

Supporting Information: Nanosecond Pulsed Discharge for CO₂ Conversion: Kinetic Modelling to Elucidate the Chemistry and Improve the Performance

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1. Detailed description of the model

The 0D model is based on solving equation (1):

$$\frac{\partial n_s}{\partial t} = \sum_{i=1}^j [(a_{s,i}^R - a_{s,i}^L) R_i] \quad (1)$$

where n_s is the density of species s (in m^{-3}), j the total number of reactions, $a_{s,i}^L$ and $a_{s,i}^R$ the stoichiometric coefficients at the left hand side and right hand side of the reaction and R_i the rate of reaction (in $\text{m}^{-3} \text{s}^{-1}$), given by:

$$R_i = k_i \prod_s n_s^{a_{s,i}} \quad (2)$$

where k_i is the rate constant (in $\text{m}^3 \text{s}^{-1}$ or $\text{m}^6 \text{s}^{-1}$ for two-body or three-body reactions, respectively) and $a_{s,i}$ was defined above. The rate constants of the heavy particle reactions are either constant or dependent on the gas temperature, whereas the rate constants of the electron impact reactions depend on the electron temperature T_e or the reduced electric field E/N (i.e., the electric field E divided by the number density of all neutral species N , usually expressed in $\text{Td} = 10^{-21} \text{ V m}^2$). The rate constants of the electron impact reactions are generally calculated according to the following equation:

$$k_i = \int_{\varepsilon_{th}}^{\infty} \sigma_i(\varepsilon) v(\varepsilon) f(\varepsilon) d\varepsilon \quad (3)$$

with ε the electron energy (usually in eV), ε_{th} the minimum threshold energy needed to induce the reaction, $v(\varepsilon)$ the velocity of the electrons (in m s^{-1}), $\sigma_i(\varepsilon)$ the cross section of collision i (in m^2), and $f(\varepsilon)$ the (normalized) electron energy distribution function (EEDF; in eV^{-1}) calculated using a Boltzmann solver. The reactions included in the model, along with their rate coefficients and the references where these data are adopted from, are listed in Tables S.1-S.5.

In this work we use the ZDPlaskin code ¹ to solve the balance equations (1) of all species, which also has a built-in Boltzmann solver, called BOLSIG+ ², to calculate the EEDF and the rate constants of the electron impact reactions based on a set of cross sections, the plasma composition, the gas temperature and the reduced electric field (E/N).

The electric field (E ; in $V\ m^{-1}$) is calculated from a given power density, using the so-called local field approximation ³:

$$E = \sqrt{\frac{P}{\sigma}} \quad (4)$$

with P the input power density (in $W\ m^{-3}$) and σ the plasma conductivity ($A\ V^{-1}\ m^{-1}$). The plasma conductivity is estimated at the beginning of the simulations as ³:

$$\sigma = \frac{e^2 n_{e,init}}{m_e v_m} \quad (5)$$

with e the elementary charge ($1.6022 \times 10^{-19}\ C$), $n_{e,init}$ the initial electron density (in m^{-3}), m_e the electron mass ($9.1094 \times 10^{-31}\ kg$) and v_m the collision frequency (in s^{-1}) calculated using BOLSIG+. During the simulation the plasma conductivity is calculated as ³:

$$\sigma = \frac{e v_d n_e}{\left(\frac{E}{N}\right)_{prev} n_0} \quad (6)$$

with v_d the electron drift velocity (in $m\ s^{-1}$), which is calculated using BOLSIG+ implemented in ZDPlaskin, and $\left(\frac{E}{N}\right)_{prev}$ the reduced electric field at the previous time step (in $V\ m^2$).

The balance equation for the gas temperature T_g (in K) is also solved:

$$N \frac{\gamma k}{\gamma - 1} \frac{dT_g}{dt} = P_{e,el} + \sum_j R_j \Delta H_j - P_{ext} \quad (7)$$

where $N = \sum n_i$ is the total neutral species density, γ is the specific heat ratio of the total gas mixture, k is the Boltzmann constant (in $J\ K^{-1}$), $P_{e,el}$ is the gas heating power density due to elastic electron-neutral collisions (in $W\ m^{-3}$), R_j is the rate of reaction j (in $m^{-3}\ s^{-1}$), ΔH_j is the heat released (or consumed when this value is negative) by reaction j (in J) and P_{ext} is the heat loss due to energy exchange with the surroundings (in $W\ m^{-3}$). The latter one is originally calculated as:

$$P_{ext} = \frac{8\lambda}{R^2} (T_g - T_{g,i}) \quad (8)$$

where λ is the gas thermal conductivity (in $\text{W m}^{-1} \text{K}^{-1}$), R the radius of the plasma zone, T_g the plasma gas temperature and $T_{g,i}$ the gas temperature just before the start of the pulse, i.e. 293.15 K at the beginning of the simulation, or the gas temperature at the end of the afterglow of the previous pulse (see main text for more explanation).

Greig et al.⁴ and Shneider⁵ showed that in ns-pulsed discharges turbulent cooling is important. Therefore, we multiply equation (8) by a factor 9 to incorporate the more effective turbulent cooling, which is also successfully applied in 0D simulations for a turbulent GAP⁶⁻⁸, with this factor based on 2D fluid dynamics simulations⁹.

The specific heat ratio of the total (ideal) gas mixture is calculated from the specific heat ratios of the individual species in the model, γ_i , using the formula:

$$N \frac{\gamma}{\gamma-1} = \sum_i n_i \frac{\gamma_i}{\gamma_i-1} \quad (9)$$

where n_i are the densities of the individual species i . The individual specific heat ratios, γ_i , can be calculated from the specific heat capacity at constant pressure $c_{p,i}$ (in $\text{J K}^{-1} \text{kg}^{-1}$) using the relation:

$$c_{p,i} = \frac{\gamma_i}{\gamma_i-1} \frac{k}{M} \quad (10)$$

where k is the Boltzmann constant and M is the molar weight of CO_2 (in kg). Since the vibrational levels are treated as separate species, only the heat capacity due to translational and rotational degrees of freedom and, in the case of CO_2 , also the heat capacity due to the symmetric vibrational modes, which are not treated as individual species, should be taken into account^{10,11}. A classical partitioning between the translational and rotational degrees of

freedom is assumed, which gives a value for the specific heat ratio, at room temperature and above, of 1.67 for the atomic species and 1.40 for the diatomic molecules . For O₃, a value of 1.27 was taken ^{10,12}. Details about the calculation of the total heat capacity and the resulting specific heat ratio for CO₂, calculated using equation (10), can be found in ¹⁰.

Table S.1: Electron impact reactions calculated with cross sections data, using the calculated EEDF, as explained in section 2.1 of the main paper, as well as the references where the data are adopted from.

No.	Reaction	Ref	Note
(X1) ^a	$e^- + CO_2 \rightarrow 2e^- + CO_2^+$	13-15	
(X2) ^a	$e^- + CO_2 \rightarrow 2e^- + O + CO^+$	13-15	
(X3) ^a	$e^- + CO_2 \rightarrow 2e^- + O^+ + CO$	16	
(X4) ^a	$e^- + CO_2 \rightarrow 2e^- + O_2 + C^+$	16	
(X5) ^a	$e^- + CO_2 \rightarrow 2e^- + O_2^+ + C$	17	
(X6) ^a	$e^- + CO_2 \rightarrow O^- + CO$	13-15	
(X7) ^b	$e^- + CO_2 \rightarrow e^- + O + CO$	13-15	
(X8) ^a	$e^- + CO_2 \rightarrow e^- + CO_2(E1)$	13-15	
(X9) ^b	$e^- + CO_2 \leftrightarrow e^- + CO_2(Vx)$	13-15	$x = a, b, c, d$
(X10) ^c	$e^- + CO_2 \leftrightarrow e^- + CO_2(Vi)$	13-15	$i = 1 - 21$
(X11) ^a	$e^- + CO \rightarrow 2e^- + CO^+$	18	
(X12) ^a	$e^- + CO \rightarrow 2e^- + C^+ + O$	19	
(X13) ^a	$e^- + CO \rightarrow 2e^- + C + O^+$	19	
(X14) ^a	$e^- + CO \rightarrow C + O^-$	20	
(X14bis) ^b	$e^- + CO \rightarrow e^- + C + O$	21	
(X15)	$e^- + CO \leftrightarrow e^- + CO(Vi)$	21	$i = 1 - 10$
(X16) ^b	$e^- + O_2 \rightarrow e^- + O + O$	22	

(X16M) ^a	$e^- + O_2 + M \rightarrow O_2^- + M$	²²	
(X17) ^a	$e^- + O_2 \rightarrow O + O^-$	²²	
(X18) ^a	$e^- + O_2 \rightarrow 2e^- + O_2^+$	²³	
(X19) ^b	$e^- + O_2 \rightarrow 2e^- + O + O^+$	²³	
(X20)	$e^- + O_2 \leftrightarrow e^- + O_2(Vi)$	²²	$i = 1,2,3,4$
(X21)	$e^- + O_3 \rightarrow e^- + O_2 + O$	²⁴	
(X22)	$e^- + O_3 \rightarrow 2e^- + O_2^+ + O$	²⁴	
(X23)	$e^- + O_3 \rightarrow e^- + O^+ + O^- + O$	²⁴	
(X24)	$e^- + O_3 \rightarrow O^- + O_2$	²⁵	
(X25)	$e^- + O_3 \rightarrow O + O_2^-$	²⁵	
(X26)	$e^- + O \rightarrow 2e^- + O^+$	²⁶	
(X27)	$e^- + C \rightarrow 2e^- + C^+$	²⁷	
^a Same cross section also used for ground state.			
^b Cross section also used for the excited states, modified by lowering the energy threshold by the energy of the excited state.			
^c Cross section for the various levels (i,j) adopted from $e^- + CO_2 \rightarrow e^- + CO_2(Vi)$ but scaled and shifted using Fridman's approximation ^{28,29}			

Table S.2: Electron impact reactions using analytical expressions for the rate coefficients, given in $m^3 s^{-1}$ and $m^6 s^{-1}$, for two-body and three-body reactions, respectively, as well as the references where the data are adopted from. T_g and T_e are given in K and eV, respectively.

No.	Reaction	Rate coefficient	Ref
(E1a)	$e^- + CO_2^+ \rightarrow CO(V1) + O$	$1.0 \times 10^{-11} T_e^{-0.5} T_g^{-1}$	30,31
(E1b)	$e^- + CO_2^+ \rightarrow C + O_2$	$1.0 \times 10^{-11} T_e^{-0.5} T_g^{-1}$	17
(E2) ^a	$e^- + CO_4^+ \rightarrow CO_2 + O_2$	$1.61 \times 10^{-13} T_e^{-0.5}$	17

(E3)	$e^- + CO^+ \rightarrow C + O$	$3.46 \times 10^{-14} T_e^{-0.48}$	32,33
(E4) ^a	$e^- + O + M \rightarrow O^- + M$	1.0×10^{-43}	31
^a The primary source was not accessible			

Table S.3: Ion-ion and ion-neutral reactions, as well as the references where the data are adopted from. The rate coefficients are given in $m^3 s^{-1}$ and $m^6 s^{-1}$, for two-body and three-body reactions, respectively. T_g is given in K.

No.	Reaction	Rate coefficient	Ref
(I1)	$CO_2 + CO^+ \rightarrow CO_2^+ + CO$	1.0×10^{-15}	34,35
(I2)	$CO_2 + O^- + M \rightarrow CO_3^- + M$	1.5×10^{-40}	34,36
(I3)	$CO_2 + O_2^- + M \rightarrow CO_4^- + M$	4.7×10^{-41}	34,36
(I4)	$CO + O^- \rightarrow CO_2 + e^-$	5.5×10^{-16}	34,37
(I5)	$CO + CO_3^- \rightarrow 2CO_2 + e^-$	5.0×10^{-19}	38
(I6) ^a	$CO_3^- + CO_2^+ \rightarrow 2CO_2(Vb) + O$	5.0×10^{-13}	31
(I7) ^a	$CO_4^- + CO_2^+ \rightarrow 2CO_2(Vb) + O_2$	5.0×10^{-13}	31
(I8) ^a	$O_2^- + CO_2^+ \rightarrow CO_2(V1) + O_2 + O$	6.0×10^{-13}	31
(I9)	$CO_3^- + O \rightarrow CO_2 + O_2^-$	8.0×10^{-17}	39
(I10a) ^a	$CO_4^- + O \rightarrow CO_3^- + O_2$	1.12×10^{-16}	34
(I10b) ^a	$CO_4^- + O \rightarrow CO_2 + O_2 + O^-$	1.4×10^{-17}	34
(I11)	$O + O^- \rightarrow O_2 + e^-$	2.3×10^{-16}	40
(I12) ^a	$O + O_2^- \rightarrow O_2 + O^-$	1.5×10^{-16}	34
(I13)	$O_2^- + M \rightarrow O_2 + M + e^-$	$2.7 \times 10^{-16} \left(\frac{T_g}{300}\right)^{0.5} \exp(-5590/T_g)$	41,42
(I14) ^c	$O^- + M \rightarrow O + M + e^-$	$2.3 \times 10^{-15} \exp(-26000/T_g)$	42-44

^a The primary source was not accessible

^c For usual values of gas temperature, i.e. $T_g \ll 26,000$ K, the rate coefficient is very low, as pointed out by Gudmundsson⁴⁵.

Table S.4: Neutral-neutral reactions, as well as the references where the data are adopted from. The rate coefficients are given in $\text{m}^3 \text{s}^{-1}$ and $\text{m}^6 \text{s}^{-1}$, for two-body and three-body reactions, respectively. T_g is given in K. The α parameter determines the effectiveness of lowering the activation energy for reactions involving vibrationally excited levels of the molecules (see details in ^{28,29})

No.	Reaction	Rate coefficient	α	Ref
(N1)	$CO_2 + M \rightarrow CO + O + M$	$6.06 \times 10^{-16} \exp(-52525/T_g)$	0.82	46
(N2)	$CO_2 + O \rightarrow CO + O_2$	$2.8 \times 10^{-17} \exp(-26500/T_g)$	0.50	47,48
(N3)	$CO_2 + C \rightarrow 2CO$	$< 1.0 \times 10^{-21}$	n.a.	49
(N4)	$CO + O + M \rightarrow CO_2 + M$	$8.3 \times 10^{-46} \exp(-1510/T_g)$	0.0	48,50
(N5)	$O_2 + CO \rightarrow CO_2 + O$	$4.2 \times 10^{-18} \exp(-24000/T_g)$	0.5	48
(N6)	$O_2 + C \rightarrow CO + O$	$1.99 \times 10^{-16} \exp(-2010/T_g)$	0.0	51
(N7)	$O + C + M \rightarrow CO + M$	$2.14 \times 10^{-41} \left(\frac{T_g}{300}\right)^{-3.08} \exp(-2144/T_g)$	0.0	47,48
(N8)	$O + O + M \rightarrow O_2 + M$	$5.2 \times 10^{-47} \exp(900/T_g)$	n.a.	47,48
(N9)	$O_2 + M \rightarrow O + O + M$	$3.0 \times 10^{-12} \frac{1}{T_g} \exp(-59380/T_g)$	1.0	47,48

Table S.5: Neutral reactions between vibrationally excited molecules, as well as the references where the data are adopted from. The rate coefficients are given in $\text{m}^3 \text{s}^{-1}$ and $\text{m}^6 \text{s}^{-1}$, for two-body and three-body reactions, respectively. T_g is given in K.

No.	Reaction	Rate coefficient	Ref
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(V1)	$CO_2(Va) + M \rightarrow CO_2 + M$	$7.14x10^{-15} \exp(-177T_g^{-1/3} + 451T_g^{-2/3})$	52-54
(V2a)	$CO_2(V1) + M \rightarrow CO_2(Va) + M$	$4.25x10^{-7} \exp(-407T_g^{-1/3} + 824T_g^{-2/3})$	54-56
(V2b)	$CO_2(V1) + M \rightarrow CO_2(Vb) + M$	$8.57x10^{-7} \exp(-404T_g^{-1/3} + 1096T_g^{-2/3})$	54-56
(V2c)	$CO_2(V1) + M \rightarrow CO_2(Vc) + M$	$1.43x10^{-7} \exp(-252T_g^{-1/3} + 685T_g^{-2/3})$	54-56
(V3)	$CO(V1) + M \rightarrow CO + M$	$1.0x10^{-18} T_g \exp(-150.7T_g^{-1/3})$	57
(V4)	$O_2(V1) + M \rightarrow O_2 + M$	$1.3x10^{-14} \exp(-158.7T_g^{-1/3})$	53,54
(V5)	$CO_2(V1) + CO_2 \rightarrow$ $CO_2(Va) + CO_2(Vb)$	$1.06x10^{-11} \exp(-242T_g^{-1/3} + 633T_g^{-2/3})$	54-56
(V6)	$CO_2(V1) + CO_2 \rightarrow$ $CO_2 + CO_2(V1)$	$1.32x10^{-18} \left(\frac{T_g}{300}\right)^{0.5} \frac{250}{T_g}$	58,59
(V7)	$CO(V1) + CO \rightarrow CO + CO(V1)$	$3.4x10^{-16} \left(\frac{T_g}{300}\right)^{0.5} \left(1.64x10^{-6} T_g + \frac{1.61}{T_g}\right)$	60,61
(V8)	$CO_2(V1) + CO \rightarrow CO_2 + CO(V1)$	$4.8x10^{-12} \exp(-153T_g^{-1/3})$	54,55

2. Extra calculated plasma characteristics

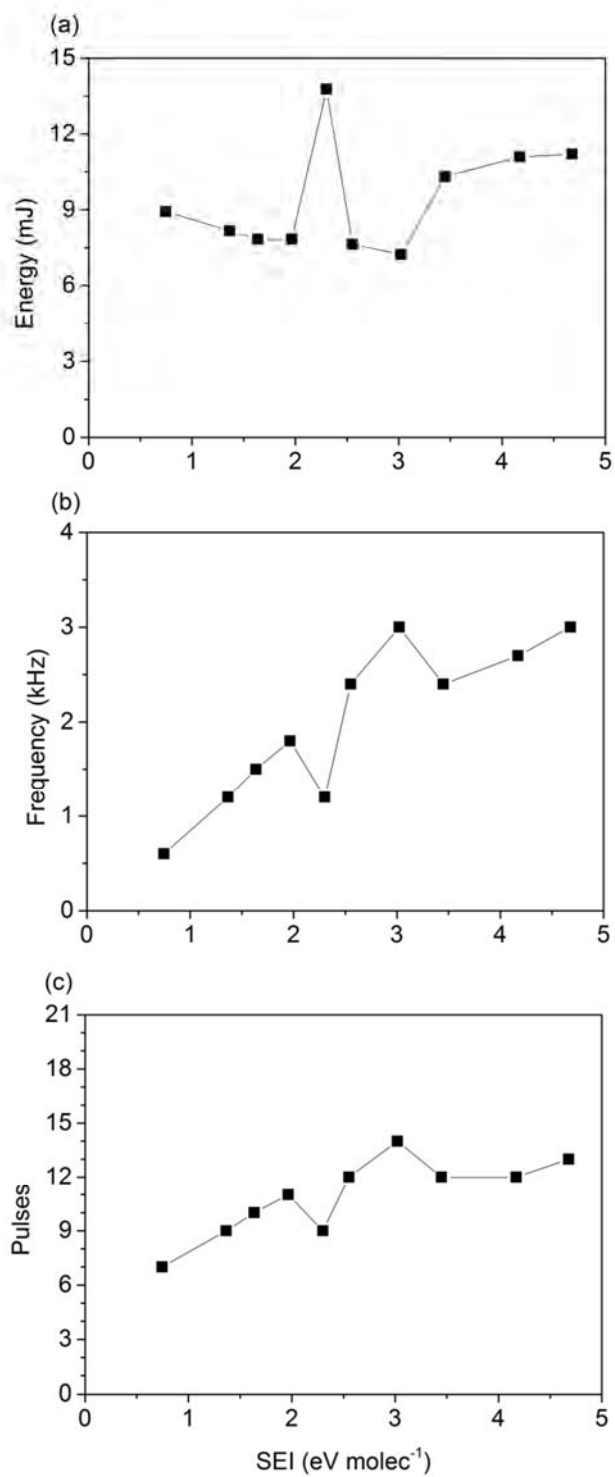


Figure S.1: Energy deposited per pulse (a), pulse frequency (b), and number of pulses felt by the gas molecules when travelling from pin HV electrode to grounded electrode (c), for the different SEI values investigated.

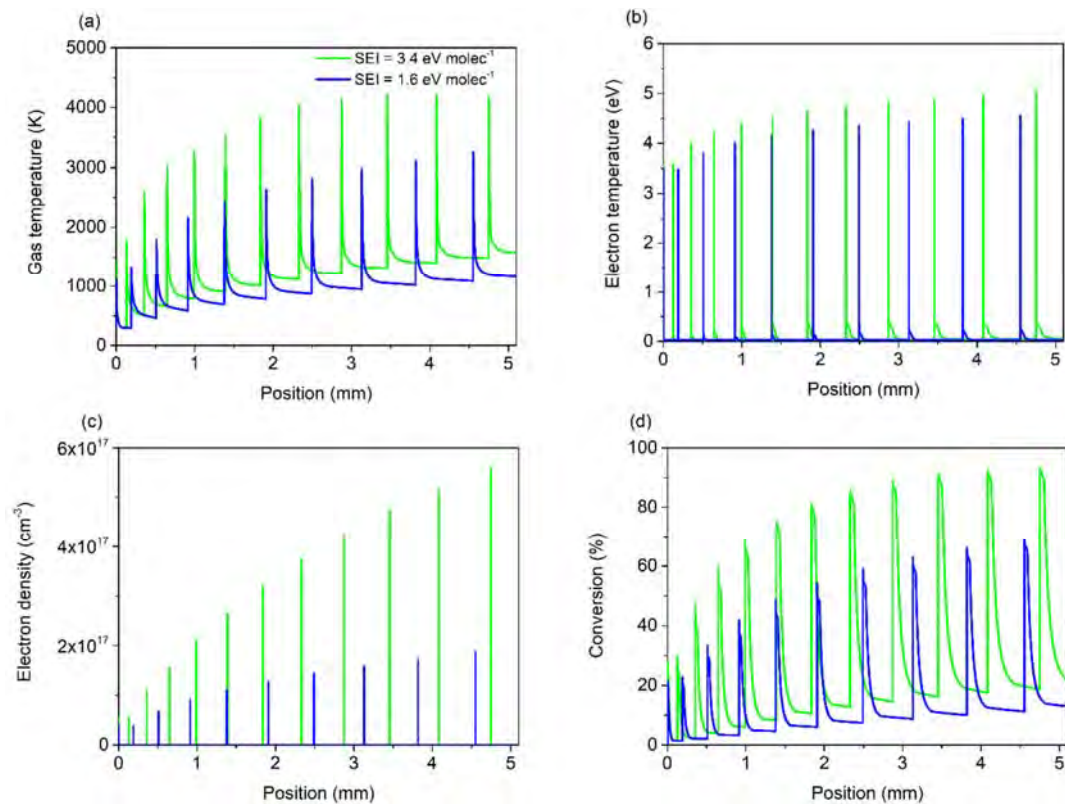


Figure S.2: Calculated gas temperature (a), electron temperature (b), electron density (c), and CO₂ conversion (d), as a function of travelled distance between HV pin electrode and grounded electrode, for two different SEI values (i.e. different from the SEI values in Figure 7 in the main paper, for extra information).

3. Details about the dissociation and formation mechanisms, and contribution of vibrational levels

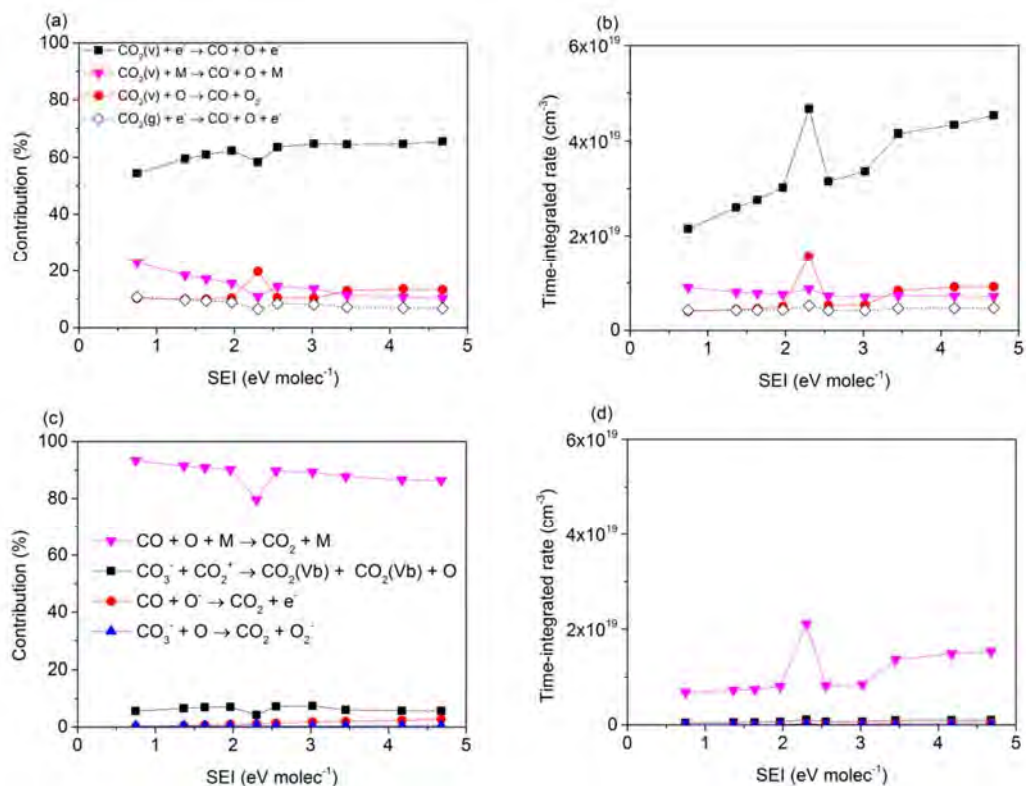


Figure S.3: Contribution of the most important dissociation (a) and formation (c) mechanisms of CO₂, and their corresponding time-integrated rates (b, d) as a function of SEI.

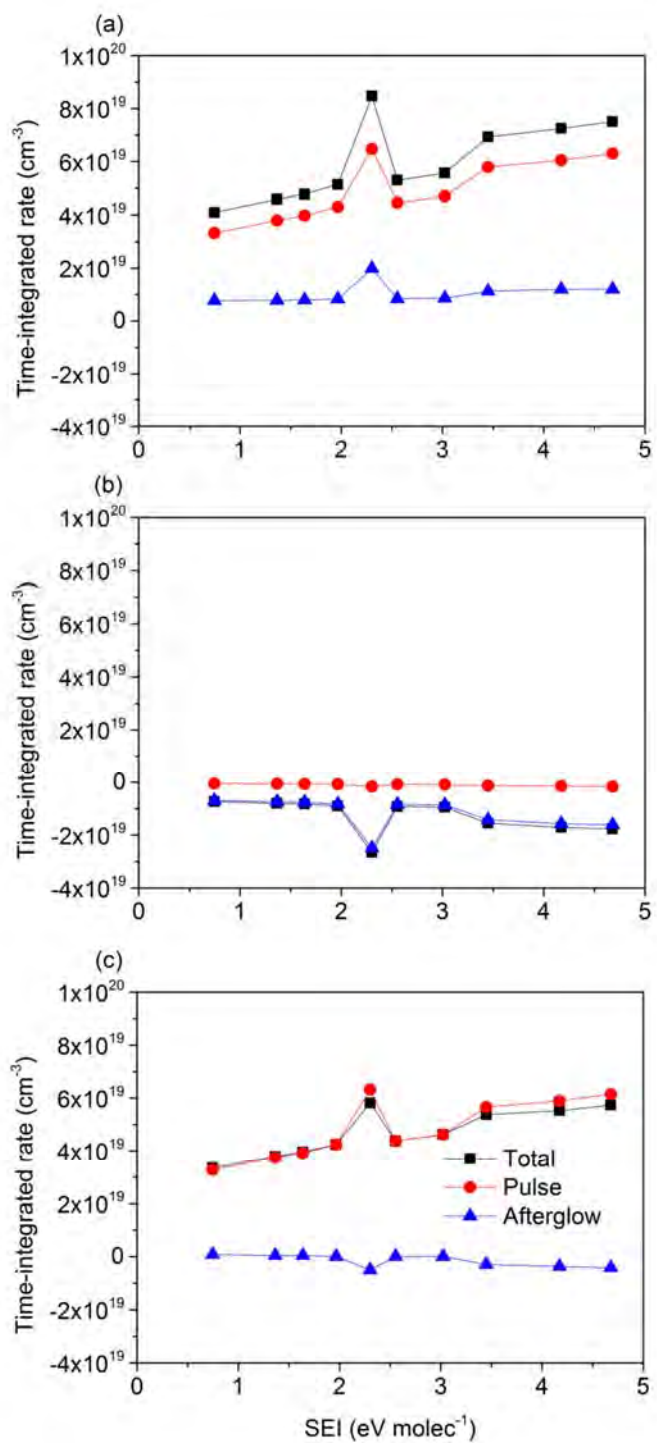


Figure S.4: Time-integrated rates of the overall dissociation (a), overall formation (plotted as negative values) (b), and the net dissociation of CO₂, as a function of SEI, for the pulse, afterglow and the sum of both (total), showing that the dissociation mainly takes place during the pulses, while net formation occurs during the afterglows.

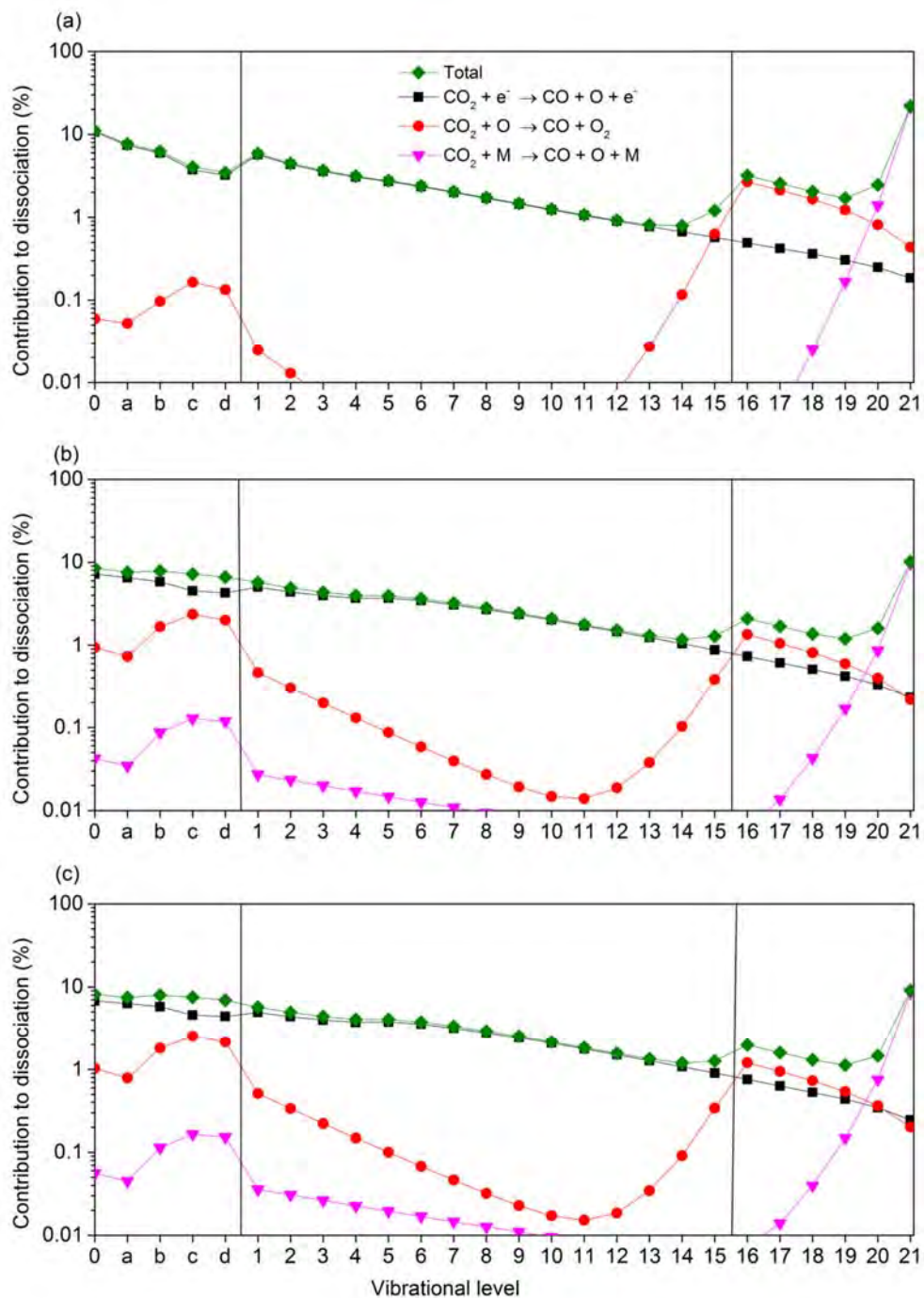


Figure S.5: Contribution of the CO₂ ground state and different vibrational levels to the total dissociation, as well as to the most important dissociation mechanisms, only accounting for the forward reactions, for different SEI values, i.e., 0.7 eV molec⁻¹ (a), 3.4 eV molec⁻¹ (b) and 4.7 eV molec⁻¹ (c).

4. Details about the effect of cooling

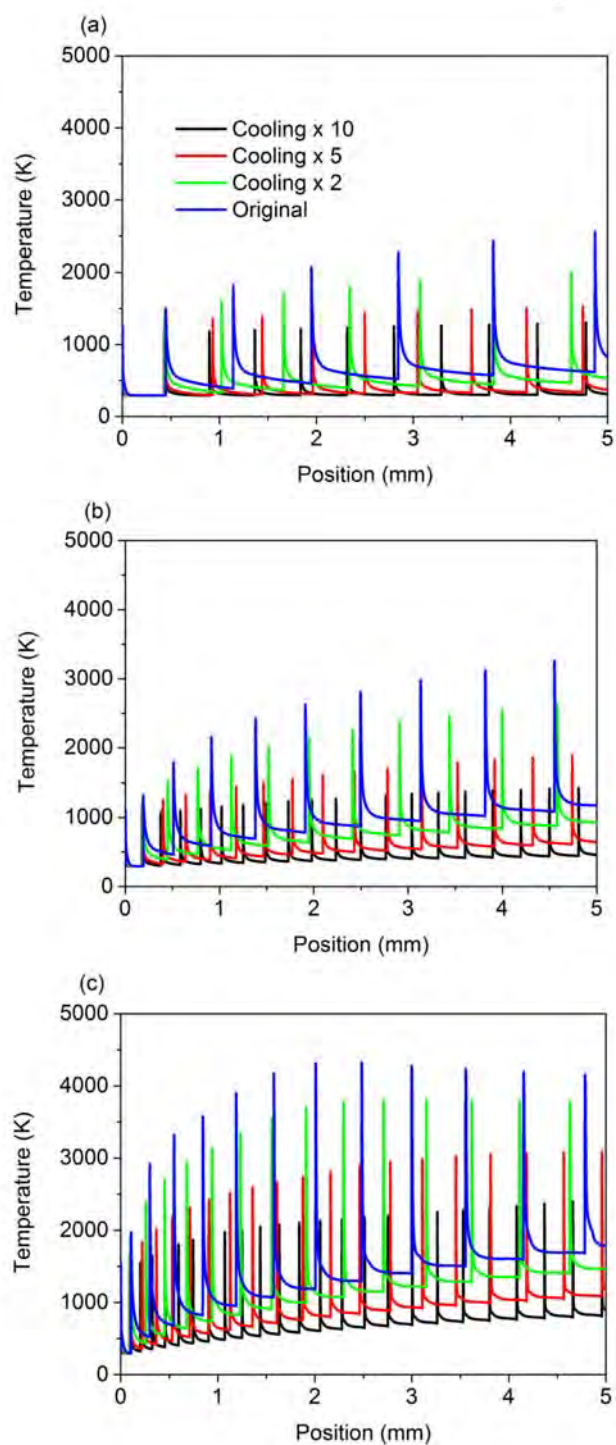


Figure S.6: Calculated gas temperature as a function of travelled distance between HV pin electrode and grounded electrode for different SEI values, i.e., 0.7 eV molec⁻¹ (a), 1.6 eV molec⁻¹ (b) and 4.7 eV molec⁻¹ (c), at different cooling rates.

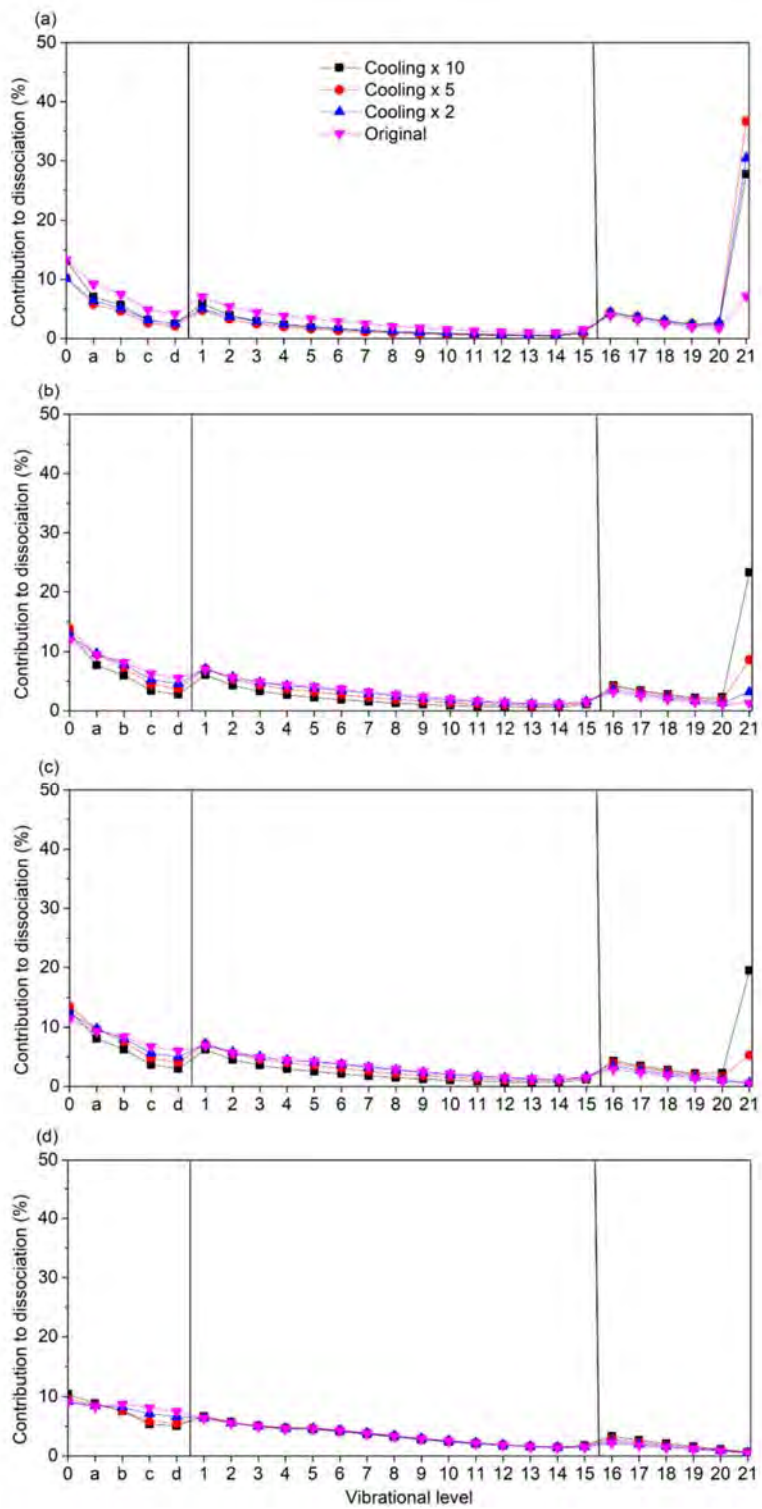


Figure S.7: Net contribution of the different CO_2 vibrational levels to the total dissociation, for different SEI values, i.e., $0.7 \text{ eV molec}^{-1}$ (a), $1.6 \text{ eV molec}^{-1}$ (b), $2.0 \text{ eV molec}^{-1}$ (c) and $4.7 \text{ eV molec}^{-1}$ (d), at different cooling rates.

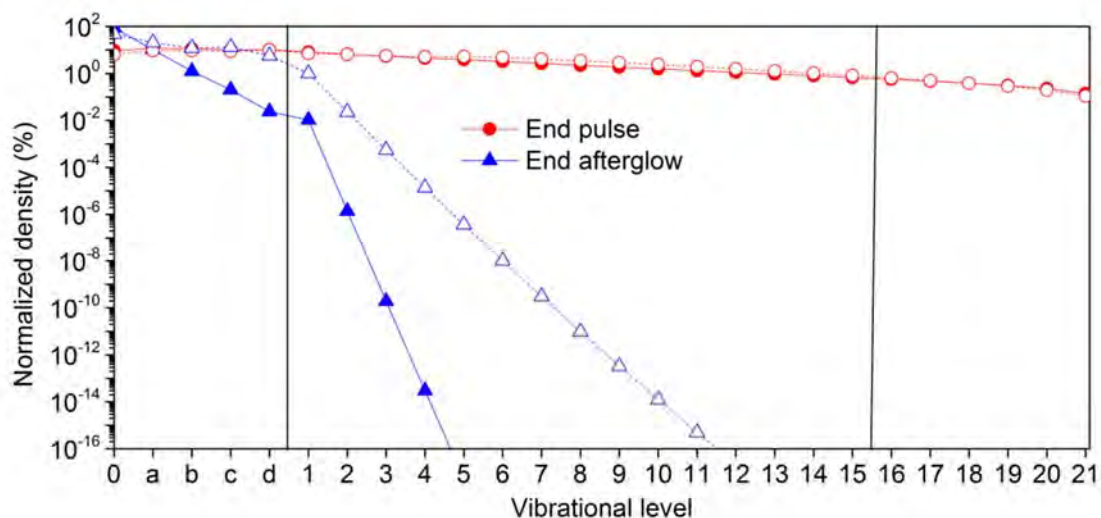


Figure S.8: Calculated VDFs at the end of the last pulse (10 ns) and at the end of the last afterglow, for $SEI = 1.6 \text{ eV molec}^{-1}$, in the original model (open symbols, dashed lines) and with a cooling rate times ten (solid symbols and lines). The VDFs at cooling rate times two and five at the end of the pulse are the same, and at the end of the afterglow, they lie in between the VDFs of the original model and of ten times higher cooling rate.

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