(E_x) \rightarrow O_2^- + O_2 + O_2$	$1.0 \times 10^{-10}$	42	c
$O^- + O_2(a^1\Delta) \rightarrow O_2^- + O$	$1.0 \times 10^{-10}$	42	

$O^- + O_2(E_x) + M \rightarrow O_3^- + M$	$1.1 \times 10^{-30} \times \exp\left(\frac{300}{T_g}\right)$	42	a, c, e
$O_2^- + O_2(E_x) + M \rightarrow O_4^- + M$	$3.5 \times 10^{-31} \times \exp\left(\frac{T_g}{300}\right)^{-1.0}$	62	a, c, f
$N^+ + N + O_2 \rightarrow N_2^+ + O_2$	$1.0 \times 10^{-29}$	42	
$N^+ + N_2O \rightarrow NO^+ + N_2$	$5.5 \times 10^{-10}$	42	
$N^+ + NO \rightarrow N_2^+ + O$	$3.0 \times 10^{-12}$	42	
$N^+ + NO \rightarrow NO^+ + N$	$8.0 \times 10^{-10}$	42	
$N^+ + NO \rightarrow O^+ + N_2$	$1.0 \times 10^{-12}$	42	
$N^+ + O + M \rightarrow NO^+ + M$	$1.0 \times 10^{-29}$	42	a
$N^+ + O \rightarrow N + O^+$	$1.0 \times 10^{-12}$	42	
$N^+ + O_2 \rightarrow NO^+ + O$	$2.5 \times 10^{-10}$	42	
$N^+ + O_2 \rightarrow O^+ + NO$	$2.8 \times 10^{-11}$	42	
$N^+ + O_2 \rightarrow O_2^+ + N$	$2.8 \times 10^{-10}$	42	
$N^+ + O_3 \rightarrow NO^+ + O_2$	$5.0 \times 10^{-10}$	42	
$N_2^+ + N_2O \rightarrow N_2O^+ + N_2$	$5.0 \times 10^{-10}$	42	
$N_2^+ + N_2O \rightarrow NO^+ + N + N_2$	$4.0 \times 10^{-10}$	42	
$N_2^+ + NO \rightarrow NO^+ + N_2$	$3.3 \times 10^{-10}$	42	
$N_2^+ + O \rightarrow NO^+ + N$	$1.3 \times 10^{-10} \times \left(\frac{300}{T_{ion}}\right)^{0.5}$	42	
$N_2^+ + O_2 \rightarrow O_2^+ + N_2$	$6.0 \times 10^{-11} \times \left(\frac{300}{T_{ion}}\right)^{0.5}$	42	
$N_2^+ + O_3 \rightarrow O_2^+ + O + N_2$	$1.0 \times 10^{-10}$	42	
$N_2O^- + N \rightarrow NO + N_2 + e^-$	$5.0 \times 10^{-10}$	41	
$N_2O^- + O \rightarrow NO + NO + e^-$	$1.5 \times 10^{-10}$	41	
$N_2O^+ + NO \rightarrow NO^+ + N_2O$	$2.9 \times 10^{-10}$	42	
$N_3^+ + NO \rightarrow N_2O^+ + N_2$	$7.0 \times 10^{-11}$	42	
$N_3^+ + NO \rightarrow NO^+ + N + N_2$	$7.0 \times 10^{-11}$	42	
$N_3^+ + O_2 \rightarrow NO_2^+ + N_2$	$4.4 \times 10^{-11}$	42	
$N_3^+ + O_2 \rightarrow O_2^+ + N + N_2$	$2.3 \times 10^{-11}$	42	
$N_4^+ + NO \rightarrow NO^+ + N_2 + N_2$	$4.0 \times 10^{-10}$	42	
$N_4^+ + O \rightarrow O^+ + N_2 + N_2$	$2.5 \times 10^{-10}$	42	
$N_4^+ + O_2 \rightarrow O_2^+ + N_2 + N_2$	$2.5 \times 10^{-10}$	42	
$NO^- + N_2O \rightarrow NO + N_2O + e^-$	$4.26 \times 10^{-10} \times \exp\left(-\frac{107.2}{T_g}\right)$	70	
$NO^- + NO \rightarrow NO + NO + e^-$	$3.28 \times 10^{-10} \times \exp\left(-\frac{105.1}{T_g}\right)$	70	
$NO^- + N \rightarrow N_2O + e^-$	$5.0 \times 10^{-10}$	42	
$NO^- + N_2O \rightarrow NO_2^- + N_2$	$2.8 \times 10^{-14}$	42	

$\text{NO}^- + \text{NO}_2 \rightarrow \text{NO}_2^- + \text{NO}$	$7.4 \times 10^{-10}$	42	
$\text{NO}^- + \text{O} \rightarrow \text{NO}_2 + \text{e}^-$	$1.5 \times 10^{-10}$	41	
$\text{NO}^- + \text{O}_2 \rightarrow \text{O}_2^- + \text{NO}$	$5.0 \times 10^{-10}$	42	
$\text{NO}_2^- + \text{N} \rightarrow \text{NO} + \text{NO} + \text{e}^-$	$5.0 \times 10^{-10}$	41	
$\text{NO}_2^- + \text{N}_2\text{O}_5 \rightarrow \text{NO}_3^- + \text{NO}_2 + \text{NO}_2$	$7.0 \times 10^{-10}$	42	
$\text{NO}_2^- + \text{NO}_2 \rightarrow \text{NO}_3^- + \text{NO}$	$4.0 \times 10^{-12}$	42	
$\text{NO}_2^- + \text{NO}_3 \rightarrow \text{NO}_3^- + \text{NO}_2$	$5.0 \times 10^{-10}$	42	
$\text{NO}_2^- + \text{O}_3 \rightarrow \text{NO}_3^- + \text{O}_2$	$1.8 \times 10^{-11}$	42	
$\text{NO}_2^+ + \text{NO} \rightarrow \text{NO}^+ + \text{NO}_2$	$2.9 \times 10^{-10}$	42	
$\text{NO}_3^- + \text{N} \rightarrow \text{NO} + \text{NO}_2 + \text{e}^-$	$5.0 \times 10^{-10}$	41	
$\text{NO}_3^- + \text{NO} \rightarrow \text{NO}_2^- + \text{NO}_2$	$3.0 \times 10^{-15}$	42	
$\text{NO}_3^- + \text{O} \rightarrow \text{NO} + \text{O}_3 + \text{e}^-$	$1.5 \times 10^{-10}$	41	
$\text{O}^- + \text{N} \rightarrow \text{NO} + \text{e}^-$	$2.6 \times 10^{-10}$	42	
$\text{O}^- + \text{N}_2(\text{g}, \nu) \rightarrow \text{N}_2\text{O} + \text{e}^-$	$0.5 \times 10^{-13}$	42	b
$\text{O}^- + \text{N}_2(\text{A}^3\Sigma_u^+) \rightarrow \text{O} + \text{N}_2 + \text{e}^-$	$2.2 \times 10^{-9}$	42	
$\text{O}^- + \text{N}_2(\text{B}^3\Pi_g) \rightarrow \text{O} + \text{N}_2 + \text{e}^-$	$1.9 \times 10^{-9}$	42	
$\text{O}^- + \text{N}_2\text{O} \rightarrow \text{N}_2\text{O}^- + \text{O}$	$2.0 \times 10^{-12}$	42	
$\text{O}^- + \text{N}_2\text{O} \rightarrow \text{NO}^- + \text{NO}$	$2.0 \times 10^{-10}$	42	
$\text{O}^- + \text{NO} + \text{M} \rightarrow \text{NO}_2^- + \text{M}$	$1.0 \times 10^{-29}$	42	a
$\text{O}^- + \text{NO} \rightarrow \text{NO}_2 + \text{e}^-$	$2.6 \times 10^{-10}$	42	
$\text{O}^- + \text{NO}_2 \rightarrow \text{NO}_2^- + \text{O}$	$1.2 \times 10^{-9}$	42	
$\text{O}^+ + \text{N} + \text{M} \rightarrow \text{NO}^+ + \text{M}$	$1.0 \times 10^{-29}$	42	a
$\text{O}^+ + \text{N} \rightarrow \text{N}^+ + \text{O}$	$1.3 \times 10^{-10}$	42	
$\text{O}^+ + \text{N}_2(\text{g}, \nu) + \text{M}$ $\quad \rightarrow \text{NO}^+ + \text{N} + \text{M}$	$6.0 \times 10^{-29} \times \left(\frac{300}{T_{\text{ion}}}\right)^2$	42	a, b
$\text{O}^+ + \text{N}_2(\text{g}, \nu) \rightarrow \text{NO}^+ + \text{N}$	$(1.5 - 2.0 \times 10^{-3} \times T_{\text{ion}} +$ $9.6 \times 10^{-7} \times T_{\text{ion}}^2) \times 1.0 \times$ $10^{-12}$	42	b
$\text{O}^+ + \text{N}_2\text{O} \rightarrow \text{N}_2\text{O}^+ + \text{O}$	$2.2 \times 10^{-10}$	42	
$\text{O}^+ + \text{N}_2\text{O} \rightarrow \text{NO}^+ + \text{NO}$	$2.3 \times 10^{-10}$	42	
$\text{O}^+ + \text{N}_2\text{O} \rightarrow \text{O}_2^+ + \text{N}_2$	$2.0 \times 10^{-11}$	42	
$\text{O}^+ + \text{NO} \rightarrow \text{NO}^+ + \text{O}$	$2.4 \times 10^{-11}$	42	
$\text{O}^+ + \text{NO} \rightarrow \text{O}_2^+ + \text{N}$	$3.0 \times 10^{-12}$	42	
$\text{O}^+ + \text{NO}_2 \rightarrow \text{NO}_2^+ + \text{O}$	$1.6 \times 10^{-9}$	42	
$\text{O}_2^- + \text{N} \rightarrow \text{NO}_2 + \text{e}^-$	$5.0 \times 10^{-10}$	42	
$\text{O}_2^- + \text{N}_2(\text{B}^3\Pi_g) \rightarrow \text{O}_2 + \text{N}_2 + \text{e}^-$	$2.5 \times 10^{-9}$	42	
$\text{O}_2^- + \text{N}_2(\text{A}^3\Sigma_u^+) \rightarrow \text{O}_2 + \text{N}_2 + \text{e}^-$	$2.1 \times 10^{-9}$	42	
$\text{O}_3^- + \text{N}_2(\text{B}^3\Pi_g) \rightarrow \text{O}_3 + \text{N}_2 + \text{e}^-$	$2.5 \times 10^{-9}$	41	

$O_3^- + N_2(A^3\Sigma_u^+) \rightarrow O_3 + N_2 + e^-$	$2.1 \times 10^{-9}$	41	
$NO^- + N_2(B^3\Pi_g) \rightarrow NO + N_2 + e^-$	$2.5 \times 10^{-9}$	41	
$NO^- + N_2(A^3\Sigma_u^+) \rightarrow NO + N_2 + e^-$	$2.1 \times 10^{-9}$	41	
$N_2O^- + N_2(B^3\Pi_g) \rightarrow N_2O + N_2 + e^-$	$2.5 \times 10^{-9}$	41	
$N_2O^- + N_2(A^3\Sigma_u^+) \rightarrow N_2O + N_2 + e^-$	$2.1 \times 10^{-9}$	41	
$NO_2^- + N_2(B^3\Pi_g) \rightarrow NO_2 + N_2 + e^-$	$2.5 \times 10^{-9}$	41	
$NO_2^- + N_2(A^3\Sigma_u^+) \rightarrow NO_2 + N_2 + e^-$	$2.1 \times 10^{-9}$	41	
$NO_3^- + N_2(B^3\Pi_g) \rightarrow NO_3 + N_2 + e^-$	$2.5 \times 10^{-9}$	41	
$NO_3^- + N_2(A^3\Sigma_u^+) \rightarrow NO_3 + N_2 + e^-$	$2.1 \times 10^{-9}$	41	
$O_2^- + NO_2 \rightarrow NO_2^- + O_2$	$7.0 \times 10^{-10}$	42	
$O_2^- + NO_3 \rightarrow NO_3^- + O_2$	$5.0 \times 10^{-10}$	42	
$O_2^+ + N \rightarrow NO^+ + O$	$1.2 \times 10^{-10}$	42	
$O_2^+ + N_2(g, v) + N_2 \rightarrow O_2^+N_2 + N_2$	$9.0 \times 10^{-31} \times \left(\frac{300}{T_{ion}}\right)^2$	42	b
$O_2^+ + N_2(g, v) \rightarrow NO^+ + NO$	$1.0 \times 10^{-17}$	42	b
$O_2^+ + NO \rightarrow NO^+ + O_2$	$6.3 \times 10^{-10}$	42	
$O_2^+ + NO_2 \rightarrow NO^+ + O_3$	$1.0 \times 10^{-11}$	42	
$O_2^+ + NO_2 \rightarrow NO_2^+ + O_2$	$6.6 \times 10^{-10}$	42	
$O_2^+N_2 + N_2 \rightarrow O_2^+ + N_2 + N_2$	$1.1 \times 10^{-6} \times \left(\frac{300}{T_{ion}}\right)^{5.3} \times \exp\left(-\frac{2360}{T_{ion}}\right)$	42	
$O_2^+N_2 + O_2 \rightarrow O_4^+ + N_2$	$1.0 \times 10^{-9}$	42	
$O_3^- + N \rightarrow NO + O_2 + e^-$	$5.0 \times 10^{-10}$	41	
$O_3^- + NO \rightarrow NO_2^- + O_2$	$2.6 \times 10^{-12}$	42	
$O_3^- + NO \rightarrow NO_3^- + O$	$1.0 \times 10^{-11}$	42	
$O_3^- + NO_2 \rightarrow NO_2^- + O_3$	$7.0 \times 10^{-11}$	42	
$O_3^- + NO_2 \rightarrow NO_3^- + O_2$	$2.0 \times 10^{-11}$	42	
$O_3^- + NO_3 \rightarrow NO_3^- + O_3$	$5.0 \times 10^{-10}$	42	
$O_4^- + N_2 \rightarrow O_2^- + O_2 + N_2$	$1 \times 10^{-10} \times \exp\left(-\frac{1044}{T_g}\right)$	42	

$O_4^- + NO \rightarrow NO_3^- + O_2$	$2.5 \times 10^{-10}$	42	
$O_4^+ + N_2(g, v) \rightarrow O_2^+ N_2 + O_2$	$4.6 \times 10^{-12} \times \left(\frac{T_{ion}}{300}\right)^{2.5} \times \exp\left(-\frac{2650}{T_{ion}}\right)$	42	b
$O_4^+ + NO \rightarrow NO^+ + O_2 + O_2$	$1.0 \times 10^{-10}$	42	

<sup>a</sup> M represents any neutral species.

<sup>b</sup> For any species indicated with (g, v), g and v stand for its ground and vibrationally excited state, respectively.

<sup>c</sup>  $O_2(E_x)$  represents the electronically excited states:  $O_2(a^1\Delta)$  and  $O_2(b^1\Sigma^+)$ .

<sup>d</sup> The rate coefficient is assumed to be equal to the rate of  $O_2^+ + O_2 + M \rightarrow O_4^+ + M$ .

<sup>e</sup> The rate coefficient is assumed to be equal to the rate of  $O^- + O_2 + M \rightarrow O_3^- + M$ .

<sup>f</sup> The rate coefficient is assumed to be equal to the rate of  $O_2^- + O_2 + M \rightarrow O_4^- + M$ .

*Table S.12 Ion-ion reactions included in the model, the corresponding rate coefficient expressions and the references.  $T_g$  is the gas temperature in K. The rate coefficients are expressed in  $cm^3 s^{-1}$  or  $cm^6 s^{-1}$  for binary or ternary reactions, respectively.*

Reaction	Rate coefficient	Ref.	Note
$O^- + O^+ + M \rightarrow O_2 + M$	$1.0 \times 10^{-25} \times \left(\frac{300}{T_g}\right)^{2.5}$	68	a
$O^- + O_2^+ + M \rightarrow O_3 + M$	$1.0 \times 10^{-25} \times \left(\frac{300}{T_g}\right)^{2.5}$	68	a
$O_2^- + O^+ + M \rightarrow O_3 + M$	$1.0 \times 10^{-25} \times \left(\frac{300}{T_g}\right)^{2.5}$	68	a
$O_2^- + O_2^+ + M \rightarrow O_2 + O_2 + M$	$1.0 \times 10^{-25} \times \left(\frac{300}{T_g}\right)^{2.5}$	68	a
$O_3^- + O^+ + M \rightarrow O_3 + O + M$	$2.0 \times 10^{-25} \times \left(\frac{300}{T_g}\right)^{2.5}$	41	a
$O_3^- + O_2^+ + M \rightarrow O_3 + O_2 + M$	$2.0 \times 10^{-25} \times \left(\frac{300}{T_g}\right)^{2.5}$	41	a
$O^- + O_2^+ \rightarrow O + O + O$	$2.60 \times 10^{-8} \times \left(\frac{300}{T_g}\right)^{0.44}$	65	a
$O_3^- + O_2^+ \rightarrow O + O + O_3$	$1.0 \times 10^{-7} \times \left(\frac{300}{T_g}\right)^{0.5}$	65	a

$O^- + O^+ \rightarrow O + O$	$4.0 \times 10^{-8} \times \left(\frac{300}{T_g}\right)^{0.43}$	65	
$O^- + O_2^+ \rightarrow O_2 + O$	$2.6 \times 10^{-8} \times \left(\frac{300}{T_g}\right)^{0.44}$	65	
$O_2^- + O^+ \rightarrow O + O_2$	$2.7 \times 10^{-7} \times \left(\frac{300}{T_g}\right)^{0.5}$	65	
$O_2^- + O_2^+ \rightarrow O_2 + O_2$	$2.01 \times 10^{-7} \times \left(\frac{300}{T_g}\right)^{0.5}$	65	
$O_2^- + O_2^+ \rightarrow O_2 + O + O$	$1.01 \times 10^{-13} \times \left(\frac{300}{T_g}\right)^{0.5}$	65	
$O_3^- + O^+ \rightarrow O_3 + O$	$1.0 \times 10^{-7} \times \left(\frac{300}{T_g}\right)^{0.5}$	69	
$O_3^- + O_2^+ \rightarrow O_2 + O_3$	$2.0 \times 10^{-7} \times \left(\frac{300}{T_g}\right)^{0.5}$	65	
$NO^- + A^+ + M \rightarrow NO + A + M$	$2.0 \times 10^{-25} \times \left(\frac{300}{T_g}\right)^{2.5}$	41	a, b
$NO_2^- + A^+ + M \rightarrow NO_2 + A + M$	$2.0 \times 10^{-25} \times \left(\frac{300}{T_g}\right)^{2.5}$	41	a, b
$N_2O^- + A^+ + M \rightarrow N_2O + A + M$	$2.0 \times 10^{-25} \times \left(\frac{300}{T_g}\right)^{2.5}$	41	a, b
$NO_3^- + A^+ + M \rightarrow NO_3 + A + M$	$2.0 \times 10^{-25} \times \left(\frac{300}{T_g}\right)^{2.5}$	41	a, b
$O_3^- + B^+ + M \rightarrow O_3 + B + M$	$2.0 \times 10^{-25} \times \left(\frac{300}{T_g}\right)^{2.5}$	41	a, c

<sup>a</sup> M represents any neutral species.

<sup>b</sup> A represents N, O, N<sub>2</sub>, O<sub>2</sub>, NO, NO<sub>2</sub> and N<sub>2</sub>O species.

<sup>c</sup> B represents N, N<sub>2</sub>, NO, NO<sub>2</sub> and N<sub>2</sub>O species.

Table S.13 Optical transitions of N<sub>2</sub> and O<sub>2</sub> species. The rate coefficients are expressed in s<sup>-1</sup>.

Reaction	Rate coefficient	Ref.	Note
$N_2(A^3\Sigma_u^+) \rightarrow N_2$	0.5	42	
$N_2(B^3\Pi_g) \rightarrow N_2(A^3\Sigma_u^+)$	$1.35 \times 10^5$	42	
$N_2(a^1\Sigma_u^-) \rightarrow N_2$	$1.0 \times 10^2$	42	
$N_2(C^3\Pi_u) \rightarrow N_2(B^3\Pi_g)$	$2.45 \times 10^7$	42	
$O_2(a^1\Delta) \rightarrow O_2$	$2.6 \times 10^{-4}$	42	
$O_2(b^1\Sigma^+) \rightarrow O_2$	$8.5 \times 10^{-2}$	42	
$O_2(b^1\Sigma^+) \rightarrow O_2(a^1\Delta)$	$1.5 \times 10^{-3}$	42	

<sup>a</sup> O<sub>2</sub>(A<sup>3</sup>Σ<sup>+</sup>, C<sup>3</sup>Δ, c<sup>1</sup>Σ<sup>-</sup>) is a combination of three electronic excited states at a threshold energy of 4.5 eV.

The reaction rate expressions of the VT relaxations and VV exchanges between N<sub>2</sub> - N<sub>2</sub>, N<sub>2</sub> - O<sub>2</sub> and O<sub>2</sub> - O<sub>2</sub> are calculated using the Forced Harmonic Oscillator (FHO) model proposed by Adamovich et al.<sup>71</sup> This method offers a semi-classical non-perturbative analytical solution for VT and VV transitions of diatomic molecules by averaging the VT and VV probabilities (P<sub>VT</sub> and P<sub>VV</sub>) over the one-dimensional Boltzmann distribution.

$$P_{VT}(i \rightarrow f) = \frac{(n_s)^s}{(s!)^2} \cdot \varepsilon^s \cdot \exp\left(-\frac{2n_s}{s+1}\varepsilon\right) \quad (10)$$

$$P_{VV}(i_1, i_2 \rightarrow f_1, f_2) \cong \frac{[n_s^{(1)} n_s^{(2)}]^s}{(s!)^2} \cdot \left(\frac{\rho_\varepsilon^2}{4}\right)^s \cdot \exp\left[-\frac{2n_s^{(1)} n_s^{(2)} \rho_\varepsilon^2}{s+1} \frac{1}{4}\right] \quad (11)$$

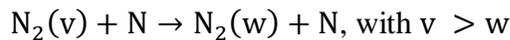
with  $s = |i - f|$ ,  $n_s = \left[\frac{\max(i,f)!}{\min(i,f)!}\right]^{1/s}$ .  $\rho_\varepsilon$  and  $\varepsilon$  are collision and potential specific parameters.

*Table S. 14 Vibrational – vibrational exchanges and vibrational – translational relaxations for N<sub>2</sub> (as an example) and the rate coefficient expression..*

Reaction	Rate coefficient
N <sub>2</sub> (v <sub>i</sub> ) + M → N <sub>2</sub> (v <sub>i</sub> - 1) + M	$Z \cdot \left(\frac{m}{kT}\right) \int_0^\infty P_{VT}(\bar{v}) \cdot \exp\left(\frac{-mv^2}{2kT}\right) v dv$
N <sub>2</sub> (v <sub>i</sub> ) + N <sub>2</sub> (v <sub>j</sub> ) → N <sub>2</sub> (v <sub>i</sub> - 1) + N <sub>2</sub> (v <sub>j</sub> + 1)	$Z \cdot \left(\frac{m}{kT}\right) \int_0^\infty P_{VV}(\bar{v}) \cdot \exp\left(\frac{-mv^2}{2kT}\right) v dv$

M represents any neutral particle in the plasma.  
v<sub>i</sub> and v<sub>j</sub> are the vibrational levels of N<sub>2</sub> (0-24).  
Z is the collision frequency and v is the particle velocity.

The reaction rates of the VT relaxations between N<sub>2</sub> – N are based on quasi classical calculations that have been reproduced through a fit as proposed by Esposito et al.<sup>72</sup>, for the following general reaction:



All the relevant trends in the rate were taken into consideration by using an additive model into the exponential argument of the reaction rate constant, as shown in the following expression (valid for v = 1 – 66 and Δv = 1 – 30):

$$K(v, T, \Delta v) = \exp \left( a_1(v, \Delta v) + \frac{a_2(v, \Delta v)}{T} + \frac{a_3(v, \Delta v)}{T^2} + \frac{a_4(v, \Delta v)}{T^3} + a_5(v, \Delta v) \cdot \ln(T) \right) \quad (12)$$

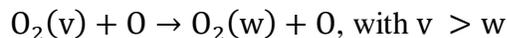
where

$$a_i(v, \Delta v) = z_{i0}(\Delta v) + z_{i1}(\Delta v)v + z_{i2}(\Delta v)v^2 + z_{i3}(\Delta v)v^3 + z_{i4}(\Delta v)v^4 \quad (13)$$

$$z_{ij}(\Delta v) = b_{ij} + c_{ij}\Delta v \quad (14)$$

For which the parameters are reported in <sup>72</sup>.

Similarly, the reaction rates of the VT relaxations between O<sub>2</sub> – O are based on quasi classical calculations that have been reproduced through a fit as proposed by Esposito et al.<sup>73</sup>, for the following general reaction:



The reaction rate constant is then determined based on the following expression:

$$K(T, v, \Delta v) = \text{DegF} \cdot \exp(a_1(v, \Delta v) + \frac{a_2(v, \Delta v)}{\ln(T)} + a_3(v, \Delta v) \cdot \ln(T)) \quad (15)$$

where  $\Delta v$  is  $(v - w)$

$$a_i(v, \Delta v) = b_{i1}(\Delta v) + b_{i2}(\Delta v) \cdot \ln(v) + \frac{b_{i3}(\Delta v) + b_{i4}(\Delta v)v + b_{i5}(\Delta v)v^2}{10^{21} + \exp(v)} \quad (15)$$

$$b_{ij}(\Delta v) = c_{ij1} + c_{ij2} \cdot \ln(\Delta v) + c_{ij3} \cdot \Delta v \cdot \exp(-\Delta v) + c_{ij4} \cdot \Delta v \cdot \Delta v \quad (16)$$

The coefficients  $c_{ijk}$  have been generated using a linear least squares method and are reported in<sup>73</sup> where the degeneracy factor (DegF) is also explained.

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