

# Fluid Modeling of the Plasma-Assisted Conversion of Greenhouse Gases to Value-Added Chemicals in a Dielectric Barrier Discharge

Proefschrift voorgelegd tot het behalen van de graad van doctor  
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te verdedigen door

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Antwerpen



Universiteit Antwerpen

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Greenhouse Gases to Value-Added Chemicals in a  
Dielectric Barrier Discharge**

**Fluid Modelling van de plasma-geassisteerde omzetting  
van broeikasgassen naar chemicaliën met toegevoegde  
waarde in een diëlektrische barrière ontlading**

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**Christophe DE BIE**

Promotor: prof. dr. Annemie Bogaerts

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# Chapter 1

## Introduction

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Socially, environmentally and economically a growing demand is being imposed for sustainability in the way energy resources are utilized. A global sustainable energy strategy that meets the increasing demand is based on an improvement of the energy efficiency of the current technologies and a more intensifying diversification of the energy resources with a huge preference for lower carbon resources.

## 1.1. Global Energy Demand

In 1974 the International Energy Agency (IEA) was established to promote energy security amongst its member countries (Belgium is a founding member) through collective response to physical disruptions in oil supply, and to provide authoritative research and analysis on ways to ensure reliable, affordable and clean energy for its 29 member countries and beyond.<sup>1</sup> The IEA annually publishes a World Energy Outlook which presents updated projections for the evolution of the global energy system, as well as detailed insights on the prospects for fossil fuels, renewables, the power sector and energy efficiency and analysis on trends in CO<sub>2</sub> emissions and fossil-fuel and renewable energy subsidies. The World Energy Outlook reports of 2014<sup>2</sup> and 2015<sup>3</sup> state that the energy use worldwide is set to grow by one-third to 2040, driven primarily by India, China, Africa, the Middle East, Southeast Asia and Latin America.

Pledges made prior to the 21<sup>st</sup> Conference of the Parties to the United Nations Framework Convention on Climate Change (COP21/CMP11; November-December, 2015) indicate that future energy policy intentions should result in a boost to lower-carbon fuels and technologies worldwide. As a result it is expected that the share of non-fossil fuels will increase from 19% of the global mix today to 25% in 2040. Therefore, the world's energy supply mix will be divided into four almost-equal parts by 2040: oil, gas, coal and low-carbon sources.<sup>3</sup> Although the demand for all fossil fuels is still increasing, natural gas, which is the least-carbon intensive, is the only one that sees its share rise by 2040. For instance, the share of oil will decrease from 34% in 2007 to 25% in 2040 and also the future use of coal, which resources are

abundant and which supply is secure, will be constrained if the global policy is to reduce the emission of carbon dioxide.<sup>2-4</sup>

A similar story can be found in the 23<sup>rd</sup> edition of the World Energy Resources Survey published in 2013 by the World Energy Council.<sup>5</sup> Formed in 1923, the Council is the UN-accredited global energy body, representing the entire energy spectrum, with more than 3000 member organizations located in over 90 countries and drawn from governments, private and state corporations, academia, NGOs and energy-related stakeholders.<sup>6</sup>

Globally, fossil fuel resources are still plentiful and will last for decades, but it becomes more difficult to recover them and there can be no guarantee that they will be exploited fast enough to meet the level of demand. The availability of energy resources is, however, of paramount importance to the society. Access to reliable, affordable commercial energy provides the basis for heat, light, mobility, communications and agricultural and industrial capacity in modern society and in this way energy stipulates the degree of civilization.<sup>7</sup> Besides, the transition of the energy market towards lower-carbon resources, also an enhancement in energy efficiency is very important in order to limit the world energy demand.

## **1.2. Reducing Greenhouse Gas Emissions**

Furthermore, the recovery, production and use of fossil fuels are accompanied by the emission of greenhouse gases and contribute in this way to global warming. Climate change due to anthropogenic greenhouse gas emission is a growing concern for the global society. Anthropogenic

greenhouse gas emissions have increased since the pre-industrial era and have led to atmospheric concentrations of carbon dioxide (CO<sub>2</sub>), methane (CH<sub>4</sub>) and nitrous oxide (N<sub>2</sub>O) that are unprecedented in at least the last 800,000 years. It is extremely likely that these greenhouse gas emissions have been the dominant cause of the observed global warming since the mid-20th century.<sup>8</sup>

Following the Synthesis Report on Climate Change<sup>8</sup> published by the Intergovernmental Panel on Climate Change<sup>9</sup> in 2014, a new international agreement on climate change was made at the 21st Conference of the Parties to the United Nations Framework Convention on Climate Change (COP21/CMP11; November-December, 2015), to keep global warming below 2°C. At the World Economic Forum 2016 Annual Meeting in Davos, Switzerland (January 2016), this new commitment to action on climate change was pointed out as one out of 10 key global challenges that matter to the world, stated as “Climate change: can we turn words into action?”. The International Council of Chemical Associations (ICCA)<sup>10</sup>, representing chemical manufacturers all over the world, and its member organization, i.e., the European Chemical Industry Council (Cefic)<sup>11</sup>, which is the main European trade association for the chemical industry, strongly endorsed the international efforts to reach a binding global agreement at COP21. In the last decades, the chemical industry made its efforts to reduce greenhouse gas emissions, and today the European chemical industry uses less than half the energy it used back in 1990. Thus, its greenhouse gas emissions have fallen by 54% on 1990 levels, while its production grew by 70%. ICCA and Cefic believe that the chemical industry is also a pillar of tomorrow’s low-carbon economy

by developing innovative solutions, which will be crucial to combating climate change.<sup>10-11</sup>

1.3. Natural Gas - Methane (CH<sub>4</sub>)

In a world in which fossil fuels make the day, natural gas has the most significant growth potential and so it becomes more and more an interesting alternative for crude oil as feedstock for the chemical industry. Table 1 gives an overview of the benefits and drawbacks of natural gas as an energy resource. Natural gas is currently the third most used energy resource in the world after crude oil and coal,<sup>2-3</sup> but the lifetime of gas resources is much longer than for oil and its lower carbon content makes natural gas the cleanest of all fossil-based fuels. Therefore, natural gas will continue making significant contribution to the world energy economy as it also is a flexible fuel. However, the exploration, development and transport of gas usually require significant upfront investment. In addition to power generation, natural gas is expected to play an increasing role as a transport fuel.<sup>5</sup>

Table 1. The benefits and drawbacks of natural gas.

(adopted from WER 2013 Survey<sup>5</sup>)

Benefits	Drawbacks
Cleanest of fossil fuels	Fields increasingly off-shore and in remote areas
Flexible and efficient fuel for power generation	High upfront investment requirement for transport and distribution system
Increasing proved reserves (reassessments and shale gas)	Increasingly long supply routes and high cost of infrastructure

Natural gas is a mixture of hydrocarbons, of which methane ( $\text{CH}_4$ ) is the principal component. Methane, which is also an important greenhouse gas, is an odorless, colorless, non-toxic gas which is lighter than air. It is currently mainly being used for home and industrial heating and for the generation of electrical power. On the other hand, methane is a greatly underutilized resource for the production of chemicals and liquid fuels, mainly because it is one of the most stable molecules.<sup>12</sup> Direct synthesis of hydrocarbons starting from methane is not yet feasible and the conventional indirect methods for partial and total oxidation of methane have poor yields and require high amounts of energy.<sup>13</sup> The utilization of natural gas as a chemical resource is currently limited to the production of synthesis gas (i.e., syngas:  $\text{H}_2 + \text{CO}$ ) by steam reforming, which is a highly energy-intensive process.<sup>14</sup>

A sustainable process for the conversion of the abundant methane reserves into more value-added chemicals and fuels is therefore renowned as a challenge for the 21st century.<sup>12</sup> More in particular, the development of a process for the direct synthesis of higher hydrocarbons and oxygenates from methane in an energy-efficient way towards economy and environment would offer significant benefits, because this will circumvent the very expensive syngas step.<sup>15</sup>

## 1.4. Carbon Dioxide (CO<sub>2</sub>)

Carbon Dioxide (CO<sub>2</sub>), naturally present in the atmosphere as part of the natural circulation of carbon among the atmosphere, oceans, soil, plants, and animals, and thus being a vital gas for life on earth, is the primary greenhouse gas emitted through human activities.<sup>16</sup> It is a very stable molecule that requires a lot of energy to be activated for the majority of synthetic routes to produce chemicals. Therefore, a first objective in the mitigation of CO<sub>2</sub> emissions is the process of Carbon Dioxide Capture and Storage (CCS), as pointed out in a special report published in 2005 by the Intergovernmental Panel on Climate Change.<sup>17</sup> Nowadays, it is clear that aside from the reduction of CO<sub>2</sub> emissions to the atmosphere and the use of CCS for this purpose, also the energy efficient utilization of (captured) CO<sub>2</sub>, as an important carbon resource to create products, will be a crucial step in order to achieve an economically viable low-carbon economy.

In 2011 Damiani et al.<sup>18</sup> published a perspective concerning the United States Department of Energy's R&D program, to reduce greenhouse gas emissions through the beneficial use of CO<sub>2</sub>. A vision for smart CO<sub>2</sub> transformation in Europe, enabling the European industry to become more resource-efficient, sustainable and competitive, was published in November 2015. This vision document, designed as part of the Smart CO<sub>2</sub> Transformation (SCOT) project, is a collaborative European project focused on accelerating the market development of CO<sub>2</sub> utilization and supported by funding from the European Seventh Framework program.<sup>16</sup> Both documents stress the potential of CO<sub>2</sub> as a carbon resource and the importance of the transition into a world where CO<sub>2</sub> is used as feedstock for making many products. Damiani et al.<sup>18</sup> state the benefits of CO<sub>2</sub> utilization as follows: it can generate



revenue to offset capture costs associated with CCS, it contributes to CO<sub>2</sub> emissions reduction, and it reduces the demand for fossil fuels. In the SCOT vision document,<sup>16</sup> also three main reasons are listed why Europe should focus on CO<sub>2</sub> utilization: (i) it can be one of the major growth areas in Europe's future low-carbon circular economy, (ii) it can help to facilitate Europe's energy transition and (iii) it can contribute to achieving Europe's aims for decreasing carbon emissions. The goal is to identify and develop a range of novel technologies that can beneficially use CO<sub>2</sub>. It is clear from both documents that the use of CO<sub>2</sub> for chemical production is one of the priority research areas concerning CO<sub>2</sub> utilization.

Today, CO<sub>2</sub> utilization is mainly limited to the direct use, i.e. without a conversion step, as an inert agent for food packaging, in carbonated drinks, in refrigeration systems, in fire extinguishers, as a solvent, and for enhanced oil recovery (particularly in the United States), as well as the indirect use for the chemical production of mainly urea, a small amount of methanol and an even smaller amount of a wide variety of other products.<sup>16-18</sup> Ongoing research on the conversion of CO<sub>2</sub> in value-added chemicals is primarily focusing on the formation of carbon monoxide (CO), methanol, polymers, urea, carboxylates, carbonates, olefins, etc.<sup>16</sup> Figure 1 gives an overview of the use of CO<sub>2</sub> and the research areas supported by the United States Department of Energy. In order to convert CO<sub>2</sub> into products, an energy source, such as heat or electricity, or material inputs, such as fly ash, hydrogen or epoxides, is required.<sup>16</sup> To become of added value, it is crucial that new CO<sub>2</sub> utilization processes have a lower carbon footprint than their equivalent classical processes using fossil fuel routes for the production of the same product.

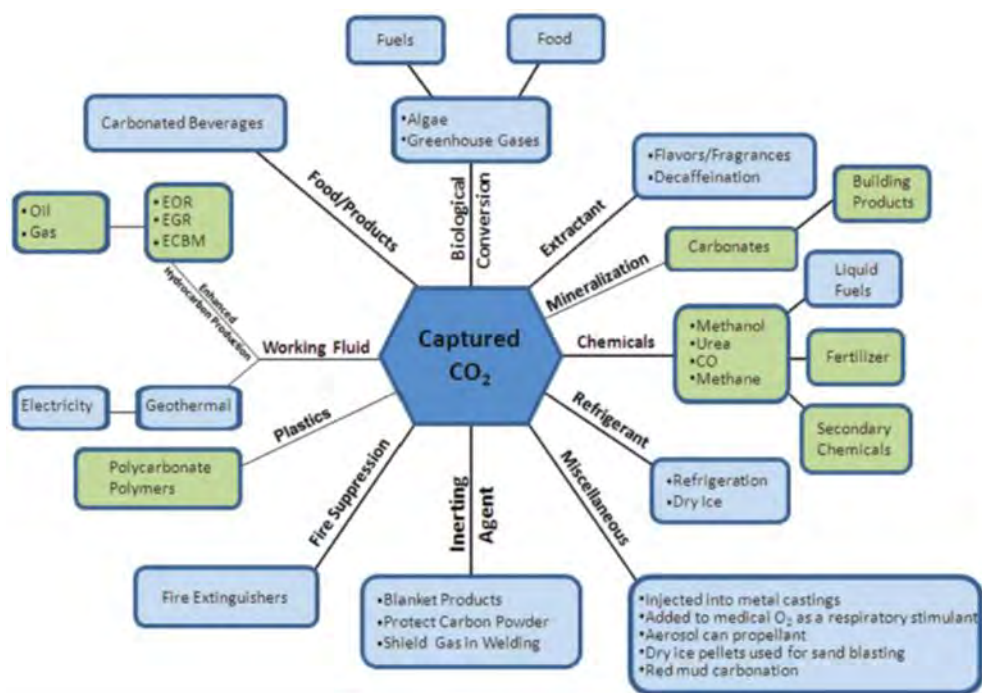


Figure 1. Overview of the use of CO<sub>2</sub>. The research areas supported by the United States Department of Energy are shown in green.<sup>18</sup>

## 1.5. Value-Added Chemicals

The value-added chemicals of interest in this research are higher hydrocarbons, such as ethane (C<sub>2</sub>H<sub>6</sub>), ethylene (C<sub>2</sub>H<sub>4</sub>), acetylene (C<sub>2</sub>H<sub>2</sub>), propane (C<sub>3</sub>H<sub>8</sub>) and Propylene (C<sub>3</sub>H<sub>6</sub>), syngas, i.e., a mixture of carbon monoxide (CO) and hydrogen gas (H<sub>2</sub>), also called synthesis gas, as well as oxygenates, such as methanol (CH<sub>3</sub>OH) and formaldehyde (CH<sub>2</sub>O).

C<sub>2</sub>H<sub>6</sub> is mainly used in the chemical industry as a feedstock for the production of C<sub>2</sub>H<sub>4</sub>, which is considered as the most important feedstock in the chemical industry.<sup>19</sup> C<sub>2</sub>H<sub>4</sub> is mainly used for the formation of polyethylenes, which are the world's most widely used plastics. Besides, it

also forms the basis for the formation of ethylene oxide, which is used in surfactants, and for the formation of ethylene glycol, which is applied as automotive antifreeze, as well as for many other applications.  $C_2H_2$  is mainly utilized as a fuel source and as a chemical building block for the formation of ethylene and different polymerization products, which are applied in the plastic industry.  $C_3H_8$  is the main component of liquefied petroleum gas (LPG), which is used as vehicle fuel.  $C_3H_6$  forms the basis for the formation of polypropylene, which is typically used in the manufacturing of packaging and textiles.

Syngas is used as a fuel source or as an intermediate for the production of other chemicals. Classical processes, including steam reforming, partial oxidation and  $CO_2$  reforming of methane, typically produce syngas with  $H_2/CO$  molar ratio greater than 3, less than 2 and less than 1, respectively.<sup>20-21</sup> The  $H_2/CO$  molar ratio from steam reforming ( $>3$ ) is much higher than that required by the stoichiometry for many synthesis processes. A low  $H_2/CO$  molar ratio is desirable for many industrial synthesis processes, such as the Fischer Tropsch synthesis or the synthesis of valuable oxygenated chemicals. A  $H_2/CO$  ratio of about 2 is preferred for the formation of methanol out of syngas.<sup>22</sup> Methanol can even be produced from syngas with a  $H_2/CO$  molar ratio as low as 0.5, when the system can simultaneously carry out methanol synthesis and the water-gas-shift reaction.<sup>20-21</sup>

$H_2$  is mainly used for the processing of fossil fuels, the production of ammonia and methanol, and as fuel in fuel cells. Furthermore, it is used in the production of carbon steels, special metals and semiconductors. In the electronics industry,  $H_2$  is employed as a reducing agent and as a carrier gas.<sup>23</sup>

CO is used to make a variety of chemicals such as acids, esters and alcohols, as well as for the reduction of ores and in the manufacture of metal carbonyls.<sup>23</sup>

Methanol is a primary liquid petrochemical, which is of great importance in the chemical and energy industries, because it can be easily stored and transported.<sup>24</sup> Methanol is one of the most commonly used raw materials in the chemical industry. More than one-third of it is used in the production of formaldehyde; the rest is mainly utilized to produce acetic acid and gasoline octane improvers. Additionally, the direct use of methanol as fuel in internal combustion engines and fuel cells opens up the possibility of methanol powered vehicles and consumer electronics.<sup>25</sup> Formaldehyde is a common building block for the synthesis of more complex compounds, which are used in a wide range of products.



# Chapter 2

## Plasma-Assisted Gas Conversion

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The major difficulty for the direct conversion of methane and carbon dioxide into value-added chemicals is that both are very stable molecules that require a large amount of energy for activation of the stable C-H and C-O bonds, respectively. Conventional methods, which make use of a high temperature and pressure and a noble catalyst, require high amounts of energy. In the last decades, there is an increasing interest in using plasma technology for gas conversion. Atmospheric pressure non-thermal low-temperature plasmas can offer a distinct advantage, because they enable in a unique way gas phase reactions at ambient conditions.

## 2.1. What is a Plasma?

Plasmas are ionized gases. Hence, they consist of positive (and negative) ions and electrons, as well as neutral species. The ionization degree can vary from 100% (fully ionized gases) to very low values (e.g.  $10^{-4}$ – $10^{-6}$ ; partially ionized gases).<sup>26</sup> A plasma is generated by supplying energy to a neutral gas, causing the formation of charge carriers. The charged species are considered to be balanced in the bulk of the plasma, giving plasmas the characteristic of quasi-neutrality. These unique properties make that the plasma state is often called the 'fourth state of matter', next to solid, liquid and gas. The name 'plasma' was introduced in 1929 by Irving Langmuir who chose this name, because the multi-component, strongly interacting ionized gas reminded him of blood plasma.<sup>27</sup>

Almost all visible matter in the universe is in the plasma state. Examples of natural plasmas are the stars, the solar wind, the earth's ionosphere, the aurora borealis and lightning. Besides these astropasmas, two main groups of laboratory plasmas can be distinguished, i.e. the high-temperature or fusion plasmas, and the so-called low-temperature plasmas or gas discharges. A subdivision can be made between plasmas which are in thermal equilibrium and those which are not in thermal equilibrium. Thermal plasmas are characterized by the fact that the temperature of all species in the plasma is the same. High temperatures are required to form these equilibrium plasmas, typically ranging from 4000 K to 20 000 K.<sup>26</sup> In non-thermal plasmas the temperature of the electrons is much higher than that of the heavy particles (ions, atoms, molecules). The most commonly used method to generate and sustain a low-temperature plasma is by applying a sufficiently high electric field to a neutral gas, which partially breaks it down, turning some atoms or

molecules into positive ions and generating free electrons. These charge carriers are accelerated by the electric field, and new charged particles may be created when these charge carriers collide with gas molecules or with the electrodes. The resulting avalanche of charged particles is eventually balanced by charge carrier losses, creating a steady-state plasma.<sup>28</sup>

There exists a wide variety of non-thermal gas discharge plasmas, each with its own characteristics and employed in a large range of applications. Based on the temporal behavior of the sustaining electric field, gas discharges can be classified as direct current (dc), alternating current (ac) or pulsed discharges.<sup>28</sup> An example of a non-thermal ac discharge is the dielectric barrier discharge (DBD), which is the type of plasma under study in this dissertation and will therefore be explained in more detail in the next section. An overview of the most important gas discharge plasmas and their applications can be found in Bogaerts et al.<sup>26</sup> and Conrads et al.<sup>28</sup>. Table 2 shows the most important gas discharges along with their parameters and possible applications.



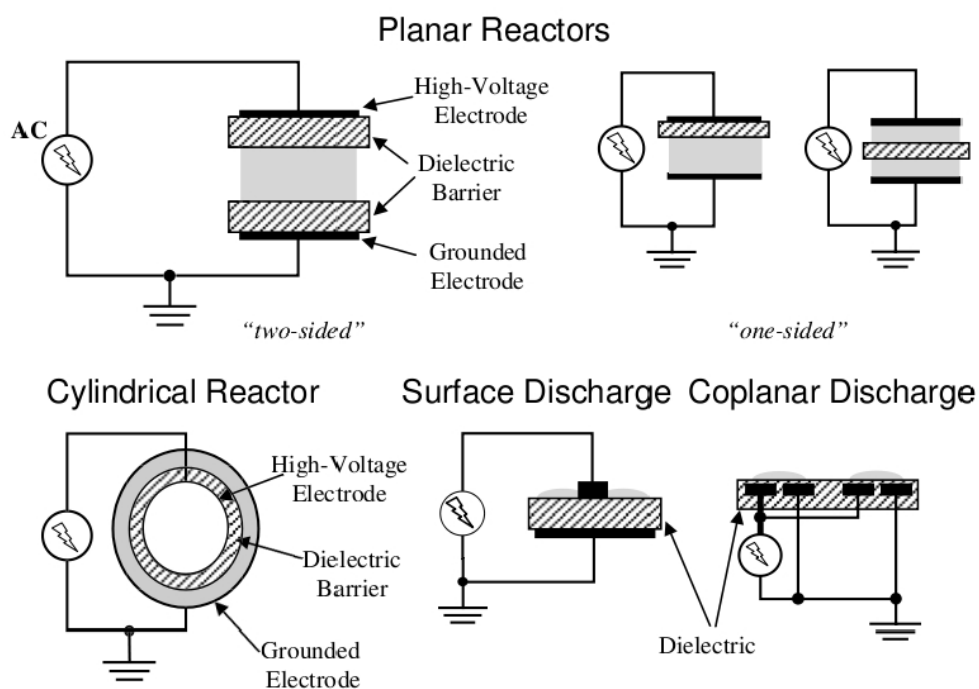
**Table 2. Plasma sources and their parameters.**(modified from Conrads et al.<sup>28</sup>)

Physics	Pressure (mbar)	$n_e$ ( $\text{cm}^{-3}$ )	$T_e$ (eV)	Application
Dielectric barrier discharge	1000	$10^{14}$	5	Ozone, microelectronics, chemistry
Corona	1000	$10^{13}$	5	Ozone, chemistry
Microwave	10-1000	$10^{13}$	1-2	Chemistry, microelectronics
Spark	$1000-10^4$	$10^{17}$	1	Chemistry, water treatment
Gliding arc	1000	$10^{12}-10^{17}$	1	Chemistry
Nanosecond pulsed	1000	$10^{12}$	5	Chemistry
DC glow	$10^{-3}$ -100			
Cathode region			100	Sputtering, deposition
Negative glow		$10^{12}$	0.1	Chemistry, radiation
Positive column		$10^{11}$	1-10	Radiation
Hollow cathode	$10^{-2}$ -800	$10^{12}$	0.1	Radiation, chemistry
Magnetron	$10^{-3}$			Sputtering
RF capacitive	$10^{-3}$ -10	$10^{11}$	1-10	Microelectronics, sputtering
RF inductive	$10^{-3}$ -10	$10^{12}$	1	Microelectronics, etching
Electron beam	$10^{-2}$ -1	$10^{12}$	1	Microelectronics

## 2.2. Dielectric Barrier Discharge

A dielectric barrier discharge (DBD) or so-called silent discharge is an electrical discharge that is generated between two electrodes of which at least one is covered with a dielectric material made of glass, quartz, alumina, etc. The gap between the two electrodes is typically a few millimeters. An ac voltage with an amplitude from 1 kV to 100 kV and a frequency of a few Hz to MHz is usually applied to this kind of discharges. Typical electrode

arrangements of planar and cylindrical DBDs are shown in Figure 2. For gas conversion purposes mostly a cylindrical reactor is used. A DBD has the advantage, unlike other non-equilibrium discharges, that it can be operated at atmospheric pressure, while remaining at ambient temperature.



**Figure 2. Typical electrode arrangements of barrier discharges.<sup>29</sup>**

The first experimental investigations with a DBD were reported in 1857 by Werner von Siemens. The research was mainly focused on the generation of ozone by blowing air or oxygen through a narrow annular gap between two coaxial glass tubes in which a DBD was maintained by an alternating electric field of sufficient amplitude. The novelty of this setup was that the electrodes, which were made of tinfoil, were not in direct contact with the plasma, which

considerably increased their lifetime. In the following decades, ozone and nitrogen oxide formation in DBDs became an important research topic.<sup>30</sup>

Today, these silent discharge ozonizers are effective tools, and a large number of ozone installations based on plasma technology are being used worldwide for water treatment. DBDs are nowadays also used to pump CO<sub>2</sub> lasers, to generate excimer radiation in the UV and VUV spectral regions, in various thin-film deposition processes, and for plasma display panels. In recent years, DBDs are increasingly being used as reactor set-up for gas treatment or gas conversion, which is the objective of this dissertation. Detailed information on the history of a DBD and the wide variety of applications for which a DBD is used can be found in literature.<sup>26, 28, 30-36</sup>

### 2.3. Breakdown: The Initiation of Reaction Kinetics

In a DBD reactor typically operating at atmospheric pressure, a large number of short-living current filaments, so-called microdischarges, which are randomly distributed both in time and in space, appear during breakdown.<sup>37</sup> It can be presumed that the plasma is enclosed in the volume surrounded by these microdischarges. Three separate steps can be distinguished during the life cycle of one such filament: (i) the formation of the discharge, i.e., the electrical breakdown, (ii) the subsequent current pulse or transport of charge across the gap, and (iii) simultaneously the excitation of the atoms and molecules present, and thus the initiation of the reaction kinetics. The durations of these three steps are of different orders of magnitude. The local breakdown is usually completed within nanoseconds, the current transport takes typically 1-100 ns, while the chemistry can last from nanoseconds to

seconds.<sup>31</sup> Approximate time-scales for the different processes involved are given in Figure 3.

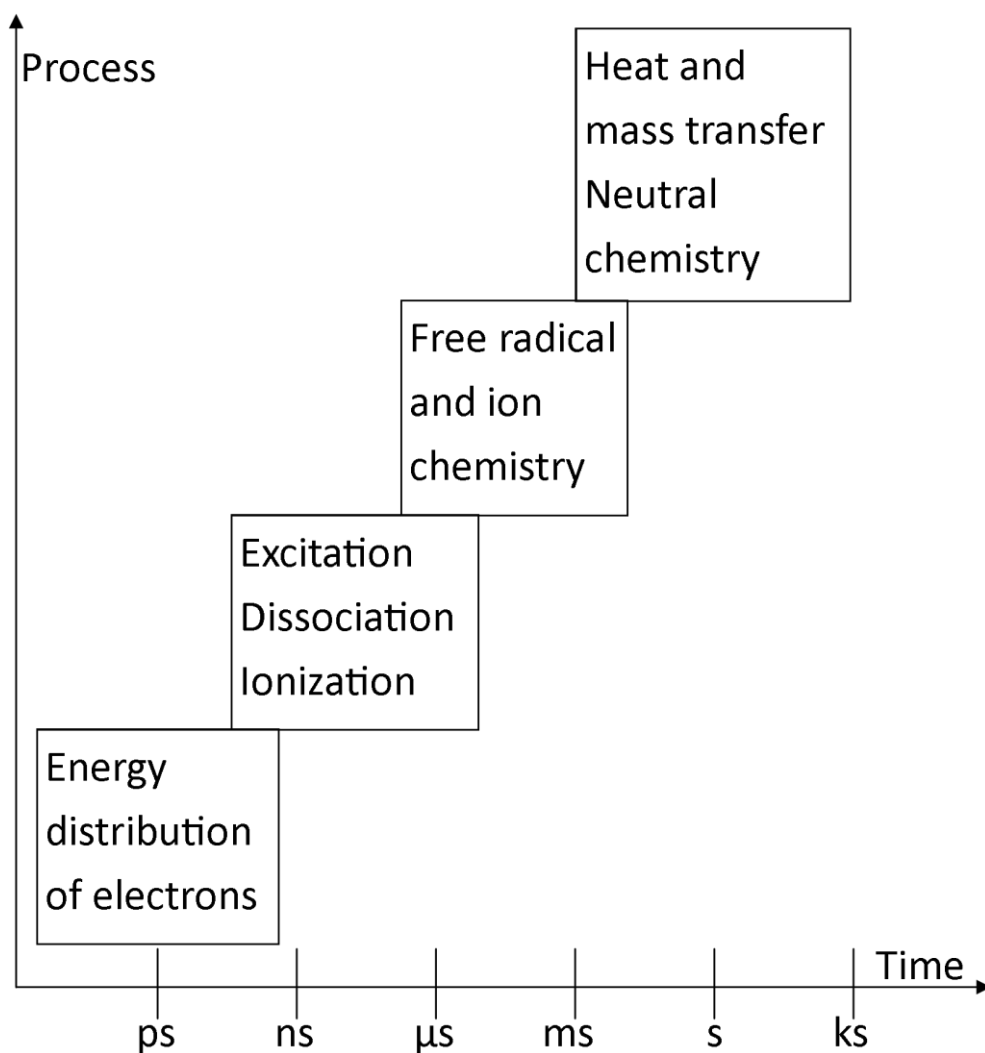
By applying an increasing voltage to the electrodes, breakdown is induced once the electric field inside the gap exceeds the corresponding reduced Paschen field of the gap. The Paschen voltage is given by the smallest constant voltage needed to initiate breakdown in the gap. This breakdown voltage depends on the gas composition and on the reactor configuration, i.e. the gas pressure and the gap width. The reduced Paschen field is obtained by dividing the Paschen voltage by the product of the gas pressure and the gap width.<sup>31</sup>

Each microdischarge has an almost cylindrical plasma channel and typically a diameter of the order of some 100  $\mu\text{m}$ . They are usually very short-lived, on the order of 100 ns or less. Both the diameter and the duration depend upon the gas used and the pressure.<sup>31</sup> The number of microdischarges is proportional to the voltage applied on the electrodes.<sup>37-38</sup> The current flows entirely within the filaments and is limited by the dielectric barrier(s) between the electrodes. Thus, the dielectric serves a dual purpose. It limits the amount of charge and energy imparted to an individual microdischarge and, at the same time, it distributes the microdischarges over the entire electrode area. Typically the current density in the filaments is 100–1000  $\text{A cm}^{-2}$ , the electron density is  $10^{14}$ – $10^{15} \text{ cm}^{-3}$ , and typical electron energies are in the range of 1–10 eV.<sup>28, 30, 39</sup> Typical charges transported by individual microdischarges are of the order of nC, and typical energies of the order of  $\mu\text{J}$ .<sup>40</sup> Over long time periods, the microdischarges, which are randomly distributed by the way they are initiated, will thus evenly fill the available volume.

The exchange of energy between the accelerated electrons and the atoms and molecules occurs within the microdischarges. The fairly energetic

electrons collide with the gas molecules and excite them and thus transform some of their kinetic energy into internal energy of the gas molecules. Due to the high electron energy, this energy exchange can be very efficient. It is not unusual that 90% of the kinetic energy or more is transformed into stored energy.<sup>31</sup> Elastic losses are therefore very low, and initially very little energy is lost as heat.<sup>31</sup> The excited species formed in the microdischarge filaments can diffuse into the regions between the filaments, which are free of charged particles, and initiate the chemical reactions (see below) before the next discharge strikes at the same location. This separation of electron-producing regions and chemically active regions can be very beneficial.<sup>39</sup>

More information about the formation of these microdischarges and the characteristics of a DBD can be found in literature.<sup>28, 30-31, 34, 37, 39-41</sup>



**Figure 3. Time-scale of the relevant processes of a filamentary DBD.**

(modified from Wagner et al.<sup>29</sup>)

## 2.4. The Plasma Chemistry

The excited molecules can now, due to their high internal energy, either dissociate or initiate other reactions.<sup>39</sup> The main types of reactions occurring in the plasma are listed in Table 3, for an arbitrary gas (called  $A_2$ ). Different plasma activation mechanisms cause vibrational and electronic excitation, as well as ionization and dissociation of species, and in this way gas conversion processes are induced. Reactive species in the discharge (free radicals, electrons, ...) will cause decomposition of the molecules, initially present in the gas mixture, and afterwards recombination will lead to the formation of value-added and/or less hazardous end products. Every reaction is characterized by a few main characteristics, such as the reactants, the products, the pressure, the temperature, the heat of the reaction, and the rate coefficient.<sup>39</sup>

These plasma chemistry processes, taking place at atmospheric pressure and ambient temperature, make a DBD reactor of interest for the conversion of greenhouse gases to higher hydrocarbons, oxygenates and syngas. Nowadays a lot of research is carried out on the use of a DBD for the conversion of  $CH_4$  and  $CO_2$ , as will be clear from the next chapters in this dissertation. However, there are still a lot of issues open for discussion. More specifically, a lot of research work still has to be performed with respect to improving the energy efficiency and the selectivities of the end products, in order to come to a sustainable industrial process, which is competitive with currently existing or other emerging technologies. In order to optimize such a process to become competitive, it is essential to understand the huge underlying plasma chemistry acting in the conversion processes. This is exactly the purpose of this PhD dissertation, where we try to obtain a better insight in

the plasma chemistry, by means of fluid modeling, as elaborated in the next chapter.

**Table 3. Overview of the main plasma reactions for an arbitrary gas, called  $A_2$ .**

(adopted from Eliasson et al.<sup>39</sup>)

<b>Electron/Molecular Reactions</b>	
Excitation	$e^- + A_2 \rightarrow A_2^* + e^-$
Dissociation	$e^- + A_2 \rightarrow 2 A + e^-$
Attachment	$e^- + A_2 \rightarrow A_2^-$
Dissociative Attachment	$e^- + A_2 \rightarrow A^- + A$
Ionization	$e^- + A_2 \rightarrow A_2^+ + 2 e^-$
Dissociative Ionization	$e^- + A_2 \rightarrow A^+ + A + 2 e^-$
Recombination	$e^- + A_2^+ \rightarrow A_2$
Detachment	$e^- + A_2^- \rightarrow A_2 + 2 e^-$
<b>Atomic/Molecular Reactions</b>	
Penning Dissociation	$M^* + A_2 \rightarrow 2 A + M$
Penning Ionization	$M^* + A_2 \rightarrow A_2^+ + M + e^-$
Charge Transfer	$A^\pm + B \rightarrow B^\pm + A$
Ion Recombination	$A^- + B^+ \rightarrow AB$
Neutral Recombination	$A + B + M \rightarrow AB + M$
<b>Decomposition</b>	
Electronic	$e^- + AB \rightarrow A + B + e^-$
Atomic	$A^* + B_2 \rightarrow AB + B$
<b>Synthesis</b>	
Electronic	$e^- + A \rightarrow A^* + e^-$ , $A^* + B \rightarrow AB$
Atomic	$A + B \rightarrow AB$





# Chapter 3

## Fluid Modeling: An Insight in the Plasma Chemistry

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Plasma modeling can offer the experimentalist the necessary information to understand the role of the different species in the immensity of chemical reactions taking place in the discharge gap. The aim of our research is to describe in detail the plasma chemistry in an atmospheric pressure DBD in different gas mixtures with  $\text{CH}_4$  and/or  $\text{CO}_2$ , by means of a 1D fluid model. More information about the fluid model applied for this research can be found in this chapter.

### 3.1. Motivation for Numerical Simulations

Experimental observations are the base for understanding natural phenomena. They lead to new theories and the discovery of proportionalities, which allows mathematical formulations of these theories. These descriptions can be tested and improved by additional observations up till the point where these observations become too difficult.<sup>27</sup> Obstacles for such observations are for example that the phenomenon happens too fast, or that the setup becomes too small or too large, or that the materials under study are very expensive or very dangerous, or that the phenomenon involves many different theoretical aspects at the same time, so that the link between theory and experiment is rather complicated.<sup>27, 42</sup>

Modeling or simulation of a phenomenon or experiment can offer here a solution to circumvent these issues. Models are used to theoretically interpret and predict experimental observations. In physics, the word “model” is used to indicate a system of equations, data, and assumptions, which gives a mathematical representation of all the major features of a certain physical phenomenon.<sup>42</sup> The equations used in the model can be solved exactly or numerically. The latter means that they have to be discretized in both space and time, so that by choosing an appropriate initial condition and by respecting the boundary conditions, the described system is recalculated again and again, so that it iteratively evolves into the desired converged solution. Both the exact and the numerical solutions of these equations have their advantages and disadvantages, but in general, numerical methods are increasingly being used, because they are able to describe enormously complex systems and they can be defined much more generally than the exact solutions.<sup>27</sup>

Also in the field of gas discharges and plasma technology numerical simulations are a useful tool to describe the discharge physics or the plasma chemistry. There exist various useful theoretical descriptions to describe the physics and chemistry in the gas discharges studied in this dissertation. Different possible simulation methods for this purpose, such as an analytical approach, a kinetic approach, a fluid model or a hybrid model, as well as their advantages and disadvantages, are discussed by Martens<sup>27</sup>. In order to describe the DBD plasma under study in this work, we decided to adopt a fluid model for the reasons given in next section.

### 3.2. The Fluid Approach

In a fluid model the various discharge species (electrons, molecules, radicals, ions) are described in terms of average, hydrodynamic quantities, such as density, momentum and energy.<sup>27</sup> The space and time variation of these quantities is described by fluid equations, which are derived by taking the velocity moments of the Boltzmann equation. The Boltzmann equation<sup>43</sup> describes the evolution of the density  $f(\vec{r}, \vec{v}, t)$  of a single particle species in the phase space spanned by configuration space  $\vec{r}$  and velocity space  $\vec{v}$ . Often the Boltzmann equation is written as:

$$\frac{\partial f}{\partial t} + \vec{v} \cdot \frac{\partial f}{\partial \vec{r}} + \vec{a} \cdot \frac{\partial f}{\partial \vec{v}} = \left( \frac{\partial f}{\partial t} \right)_c \quad (1)$$

where  $\vec{a}$  is the acceleration of the particle and  $(\partial f / \partial t)_c$  is the change of the distribution function  $f$  due to collisions.<sup>27</sup> More detailed information on the continuity equations for density, momentum and energy obtained from the Boltzmann equation is given below. Surface processes are accounted for in

the boundary conditions of the fluid equations. Usually the fluid equations are coupled to macroscopic Maxwell equations, such as Poisson's equation, which describes the effect of space charge on the electric field. In this way, a complete, self-consistent description of the discharge is obtained. Note that the assumptions made in this approach can only be applied over a limited range of discharge conditions. Detailed information on this can be found in Hagelaar<sup>42</sup>. However, for the DBD under study, the fluid approach is very useful and quite reliable. A great advantage of fluid models is that they can simulate the time evolution of a discharge in one or two spatial dimensions within a manageable period of computation time, i.e., a few hours, even for a complex plasma chemistry, as illustrated in the next chapters. On the other hand, in a fluid model each type of species is considered as one group, and therefore a fluid model cannot describe the behavior of the species individually. Furthermore, it is supposed that the plasma must have a high enough density so that it resembles a continuum.<sup>27</sup> It is assumed that the species are more or less in equilibrium with the electric field, i.e., the energy gain due to the electric field is more or less balanced by the energy loss due to collisions, which is not always the case, e.g., for energetic electrons in a plasma. In addition, a fluid model requires input data on macroscopic properties of the species, which are based on assumptions of the particle energy distribution function.<sup>42</sup> Moreover it is not so easy to describe filaments in a DBD by means of a fluid model.

### 3.3. Plasimo's MD2D: The Fluid Model Applied

The model employed in this study is a one-dimensional fluid model, called Plasimo's MD2D.<sup>44-45</sup> Originally, MD2D was developed to describe the behavior of microdischarges in display technology, such as plasma addressed liquid crystal (PALC) and plasma display panel (PDP) technology.<sup>42, 46-48</sup> Later the model was transformed and extended by Brok and van Dijk, and incorporated into Plasimo.<sup>49</sup> In this way the model has previously been used for investigating the breakdown phenomena in fluorescent lamps,<sup>49-51</sup> the discharge characteristics of the plasma needle used for biomedical applications,<sup>52</sup> the behavior of DBDs at low pressure<sup>53</sup> and the characteristics of DBDs used as ionization source in analytical spectrochemistry.<sup>54-56</sup>

Analogous to other fluid models used for the description of low temperature plasmas,<sup>43, 57-60</sup> the MD2D fluid model is based on a set of balance equations derived from the Boltzmann transport equation (see previous section).

The first equation is the particle continuity equation, which describes the continuity of each type of species  $p$  incorporated in the model, in terms of its density  $n_p$ , flux  $\vec{\Gamma}_p$  and source  $S_p$  as a function of time and space:

$$\frac{\partial n_p}{\partial t} + \vec{\nabla} \cdot \vec{\Gamma}_p = S_p \quad (2)$$

The source term  $S_p$  is obtained by considering the volume reactions in which species  $p$  are produced or lost.

The second equation is the drift-diffusion equation, which describes the flux  $\vec{\Gamma}_p$  of each type of species  $p$  by means of the summation of a drift component

(only for the charged species), driven by the electric field  $\vec{E}$ , and a diffusion component, caused by the gradient of the density:

$$\vec{\Gamma}_p = \pm \mu_p \vec{E} n_p - D_p \vec{\nabla} n_p \quad (3)$$

$\mu_p$  and  $D_p$  denote here the mobility and diffusion coefficient of species p.

For the electrons also the electron energy balance equation is solved. The assumption that the energy is directly related to the local electric field is not valid for electrons, because they have a much lower mass compared with the heavy particles. Electron parameters are therefore expressed as a function of the average energy  $\bar{\varepsilon}$  which results from the following balance equation:

$$\frac{\partial(n_{\varepsilon})}{\partial t} + \vec{\nabla} \cdot \vec{\Gamma}_{\varepsilon} = S_{\varepsilon} \quad (4)$$

$S_{\varepsilon}$  is again a source term, which depends on the heating by the electric field and on the energy gained or lost in the various reactions.  $n_{\varepsilon}$  is the electron energy density:

$$n_{\varepsilon} = n_e \bar{\varepsilon} \quad (5)$$

and  $\vec{\Gamma}_{\varepsilon}$  denotes the electron energy flux:

$$\vec{\Gamma}_{\varepsilon} = \frac{5}{3} \bar{\varepsilon} \vec{\Gamma}_e + q \quad (6)$$

where q is the heat flux, which is assumed to be proportional to the gradient of the electron mean energy:

$$q = -\frac{5}{3} n_e D_e \nabla \bar{\varepsilon} \quad (7)$$

Substitution of equation (7) and equation (3) for  $\vec{\Gamma}_e$  transforms equation (6) into a drift-diffusion equation for the electron energy flux:

$$\vec{\Gamma}_{\bar{\epsilon}} = -\frac{5}{3}\mu_e \vec{E} n_e \bar{\epsilon} - \frac{5}{3}n_e D_e \vec{\nabla} \bar{\epsilon} \quad (8)$$

The first term is called the hydrodynamic flux of enthalpy and the second term is the heat conduction flux.

This set of partial differential equations is coupled to the Poisson equation, which delivers the electric field distribution:

$$\vec{\nabla} \cdot (\epsilon_m \vec{\nabla} \varphi) = -\vec{\nabla} \cdot (\epsilon_m \vec{E}) = -\sum_p q_p n_p \quad (9)$$

$\varphi$  is here the electric potential as a function of time and space,  $\epsilon_m$  is the permittivity of the medium (i.e. the plasma and the dielectrics) and  $q_p$  is the charge of species  $p$ . This Poisson equation is not only solved within the plasma, but also inside the dielectrics of the DBD plasma, where it reduces to:

$$\nabla^2 \varphi = 0 \quad (10)$$

because no charges are present inside the dielectrics.

The effect of charge accumulation on the surface of the dielectric materials is considered using Gauss's law:

$$\epsilon_{dielectric} \vec{E}_{dielectric} \cdot \vec{u}_n - \epsilon_{gas} \vec{E}_{gas} \cdot \vec{u}_n = \sigma \quad (11)$$

where  $\vec{E}_{dielectric}$  and  $\vec{E}_{gas}$  are the electric field inside the dielectric and in the gas, respectively,  $\vec{u}_n$  is the unit vector normal to the wall, where the charge accumulation occurs.  $\sigma$  is the surface charge density on the dielectric, calculated from the charged particle fluxes directed to the surface.

Furthermore, at the open boundaries of the reactor, where the gas enters and leaves the reactor, homogeneous Neumann boundary conditions are employed, meaning that the derivatives of the plasma quantities in the



direction perpendicular to these boundaries are set to zero; this applies to the densities of all the active species, the electron energy density and the electric potential. At the physical boundaries, i.e., the electrodes and the dielectric, the boundary conditions for  $n_p$  and  $n_e$  are given by the expressions for the flux densities  $\vec{\Gamma}_p$  and  $\vec{\Gamma}_e$ . These boundary conditions are determined by the reflection coefficients and the secondary electron emission coefficients of the different species included in the model. Besides, the correct electrode properties and dielectric properties are defined in the model. Detailed information about the boundary conditions used in this fluid model can be found in Mihailova et al.<sup>61</sup>.

The coupled differential equations are solved by the so-called “modified strongly implicit method”,<sup>62</sup> using an extra stabilization method,<sup>42</sup> until convergence is reached over the discharge cycles. The electron transport parameters and rate coefficients are not updated with each iteration, but they are updated whenever the densities of the molecules change a few percent. A more detailed description of the physics used in the model and of the numerical methods that are used is reported by Hagelaar<sup>42</sup> and by Brok et al.<sup>49</sup>.

Because the aim of our research is to determine the conversion of the inlet gases and the yields of the reaction products, calculations are carried out for a residence time up to 20 s. To limit the calculation time, the fluid model is used to follow all species as a function of time with a maximal time step in the order of 10 ns, until a periodic steady state is reached for the charged species. This takes typically 2 ms or 20 ac periods. Subsequently, the time averaged electron density, electron energy and rate coefficients of electron impact reactions are calculated and taken as a constant input for a reduced fluid

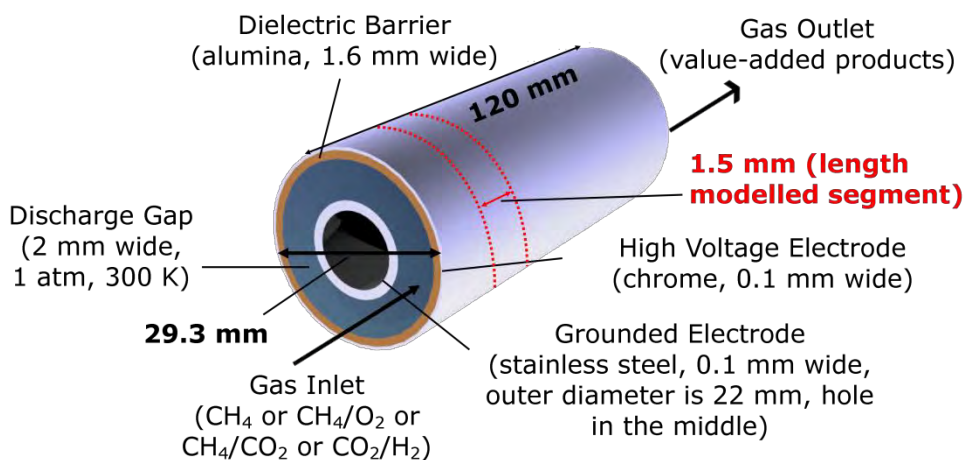
model, in which the electron energy balance equation and the Poisson equation are not solved. In this second part, the conversion of the molecules is calculated with a larger time step in the order of 100  $\mu$ s. Back-coupling to the short time step calculations is carried out regularly, to update the electron energy and density and the rate coefficients of the electron impact reactions if necessary. This decoupling of the model into charged species kinetics and neutral chemistry kinetics allows to increase the calculation speed with a factor of  $10^4$ . Typically, the calculations carried out in this PhD work take about 2 or 3 days on today's personal computers.

### 3.4. The Reactor Set-Up under Study

The numerical model is applied to an atmospheric pressure cylindrical DBD (see Figure 4). The reactor consists of two coaxial electrodes. The inner electrode (stainless steel) has an outer diameter of 22 mm. The outer electrode (chrome) has a diameter of 29.3 mm and at the inside it is in contact with a dielectric tube made of alumina. The alumina tube has an inner diameter of 26 mm and a wall thickness of 1.6 mm, leading to a discharge gap of 2 mm between both cylinders, i.e., the region where the gas flows through the reactor. The outer electrode is powered, whereas the inner electrode is grounded. The background gas temperature is 300 K and assumed to be constant in time and uniform in space. This is justified, because in a DBD there is only local heating due to the discharge filaments. However, the latter only take a very small fraction of the reactor volume for several nanoseconds, with a repetition in the microseconds scale, yielding a volume-corrected filament frequency of about 0.01% per discharge period.<sup>63</sup> Thus overall, the gas heating

is very limited. Furthermore, often a water jacket is used in experiments to cool the reactor and keep the reactor temperature constant at about 300 K.<sup>25, 64-68</sup> The total length of the reactor in the experiment is 120 mm. A residence time of 20 s corresponds for this set-up to a gas flow rate of about 0.05 L·min<sup>-1</sup>. More detailed information on the reactor set-up under study has been reported by Paulussen et al.<sup>68</sup>

In the model, however, only a segment of 1.5 mm long is considered. This is done to limit the calculation time and to avoid having to deal with filament formation in the reactor, as this cannot yet be simulated with the present model. On the other hand, by using 3 grid cells, instead of 1, in the axial direction, it is possible to describe the boundary conditions (see Section 3.3.) in a proper way in both the axial and the radial direction.



**Figure 4. Schematic diagram of the reactor under study.**

It needs to be realized that the effect of gas flow in the reactor is not modeled explicitly. Indeed, the real reactor can be considered as a kind of plug flow reactor, hence the concentration of the species varies as a function of the position in the reactor when the gas flows through. However, in the model this can be approximated by considering the reactor as a batch reactor, where the concentration of the species varies as a function of the residence time. Indeed, the variation of the concentrations as a function of time in a batch reactor is the same as the variation as a function of position in a plug flow reactor. In other words, the effect of gas flow is accounted for by studying the time variation of the species concentrations, where the residence time is calculated as the reactor volume divided by the gas flow rate.

### 3.5. Transport and Wall Interaction Coefficients

The species and reactions included in the different gas mixtures under study in this dissertation will be discussed in Chapter 4 for pure CH<sub>4</sub>, in Chapter 5 for CH<sub>4</sub>/O<sub>2</sub> and CH<sub>4</sub>/CO<sub>2</sub>, and in Chapter 6 for CO<sub>2</sub>/H<sub>2</sub>. Here we will discuss the determination of their transport coefficients for diffusion and mobility (only for the charged species), their sticking coefficients and their secondary electron emission coefficients, as this determination is generally valid for the different chapters.

The diffusion coefficient  $D_{ij}$  (m<sup>2</sup>·s<sup>-1</sup>) of the neutral species  $j$  in the background gas  $i$  is obtained by the Chapman-Enskog equation:<sup>69-70</sup>

$$D_{ij} = \frac{3k_b T \sqrt{\frac{4\pi k_b T}{2m_{ij}}}}{16p\pi\sigma_{ij}^2\Omega_D(\Psi)} \quad (12)$$

where  $k_b$  is the Boltzmann constant,  $T$  is the background gas temperature (K),  $p$  is the total pressure (Pa),  $m_{ij}$  is the reduced mass (kg),  $\sigma_{ij}$  is the characteristic length (m) and  $\Omega_D$  is the dimensionless diffusion collision integral. This collision integral, which is a function of the dimensionless temperature  $\Psi$ , is given by

$$\Omega_D = \frac{A}{\Psi^B} + \frac{C}{e^{D\Psi}} + \frac{E}{e^{F\Psi}} + \frac{G}{e^{H\Psi}} \quad (13)$$

where  $\Psi$  equals  $k_b T / \varepsilon_{ij}$ ,  $A = 1.06036$ ,  $B = 0.15610$ ,  $C = 0.19300$ ,  $D = 0.47635$ ,  $E = 1.03587$ ,  $F = 1.52996$ ,  $G = 1.76474$  and  $H = 3.89411$ .<sup>69</sup>  $\sigma_{ij}$  and  $\varepsilon_{ij}$  are calculated by

$$\sigma_{ij} = \frac{\sigma_i + \sigma_j}{2} \quad (14)$$

$$\varepsilon_{ij} = \sqrt{\varepsilon_i \varepsilon_j} \quad (15)$$

with  $\sigma$  (m) and  $\varepsilon$  (J) being the characteristic length and energy for every species in the 12-6 Lennard-Jones potential. These Lennard-Jones parameters were reported for most of the neutral species by Reid et al.<sup>69</sup> and by Svehla<sup>71</sup> and for the other species they were obtained by linear interpolation.

Finally the diffusion coefficient  $D_j$  of the species  $j$  in the entire gas mixture, i.e., the sum of all background gases  $i$ , is obtained from the different  $D_{ij}$ -values using Blanc's law:<sup>72</sup>

$$\frac{p_{tot}}{D_j} = \sum_i \frac{p_i}{D_{ij}} \quad (16)$$

with  $p_{tot}$  the total pressure and  $p_i$  the partial pressure of the background gas  $i$ .

The ion mobility  $\mu_{i,j}$  ( $\text{m}^2 \cdot \text{V}^{-1} \cdot \text{s}^{-1}$ ) of an ion  $j$  in the background gas  $i$  is calculated using the low electric field Langevin mobility expression:<sup>72</sup>

$$\mu_{i,j} = 0.515 \frac{T}{p \sqrt{m_{ij} \alpha_i}} \quad (17)$$

with  $T$  again the background gas temperature (K),  $p$  the gas pressure (Pa),  $m_{ij}$  the reduced mass (amu) and  $\alpha_i$  the polarizability ( $\text{\AA}^3$ ) of the background gas, which was obtained from Böttcher et al.<sup>73</sup> Afterwards the mobility coefficient  $\mu_j$  of the ion  $j$  in the entire gas mixture can be obtained in a similar way as the diffusion coefficient according to Blanc's law.

The mobility of the electrons and the rates of their collision reactions are described as parameters depending on the mean electron energy. These dependencies are calculated using the external Boltzmann solver Bolsig+,<sup>74</sup> which creates lookup tables for the mean electron energy, the electron mobility and the reaction rate coefficients as function of the reduced electric field. Accordingly, the electron mobility and the rate coefficients can be used as a function of the mean electron energy, which is calculated with the electron energy balance equation (see Section 3.3.).

From the ion mobility  $\mu_j$ , the ion diffusion coefficient  $D_j$  of an ion  $j$  can directly be obtained using the Einstein relation, in order to remain consistent with the physical approximations used in the model:

$$D_j = \frac{k_b T_{ion}}{e} \mu_j \quad (18)$$

where  $k_b$  is again the Boltzmann constant,  $T_{ion}$  is the ion temperature (K), which is assumed to be equal to the background gas temperature, and  $e$  is the

elementary charge. The Einstein relation is also used to obtain the electron diffusion coefficient from the electron mobility.

The sticking coefficients for the different higher hydrocarbon radicals are based on reported values by Bohmeyer et al.<sup>75</sup> and by Eckert et al.<sup>76</sup> Although the reported sticking coefficients are defined for somewhat different conditions, a good indication of the trend of the coefficients can be deduced. The sticking coefficients for the oxygen containing radicals were assumed to be one. The sticking probabilities for the various molecules and the ions were assumed to be zero and one, respectively. Note that the description of the surface reactions in the model is currently limited to this rough approximation and therefore the calculated densities of the radicals and molecules might be overestimated. The calculated densities of the ions, on the other hand, might be underestimated, although this is not so likely, as sticking equal to one is quite realistic for the ions, because they are indeed mostly neutralized upon arrival at the walls. For the ions, also secondary electron emission is considered when they collide with the reactor wall. A secondary electron emission coefficient of 0.05 was assumed and a corresponding energy of 5 eV.

### 3.6. Definitions of Conversion, Yield and Selectivity

Besides typical plasma characteristics, such as species densities, rates of the various reactions, electron energy, etc., the model can also calculate the conversion of the inlet gases, as well as the yields and selectivities of the reaction products, which is of interest for the application of gas conversion, investigated in this PhD thesis. The definitions of the conversions  $X$ , the yields  $Y$  and the selectivities  $S$  are as follows. The definitions can be slightly different, depending on the gas or gas mixture under study. Therefore, the gases or gas mixtures to which these specific definitions apply, are given between brackets.

$$X_{CH_4/CO_2/O_2/H_2} = \frac{n_{CH_4/CO_2/O_2/H_2,converted}}{n_{CH_4/CO_2/O_2/H_2,feed}} \times 100\% \quad (19)$$

$$Y_{H_2} = \frac{n_{H_2}}{2 \times n_{CH_4,feed}} \times 100\% \quad (CH_4, CH_4/O_2, CH_4/CO_2) \quad (20)$$

$$Y_{C_xH_yO_z} = \frac{x \times C_xH_yO_z}{n_{CH_4,feed}} \times 100\% \quad (CH_4, CH_4/O_2) \quad (21)$$

$$Y_{C_xH_yO_z} = \frac{x \times C_xH_yO_z}{n_{CH_4,feed} + n_{CO_2,feed}} \times 100\% \quad (CH_4/CO_2) \quad (22)$$

$$Y_{C_xH_yO_z} = \frac{x \times C_xH_yO_z}{n_{CO_2,feed}} \times 100\% \quad (CO_2/H_2) \quad (23)$$

$$Y_{H_2O} = \frac{n_{H_2O}}{2 \times (n_{CH_4,feed} + n_{O_2,feed})} \times 100\% \quad (CH_4/O_2) \quad (24)$$

$$Y_{H_2O} = \frac{n_{H_2O}}{2 \times (n_{CH_4,feed} + n_{CO_2,feed})} \times 100\% \quad (CH_4/CO_2) \quad (25)$$

$$S_{H_2} = \frac{n_{H_2}}{2 \times n_{CH_4,converted}} \times 100\% \quad (CH_4, CH_4/O_2, CH_4/CO_2) \quad (26)$$



$$S_{C_xH_yO_z} = \frac{x \times C_{xH_yO_z}}{n_{CH_4,converted}} \times 100\% (CH_4, CH_4/O_2) \quad (27)$$

$$S_{C_xH_yO_z} = \frac{x \times C_{xH_yO_z}}{n_{CH_4,converted} + n_{CO_2,converted}} \times 100\% (CH_4/CO_2) \quad (28)$$

$$S_{C_xH_yO_z} = \frac{x \times C_{xH_yO_z}}{n_{CO_2,converted}} \times 100\% (CO_2/H_2) \quad (29)$$

$$S_{H_2O} = \frac{n_{H_2O}}{2 \times (n_{CH_4,converted} + n_{O_2,converted})} \times 100\% (CH_4/O_2) \quad (30)$$

$$S_{H_2O} = \frac{n_{H_2O}}{2 \times (n_{CH_4,converted} + n_{CO_2,converted})} \times 100\% (CH_4/CO_2) \quad (31)$$

In these definitions the parameter  $x$  denotes the stoichiometric balance coefficient, which corresponds also to the index in the compound name of  $C_xH_y$  or  $C_xH_yO_z$ . Furthermore, note that the yield and selectivity of CO are calculated with  $Y_{C_xH_yO_z}$  and  $S_{C_xH_yO_z}$ , respectively, with  $y = 0$ , and that the yield and selectivity of the higher hydrocarbons ( $C_xH_y$ ) are calculated with  $Y_{C_xH_yO_z}$  and  $S_{C_xH_yO_z}$ , respectively, with  $z = 0$ .

### 3.7. Aim and Outline of the PhD Dissertation

The aim of this dissertation is to come to a better understanding of the huge plasma chemistry governing gas conversion processes in a DBD using numerical simulations. More specifically, the goal is to develop a reliable chemistry set for the description of the gas phase chemistry in pure  $\text{CH}_4$ ,  $\text{CH}_4/\text{O}_2$ ,  $\text{CH}_4/\text{CO}_2$  and  $\text{CO}_2/\text{H}_2$  gas discharges by 1D fluid modeling. In this way, calculation results can be obtained on the densities of the different plasma species, the conversions of the inlet gases, the yields and selectivities of the end products and the dominant reaction pathways for each of the gas mixtures studied. This allows us to determine whether or not a specific gas mixture is suitable for the production of a specific end-product of interest. Our calculation results are validated with reported results in literature and for pure  $\text{CH}_4$  also with some experiments for the reactor set-up under study. Based on these results, we hope to clarify whether a sustainable competitive industrial process for gas conversion in a DBD can be developed in the future.

In the next chapters, the construction of the chemistry sets, as well as the obtained results for the different gas mixtures studied, are described. In **Chapter 4**, the fluid model is applied to describe the conversion of pure  $\text{CH}_4$  into higher hydrocarbons. **Chapter 5** concerns the fluid modeling of the gas phase chemistry for partial oxidation ( $\text{CH}_4/\text{O}_2$ ) and for dry reforming ( $\text{CH}_4/\text{CO}_2$ ) of methane, focusing on the formation of oxygenates and syngas. In **Chapter 6**, the aim is to investigate the potential of the hydrogenation of carbon dioxide ( $\text{CO}_2/\text{H}_2$ ) in a DBD using a fluid model.

Finally, in **Chapter 7**, a general conclusion is given, as well as an outlook for the future.



# Chapter 4

## The Conversion of CH<sub>4</sub> into Higher Hydrocarbons

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The fluid model described in previous chapter is applied here to the conversion process of methane into higher hydrocarbons. The spatially averaged densities of the various plasma species as a function of time are discussed. Besides, the conversion of methane and the yields of the reaction products as a function of the residence time in the reactor are shown and compared with experimental data. Higher hydrocarbons (C<sub>2</sub>H<sub>y</sub> and C<sub>3</sub>H<sub>y</sub>) and hydrogen gas are typically found to be important reaction products. Furthermore, the main underlying reaction pathways are determined.

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## 4.1. Introduction

As discussed in Chapter 1, a sustainable process for the conversion of the abundant methane reserves into more value-added chemicals and fuels is renowned as a challenge for the 21st century. More in particular, the development of a process for the direct synthesis of higher hydrocarbons and oxygenates from methane in an energy-efficient way would offer significant benefits, because this will circumvent the very expensive syngas step. In this chapter the plasma chemistry governing the conversion of pure CH<sub>4</sub> into higher hydrocarbons (C<sub>x</sub>H<sub>y</sub>) is discussed.

Experimental results on the conversion in a pure methane plasma found in literature show that the typical end products are H<sub>2</sub> and higher hydrocarbons, mostly C<sub>2</sub>H<sub>6</sub> and in a lower content C<sub>3</sub>H<sub>8</sub>, C<sub>2</sub>H<sub>4</sub> and C<sub>2</sub>H<sub>2</sub>.<sup>13, 77-80</sup> Modeling results on gas phase physics and chemistry in different kinds of methane containing discharges have been investigated extensively during the past thirty years.<sup>20, 81-109</sup> A minority of them concerns the modeling of the plasma as a gas conversion reactor in pure CH<sub>4</sub>.<sup>92, 103</sup> Up to now, these numerical studies mostly concerned zero-dimensional simulations largely based on specific empirical input so that semi-empirical simulations were obtained, which are only valid for the experimental set-up under study. Only Yang<sup>92</sup> used a more generic method to describe the gas conversion in a pure methane plasma, which can be generally used for this kind of gas discharges. In this paper again a 0D model was used, the plasma chemistry presented was limited and the presented results were rather preliminary.

In order to achieve our goal, i.e., to describe in detail the plasma chemistry in an atmospheric pressure DBD in different gas mixtures with CH<sub>4</sub> and/or CO<sub>2</sub>,

we started by developing a 1D fluid model for an atmospheric pressure DBD in pure methane. In this chapter we present our most important results on the conversion of CH<sub>4</sub> into higher hydrocarbons. First of all, the spatially averaged densities of the various plasma species as a function of time will be discussed. Furthermore, the conversion of CH<sub>4</sub>, and the yields and selectivities of the reaction products will be shown. Finally, the main underlying reaction pathways for the conversion of CH<sub>4</sub> into higher hydrocarbons will be pointed out.

## 4.2. Species Included in the Model

In order to describe the chemistry in a pure methane plasma, 36 different species (electrons, molecules, ions and radicals) are taken into account in the model. The selection of species is based on other modeling studies for methane discharges under various conditions.<sup>70, 81, 110</sup> In addition to the feed gas CH<sub>4</sub>, also H<sub>2</sub> and some higher order neutral molecules C<sub>2</sub>H<sub>6</sub>, C<sub>2</sub>H<sub>4</sub>, C<sub>2</sub>H<sub>2</sub>, C<sub>2</sub>, C<sub>3</sub>H<sub>8</sub> and C<sub>3</sub>H<sub>6</sub> are considered in the model, as it was shown in literature that they are formed in the plasma at high densities.<sup>78, 80</sup> High densities of C<sub>2</sub>H<sub>2</sub> in the discharge may lead to polymerization and in order to deal with this, in a first attempt the polymerization product C<sub>4</sub>H<sub>2</sub> is also included in the model. Furthermore, 11 radical species and 16 ionic species are taken into account corresponding to the products of dissociation and ionization reactions, respectively, of these high density molecules.

A methane plasma has a very strong electropositive character.<sup>70</sup> The negative ion densities are about one order of magnitude lower than the electron and the positive ion densities<sup>82-83</sup> and therefore, negative ions are

not incorporated in the model. Although some vibrational excitation reactions are included in the model, vibrationally excited species are not taken into account separately in order to limit the number of species and reactions, and because vibrationally excited species are considered to be of minor importance in a DBD.<sup>111-112</sup> Also rotationally and electronically excited species are not taken into account in the model. Indeed, the electron energy required for rotational excitations is negligible compared with this for vibrational excitations,<sup>70, 110</sup> and all electronically excited states of methane lead to dissociation.<sup>113</sup> Therefore, it is also assumed here that the electronically excited states for the higher order neutrals lead to dissociation. An overview of the different species taken into account in the model can be found in Table 4.

**Table 4. Overview of the species included in the model, besides the electrons.**

Molecules	Ions	Radicals
CH <sub>4</sub>	CH <sub>5</sub> <sup>+</sup> , CH <sub>4</sub> <sup>+</sup> , CH <sub>3</sub> <sup>+</sup> , CH <sub>2</sub> <sup>+</sup> , CH <sup>+</sup> , C <sup>+</sup>	CH <sub>3</sub> , CH <sub>2</sub> , CH, C
C <sub>2</sub> H <sub>6</sub> , C <sub>2</sub> H <sub>4</sub> , C <sub>2</sub> H <sub>2</sub> , C <sub>2</sub> , C <sub>3</sub> H <sub>8</sub> , C <sub>3</sub> H <sub>6</sub>	C <sub>2</sub> H <sub>6</sub> <sup>+</sup> , C <sub>2</sub> H <sub>5</sub> <sup>+</sup> , C <sub>2</sub> H <sub>4</sub> <sup>+</sup> , C <sub>2</sub> H <sub>3</sub> <sup>+</sup> , C <sub>2</sub> H <sub>2</sub> <sup>+</sup> , C <sub>2</sub> H <sup>+</sup> , C <sub>2</sub> <sup>+</sup>	C <sub>2</sub> H <sub>5</sub> , C <sub>2</sub> H <sub>3</sub> , C <sub>2</sub> H, C <sub>3</sub> H <sub>7</sub> , C <sub>3</sub> H <sub>5</sub>
H <sub>2</sub>	H <sub>3</sub> <sup>+</sup> , H <sub>2</sub> <sup>+</sup> , H <sup>+</sup>	H
C <sub>4</sub> H <sub>2</sub>		

### 4.3. Reactions Included in the Model

A consistent set of 367 gas phase reactions involving the 36 defined species was built to describe the plasma chemistry in the discharge gap. These gas phase reactions can be divided into four groups: 100 electron-neutral, 35 electron-ion, 92 neutral-neutral and 140 ion-neutral reactions. The electron-

neutral reactions include 6 momentum transfer, 15 vibrational excitation, 47 ionization and 32 dissociation reactions. The electron-ion reactions are all dissociative recombination reactions, because volume recombination is an important process at atmospheric pressure, which is logical because of the high densities. An overview of the reactions considered in the model is given in the Appendices.

The rates of the different reactions are calculated in the model from the densities of the colliding species and the corresponding reaction rate coefficients. For the electron-neutral and electron-ion reactions, an energy dependent reaction rate coefficient is used. The Boltzmann solver Bolsig+<sup>74</sup> (see previous chapter) is used to create the lookup tables for the rate coefficients of the electron-neutral reactions based on the energy dependent collision cross sections for these reactions. The references for the cross sections can be found in Table A.1. of the Appendices. The lookup tables for the electron-ion dissociative recombination reactions are built using the functions in combination with the branching ratios for the different channels of which a detailed overview is given in Table A.2. of the Appendices. The neutral-neutral and ion-neutral reactions are defined in the model with a constant reaction rate coefficient, for a fixed pressure and temperature of 1 atm and 300 K, respectively. The constant rate coefficients and the corresponding references for the neutral-neutral and ion-neutral reactions are summarized in Table A.3. and Table A.4. of the Appendices, respectively. Note that the rate coefficient of the recombination reaction of CH<sub>3</sub> with C<sub>2</sub>H<sub>5</sub> resulting in the formation of C<sub>3</sub>H<sub>8</sub> was estimated based on the matching between experimental results and our calculation results. The values reported in literature for this reaction are either too low<sup>114</sup> (i.e.,  $5.60 \times 10^{-11} \text{ cm}^3 \cdot \text{s}^{-1}$ ,



which is equal to  $2.29 \times 10^{-30} \text{ cm}^6 \cdot \text{s}^{-1}$  as adjusted for a three-body collision by dividing by the density of the background gas) or too high<sup>115</sup> (i.e.,  $1.87 \times 10^{-23} \text{ cm}^6 \cdot \text{s}^{-1}$ ). Therefore, a rate coefficient of  $1 \times 10^{-28} \text{ cm}^6 \cdot \text{s}^{-1}$  is assumed in the model.

## 4.4. Operating Conditions

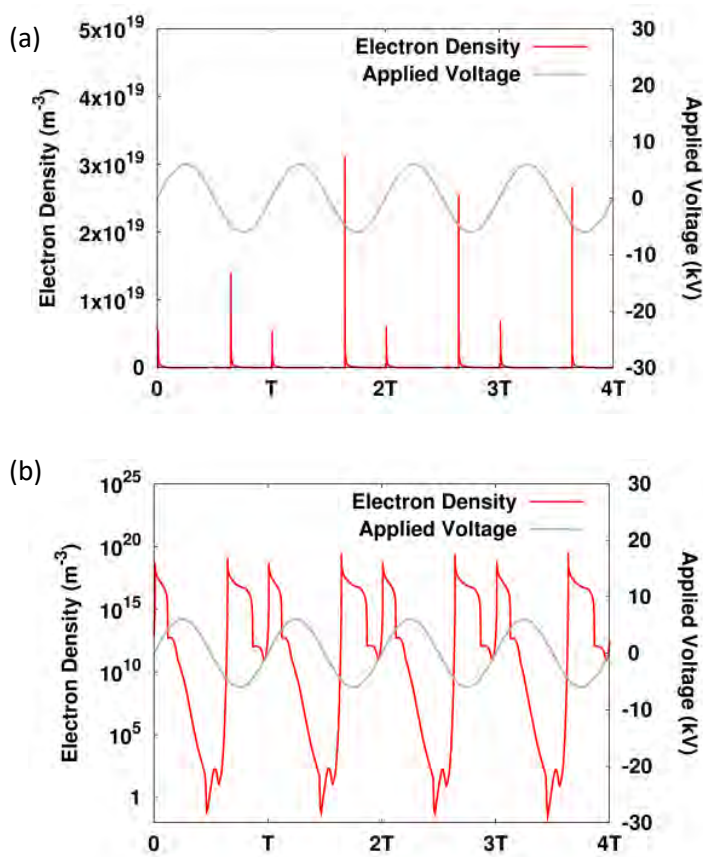
The calculations are carried out at a fixed applied voltage of 6 kV and a frequency of 10 kHz, which are typical operating conditions applied in the experiments.<sup>68</sup> Experiments are performed for this DBD set-up to validate the calculated results. The analysis of the reaction product mixture is done by gas chromatography. A Trace GC from Thermo is equipped with two analysis channels. A first channel contains a thermal conductivity detector (TCD) to analyze the outcome of two serial installed packed columns: a Haysep Q (80-100, 2m\*1/8" Siltek) and a Molsieve 5A (80-100, 3m\*1/8"). The second channel has a flame ionization detector (FID) installed after a RTX-1 capillary column (5μ, 25m\*0.53mm).

## 4.5. Results and Discussion

### 4.5.1. Densities of the Plasma Species

Figure 5 illustrates the calculated periodic behavior of the spatially averaged electron density on a linear (a) and on a logarithmic (b) scale as a function of time, for four periods of the applied voltage. The applied voltage as a function of time is also plotted. It is clear that multiple breakdowns in the gas appear each half period following the applied voltage. The difference in the electron

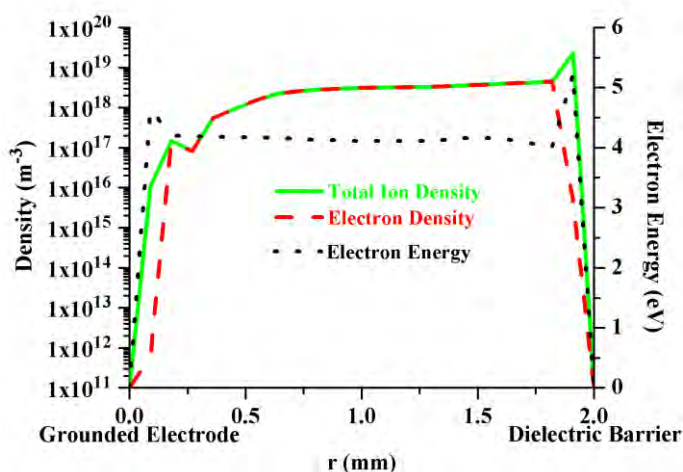
density behavior for the positive and the negative polarity of the applied voltage is due to the dissimilarity in surface dimensions and properties of the inner and outer electrode (only one of the electrodes is covered by a dielectric, see Figure 4). The overall spatially and time averaged electron density amounts to  $10^{17} \text{ m}^{-3}$ . The overall spatially and time averaged electron energy was calculated to be about 2 eV.



**Figure 5.** Spatially averaged electron density, on a linear (a) and a logarithmic (b) scale, as a function of time, as well as the applied voltage for four periods of time.

Note that the present model cannot deal with filament formation in the reactor. Therefore, the presented electric behavior corresponds to a DBD treated as a homogeneous glow discharge. Of course, this behavior is quite different from the experimental behavior, but we believe that the rest of our calculation results, such as conversion and yields, and the reaction pathways, are still valid.

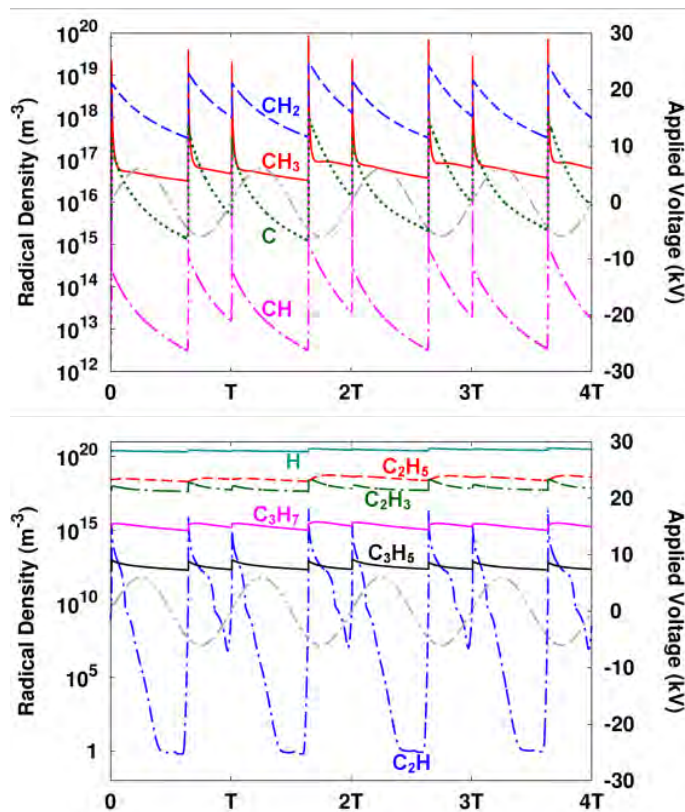
The spatial variation of the electron density, total ion density and electron energy, taken at the maximum of its time profile, is depicted in Figure 6. It is clear that in the bulk plasma, the electron and ion densities are in the order of  $10^{18} \text{ m}^{-3}$ , and they are more or less equal to each other, providing charge neutrality in the bulk. However, close to the electrodes, the electron density drops to zero, and the total positive ion density is several orders of magnitude higher than the electron density, providing a net positive space charge. This behavior is typical for the sheath formation in a DBD.<sup>116</sup> A different behavior is observed in the pre-sheath near the inner (grounded) electrode, where the ion density drops one order of magnitude, while near the dielectric barrier at the outer (powered) electrode, the ion density rises one order of magnitude. This different behavior is attributed to the fact that at this particular moment in time the powered electrode (covered by the dielectric barrier) is the cathode, which attracts the ions, while the grounded electrode is the anode, which repels the ions. Due to the acceleration of the electrons in the high electric field in the sheath, these electrons have an increased energy there.



**Figure 6.** Calculated spatial profiles of the electron and total ion density (left axis) and electron energy (right axis) in the gap between both electrodes, taken at the maximum of their time profile. The inner (grounded) electrode is at the left, whereas the outer (powered) electrode with the dielectric layer is at the right.

Collisions of the electrons with the background gas molecules lead to the formation of radicals and ions. The number densities of these radicals and ions exhibit the same periodic behavior as the electron density. Figure 7 shows the spatially averaged radical densities as a function of time. In case of the radicals this periodic trend is superimposed on a rising or declining trend which acts over a longer time-scale until periodic steady state is reached. The variation through a period, i.e. the difference between the minimum and maximum value in one period, varies from less than one order of magnitude for C<sub>2</sub>H<sub>5</sub>, C<sub>2</sub>H<sub>3</sub>, C<sub>3</sub>H<sub>7</sub>, C<sub>3</sub>H<sub>5</sub> and H, to several orders of magnitude for CH<sub>3</sub>, CH<sub>2</sub>, CH, C and C<sub>2</sub>H. This can be explained by the fact that, except for C<sub>2</sub>H, this last group of radicals is directly formed from the background gas CH<sub>4</sub> by electron impact dissociation, which is not the case for the higher order radicals. The overall spatially and time averaged radical densities vary from about 10<sup>12</sup> m<sup>-3</sup>

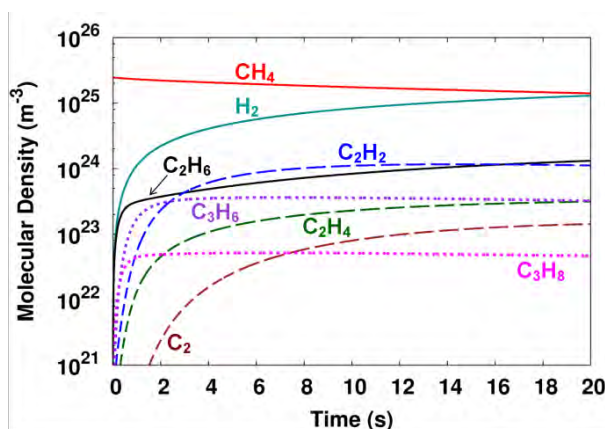
for the less abundant radicals to about  $10^{20} \text{ m}^{-3}$  for the most abundant radicals. The most abundant radicals are H, CH<sub>3</sub>, CH<sub>2</sub>, C<sub>2</sub>H<sub>5</sub> and C<sub>2</sub>H<sub>3</sub>. The overall spatially and time averaged ion densities vary from almost zero to the order of  $10^{16} \text{ m}^{-3}$  for the most important ions (CH<sub>5</sub><sup>+</sup>, C<sub>2</sub>H<sub>5</sub><sup>+</sup>, C<sub>2</sub>H<sub>4</sub><sup>+</sup>, C<sub>2</sub>H<sub>3</sub><sup>+</sup>).



**Figure 7.** Spatially averaged radical densities as a function of time, as well as the applied voltage for four periods of time.

Recombination of the radicals leads to the formation of higher order hydrocarbons and hydrogen gas. The spatially averaged densities of these molecules do not exhibit this periodic behavior. Indeed, their densities behave more or less independent from the applied voltage, since they are only indirectly correlated with the electron density and electron energy by the

densities of the radicals from which they are formed (see discussion about the reaction pathways in Section 4.5.3.). The net production of these higher hydrocarbon molecules and hydrogen gas is higher than their net consumption, and as result a gradual increase in the densities is observed each half period of the applied voltage. In contrast, the net consumption of CH<sub>4</sub> is higher than its net production, and therefore a gradual decrease in the CH<sub>4</sub> density is observed each half period. Therefore, it is more interesting to look to the variation of the molecule densities on a longer time-scale.



**Figure 8. Spatially averaged molecular densities as a function of the residence time.**

Figure 8 illustrates the spatially averaged molecule densities as a function of the residence time in the plasma reactor. Note that a residence time of 20 s corresponds to a gas flow rate of 0.05 L·min<sup>-1</sup> for the experimental set-up under study. The density of the background gas methane is initially  $2.45 \times 10^{25}$  m<sup>-3</sup>, but is decreasing due to dissociation and ionization reactions governing the conversion process. As a result, H<sub>2</sub>, C<sub>2</sub>H<sub>6</sub>, C<sub>2</sub>H<sub>4</sub>, C<sub>2</sub>H<sub>2</sub>, C<sub>2</sub>, C<sub>3</sub>H<sub>8</sub> and C<sub>3</sub>H<sub>6</sub> are formed and are also present in the discharge at high densities, as shown in Figure 8. It appears that the production is most pronounced in the first 1 to 2 s

and that the densities of the higher hydrocarbons and H<sub>2</sub> molecules do not significantly change anymore for a longer residence time. However, the logarithmic scale is a bit misleading and the conversion still continues, as will be illustrated in Section 4.5.2. below. The spatially averaged densities vary between  $10^{22} \text{ m}^{-3}$  and  $10^{25} \text{ m}^{-3}$  for the different molecules. H<sub>2</sub> seems to be formed at the highest density, and after 20 s, its density is comparable to the CH<sub>4</sub> density. As far as the higher hydrocarbon species are concerned, it appears from Figure 8 that C<sub>2</sub>H<sub>6</sub> and C<sub>2</sub>H<sub>2</sub> are formed with the highest density, which is only about one order of magnitude lower than the CH<sub>4</sub> density after 20 s. As a result of the polymerization of C<sub>2</sub>H<sub>2</sub>, also C<sub>4</sub>H<sub>2</sub> is formed with a density of  $10^{24} \text{ m}^{-3}$ . At first sight, this density seems rather high. This can be explained by the fact that C<sub>4</sub>H<sub>2</sub> is considered in the model as the sum of all higher polymerized species. Moreover, in the model no loss mechanism for C<sub>4</sub>H<sub>2</sub> is included and the sticking probability of C<sub>4</sub>H<sub>2</sub> is defined zero, as for the other molecules (see Section 3.5. above).

#### 4.5.2. Conversion, Yields and Selectivities

Figure 9(a) illustrates the calculated conversion of CH<sub>4</sub> and the yields of the reaction products, i.e., H<sub>2</sub> and the summation over all C<sub>2</sub>H<sub>y</sub> and C<sub>3</sub>H<sub>y</sub> hydrocarbons, as a function of residence time in the reactor (solid lines). The measured conversion and yields of these products, for similar operating conditions, are depicted with dashed lines.

As expected, both the conversion and the various yields increase as a function of residence time. After 20 s, only 40% of CH<sub>4</sub> is converted and the H<sub>2</sub> and C<sub>2</sub>H<sub>y</sub> molecules are formed with the highest yields. Reasonable

agreement is reached between calculated and experimental results, taking into account the complexity of the plasma chemistry. The calculated and measured CH<sub>4</sub> conversion and C<sub>3</sub>H<sub>y</sub> yield agree within 5 %. However, the differences are significant for the H<sub>2</sub> yield and the C<sub>2</sub>H<sub>y</sub> yield, although they show at least similar trends between calculated and experimental values. A possible explanation for these significant differences is given below when the selectivities of H<sub>2</sub> and C<sub>2</sub>H<sub>2</sub> are discussed. The calculated and measured carbon and hydrogen balances are plotted in Figure 9(b), and show an agreement within 20 %. A possible explanation for the differences between the calculated and the measured balances is the uncertainty of the used sticking coefficients. The carbon balance drops slightly as a function of residence time, due to sticking at the walls in the form of solid carbon. After a residence time of 20 s, roughly 20% of the carbon atoms is left in the reactor.

In Figure 9(c) the calculated (solid lines) and measured (dashed lines) selectivities of the individual reaction products are plotted as a function of the conversion of CH<sub>4</sub>. From the higher hydrocarbons, C<sub>2</sub>H<sub>6</sub> (dark blue) has the highest selectivity, both in the calculated and the measured results. The selectivity is especially high (100% in the calculations) at very low conversion of CH<sub>4</sub>. This is because when the discharge is ignited, electron impact dissociation of CH<sub>4</sub> leads to the formation of H<sub>2</sub> and CH<sub>3</sub>. This methyl radical will immediately initiate the recombination reactions towards C<sub>2</sub>H<sub>6</sub>, which in turn is converted later in new radicals and the other higher hydrocarbons. A more thorough discussion on the dominant reaction pathways can be found in the next section. However, this very low conversion is not interesting from an applications point of view. The typical selectivity, in the range of 10-40% CH<sub>4</sub> conversion, is around 20-30%.



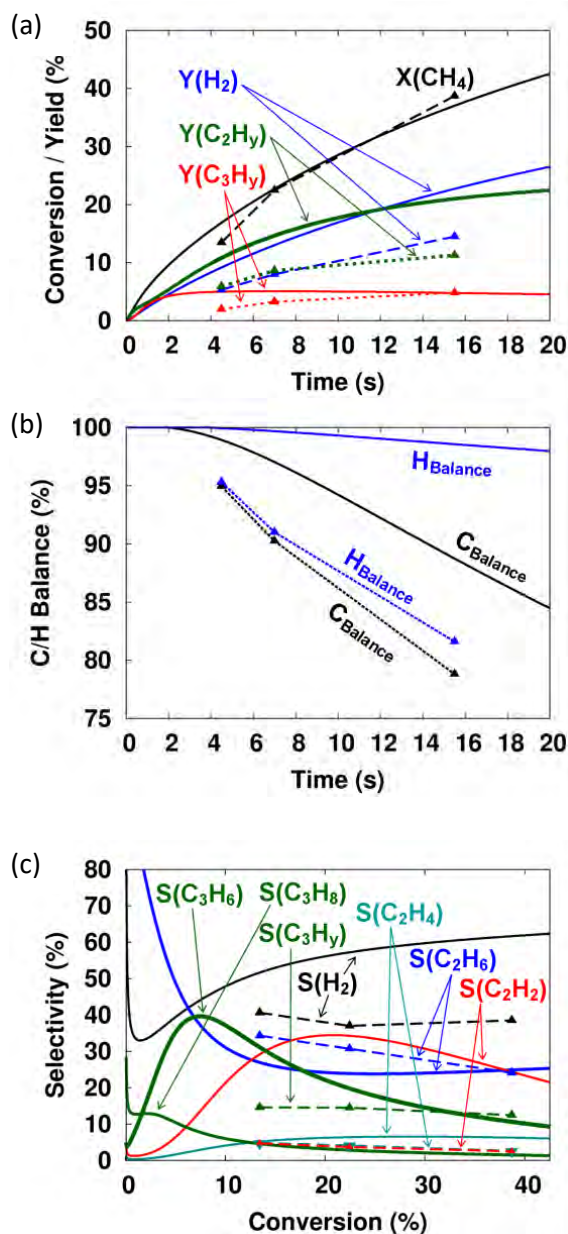


Figure 9. (a) Calculated (solid lines) and experimental (dashed lines) conversion of  $\text{CH}_4$  and yields of the reaction products, as a function of residence time in the reactor. In (b) the calculated (solid lines) and measured (dashed lines) carbon-balances and hydrogen-balances are illustrated. In (c) the calculated (solid lines) and experimental (dashed lines) selectivities of the individual hydrocarbon reaction products are plotted as a function of the conversion of  $\text{CH}_4$ . Note that the selectivity of  $\text{C}_3\text{H}_6$  could not be measured.

The experimental results show that C<sub>2</sub>H<sub>4</sub> (dark cyan, dashed) and C<sub>2</sub>H<sub>2</sub> (red, dashed) have a much lower selectivity than C<sub>2</sub>H<sub>6</sub>. The calculated selectivity of C<sub>2</sub>H<sub>4</sub> (dark cyan, solid) is in good agreement with the experiment (i.e., in the order of 5-10%), but the calculated selectivity of C<sub>2</sub>H<sub>2</sub> (red, solid) is too high compared to the experimental results. A possible reason might be that the further polymerization of C<sub>2</sub>H<sub>2</sub> molecules into higher molecules is underestimated in the model. Indeed, dust formation appears to be important in acetylene plasmas. In previous models by our group,<sup>117-119</sup> these polymerization reactions were studied in detail by an extensive chemistry set, including neutral, positive and negative ion pathways. However, in the present model, the polymerization is only treated by one chemical reaction (i.e., C<sub>2</sub>H insertion; see Section 4.5.3. below), in order not to further complicate our plasma chemistry set, which is already huge. Therefore, the obvious overestimated C<sub>2</sub>H<sub>2</sub> selectivity in our model is probably attributed to the underestimation of C<sub>2</sub>H<sub>2</sub> polymerization. Moreover, the overestimated C<sub>2</sub>H<sub>2</sub> formation explains why the calculated yield of the overall C<sub>2</sub>H<sub>y</sub> fraction is higher than the measured values (Figure 9(a)).

The calculated and measured yields of the summation over all C<sub>3</sub>H<sub>y</sub> molecules are in an almost perfect agreement (Figure 9(a)). The sum of the calculated selectivities of C<sub>3</sub>H<sub>8</sub> (dark green, solid) and C<sub>3</sub>H<sub>6</sub> (light green, solid) is in reasonable agreement with the total measured selectivity of C<sub>3</sub>H<sub>y</sub> (green, dashed). However, it is not possible to compare the calculated selectivities of the different compounds, as the measured peaks of the different C<sub>3</sub>H<sub>y</sub> molecules overlap in the chromatogram.

Besides the higher hydrocarbons, H<sub>2</sub> is also formed as a main end product in the discharge. The calculated yields and selectivities of H<sub>2</sub> are a bit higher than

the measured values. This is probably because the production of H<sub>2</sub> by electron impact dissociation of C<sub>2</sub>H<sub>6</sub> and C<sub>3</sub>H<sub>8</sub> (see next section for the most important consumption and production pathways of H<sub>2</sub>) is assumed a bit too high in the model.

As mentioned above, the formation of C<sub>4</sub>H<sub>2</sub> by polymerization reactions of C<sub>2</sub>H<sub>2</sub> species is also included in the model. However, as C<sub>4</sub>H<sub>2</sub> could not be measured in the experiments, it is treated as a loss of carbon in the model, in order to match the calculated and measured carbon balances. The calculated yield of C<sub>4</sub>H<sub>2</sub> after 20s amounts to 13.75 %.

Reported results in literature based on experiments on the conversion of methane into higher hydrocarbons, at similar conditions, show similar trends, namely the end products were mainly H<sub>2</sub> and C<sub>2</sub>H<sub>y</sub> (mostly C<sub>2</sub>H<sub>6</sub>) as well as, to a lower extent, some higher hydrocarbons (C<sub>3</sub>H<sub>y</sub>, C<sub>4</sub>H<sub>y</sub>, ...).<sup>13, 78, 80</sup>

### 4.5.3. Dominant Reaction Pathways

#### (a) Electron impact reactions with CH<sub>4</sub>: the formation of radicals and ions

As soon as the sinusoidal voltage is applied to the reactor and the discharge is ignited, electron impact ionization and dissociation of CH<sub>4</sub> occurs, and this results in the consumption of CH<sub>4</sub> and the creation of new species (electrons, ions, radicals). The formation of new electrons and ions in the plasma is important in order to sustain the discharge. The most important channels for electron impact ionization of CH<sub>4</sub> are:



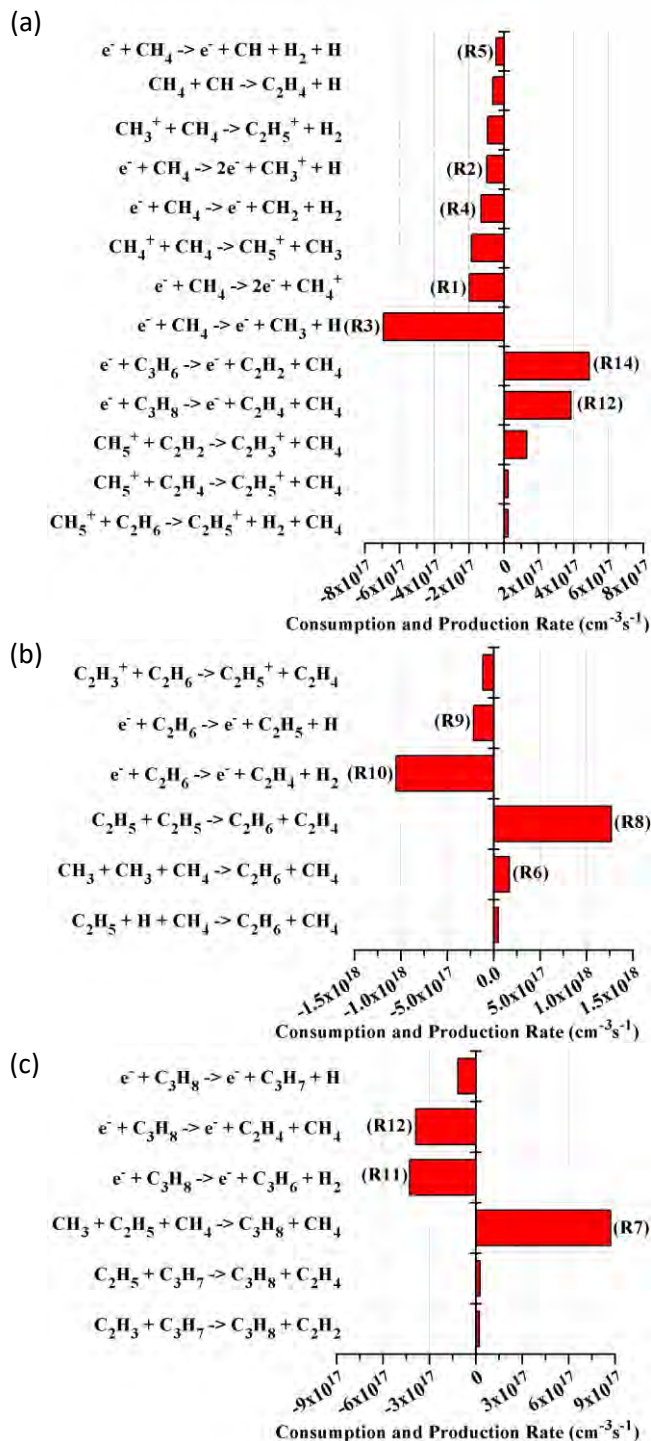


Our calculations point out that reaction (R1) is responsible for 66% of the total electron impact ionization of CH<sub>4</sub>, while reaction (R2) is responsible for 33%, which is in good agreement with the results reported by Yang.<sup>92</sup>

The dissociation of CH<sub>4</sub> leads to the formation of radicals. It is of special interest when studying the gas conversion process, because these radicals are important reagents in the production of higher order hydrocarbons. The most important channels for consumption of CH<sub>4</sub> are electron impact dissociation reactions, more specifically:



Our calculations point out that reaction (R3) is responsible for 79% of the total electron impact dissociation of CH<sub>4</sub>, while reactions (R4) and (R5) are responsible for 15% and 5%, respectively. Similar results were reported by Yang.<sup>92</sup>



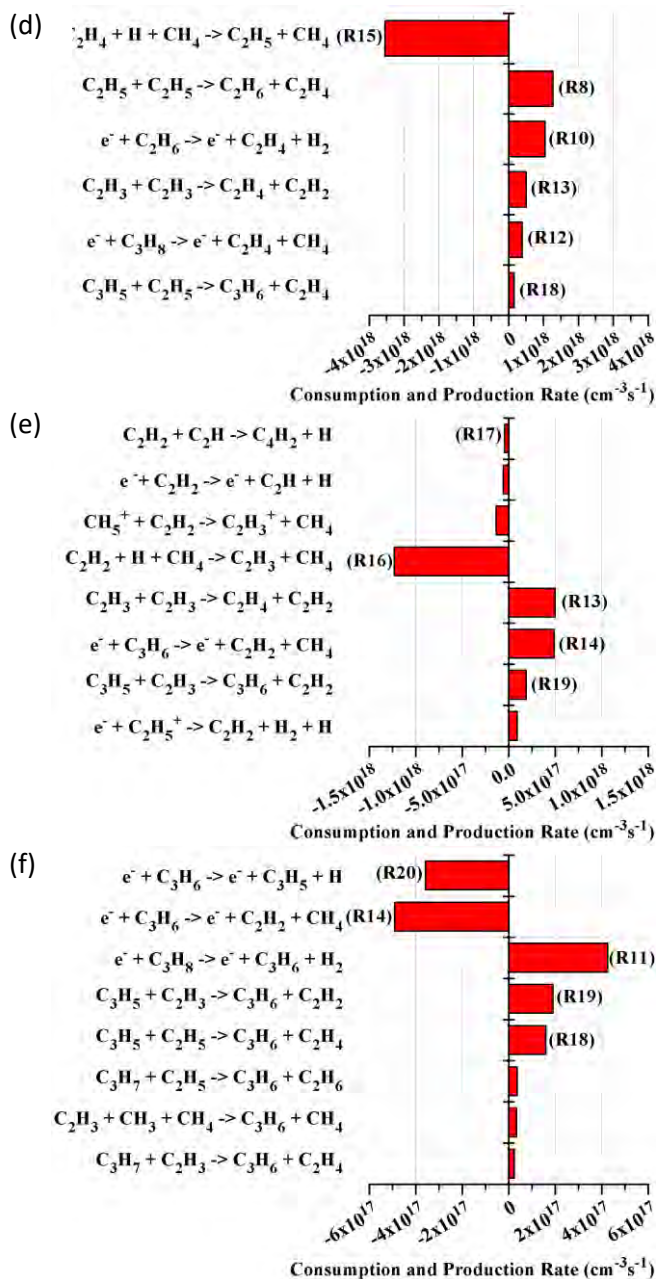


Figure 10. Calculated time-averaged reaction rates of the dominant reaction pathways for the production and consumption of CH<sub>4</sub> (a), C<sub>2</sub>H<sub>6</sub> (b), C<sub>3</sub>H<sub>8</sub> (c), C<sub>2</sub>H<sub>4</sub> (d), C<sub>2</sub>H<sub>2</sub> (e) and C<sub>3</sub>H<sub>6</sub> (f). The production rates are plotted as positive values (i.e., right-hand side of the figures), whereas the consumption rates are defined as negative values (i.e., left-hand side of the figures). The most important pathways are labeled, and the labels correspond to the reactions given in the text.

The dominant reactions for CH<sub>4</sub> consumption (and production) are depicted in Figure 10(a). It is clear that the electron impact dissociation reaction to CH<sub>3</sub> (i.e., reaction (R3)) is by far the dominant consumption process of CH<sub>4</sub>, followed by electron impact ionization to CH<sub>4</sub><sup>+</sup> (i.e., reaction (R1)). Besides the electron impact ionization and dissociation reactions, also some neutral-neutral and ion-neutral reactions are important for the consumption of CH<sub>4</sub> (see Figure 10(a)).

Note that electron impact vibrational excitation of CH<sub>4</sub> is also an important process. However, in the model these vibrational excitation reactions are only considered as an energy loss for the electrons (i.e., the vibrationally excited species are not taken into account separately) and therefore these reactions are not included in Figure 10(a) since they neither entail consumption or production of CH<sub>4</sub>. In literature it is reported that a similar result is obtained whether the vibrationally excited species are taken into account or not, because in that case the electron impact excitation to CH<sub>4</sub><sup>\*</sup> is balanced by the de-excitation of CH<sub>4</sub><sup>\*</sup> on the reactor wall.<sup>92</sup>

It can also be deduced from Figure 10(a) that the most important pathways for the regeneration of CH<sub>4</sub> are based on electron impact dissociation of higher hydrocarbons, such as C<sub>3</sub>H<sub>6</sub> and C<sub>3</sub>H<sub>8</sub> (see below).

### **(b) The recombination of CH<sub>3</sub>: the formation and loss of C<sub>2</sub>H<sub>6</sub> and C<sub>3</sub>H<sub>8</sub>**

The most important radical produced out of CH<sub>4</sub> is CH<sub>3</sub>, which is mainly formed by reaction (R3) above. This radical will initiate the recombination reactions towards higher hydrocarbons such as C<sub>2</sub>H<sub>6</sub> and especially C<sub>3</sub>H<sub>8</sub>:



The most important pathways for the production and consumption of ethane (C<sub>2</sub>H<sub>6</sub>) and propane (C<sub>3</sub>H<sub>8</sub>) are illustrated in Figures 10(b) and 10(c), respectively. It is clear that reaction (R7) is the dominant production process for C<sub>3</sub>H<sub>8</sub> (see Figure 10(c)), but reaction (R6) is only responsible for about 11% of the C<sub>2</sub>H<sub>6</sub> production. Indeed, as is apparent from Figure 10(b), C<sub>2</sub>H<sub>6</sub> is mainly (83%) formed by the recombination of two C<sub>2</sub>H<sub>5</sub> radicals:

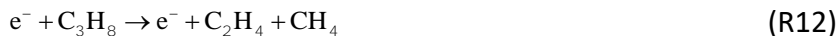


This results from the fact that the overall averaged density of C<sub>2</sub>H<sub>5</sub> ( $7 \times 10^{20} \text{ m}^{-3}$ ) is three orders of magnitude higher than the CH<sub>3</sub> density, while the rate coefficient of reaction (R6) (i.e.,  $1.56 \times 10^{-38} \text{ m}^6 \text{ s}^{-1}$ , or  $3.82 \times 10^{-13} \text{ m}^3 \text{ s}^{-1}$  for a CH<sub>4</sub> gas density of  $2.446 \times 10^{25} \text{ m}^{-3}$ ) is five orders of magnitude higher than the rate coefficient of reaction (R8) (i.e.,  $2.41 \times 10^{-18} \text{ m}^3 \text{ s}^{-1}$ ). Taking into account that the rates of both reactions depend on the square of the concentrations of CH<sub>3</sub> and C<sub>2</sub>H<sub>5</sub>, respectively, it is clear that the rate of reaction (R8) is almost one order of magnitude higher than the rate of reaction (R6).

Electron impact dissociation reactions are the most important loss processes for both C<sub>2</sub>H<sub>6</sub> and C<sub>3</sub>H<sub>8</sub>, leading to the formation of C<sub>2</sub>H<sub>4</sub>, C<sub>2</sub>H<sub>5</sub> and C<sub>3</sub>H<sub>6</sub>:







Especially reaction (R10) is important as loss process for C<sub>2</sub>H<sub>6</sub> (see Figure 10(b)), whereas both reactions (R11) and (R12) contribute nearly equally to the loss of C<sub>3</sub>H<sub>8</sub> (see Figure 10(c)).

**(c) The formation and loss of higher order unsaturated hydrocarbons: C<sub>2</sub>H<sub>4</sub>, C<sub>2</sub>H<sub>2</sub> and C<sub>3</sub>H<sub>6</sub>**

The most important pathways for the production and consumption of C<sub>2</sub>H<sub>4</sub>, C<sub>2</sub>H<sub>2</sub> and C<sub>3</sub>H<sub>6</sub> are plotted in Figures 10(d), 10(e) and 10(f), respectively. The production of C<sub>2</sub>H<sub>4</sub> occurs mainly by the recombination of two C<sub>2</sub>H<sub>5</sub> radicals (i.e., reaction (R8) above) and by electron impact dissociation of C<sub>2</sub>H<sub>6</sub> (i.e., reaction (R10) above). Also electron impact dissociation of C<sub>3</sub>H<sub>8</sub> (i.e., reaction (R12) above) and the recombination of two C<sub>2</sub>H<sub>3</sub> radicals (reaction (R13)) contribute to some extent:



The latter reaction, as well as the electron impact dissociation of C<sub>3</sub>H<sub>6</sub>, are mainly responsible for the production of C<sub>2</sub>H<sub>2</sub>:



Hydrogen attachment reactions are the most important loss processes for both C<sub>2</sub>H<sub>4</sub> and C<sub>2</sub>H<sub>2</sub>, leading to the formation of C<sub>2</sub>H<sub>5</sub> and C<sub>2</sub>H<sub>3</sub> radicals, respectively:





Note in Figure 10(e) also the occurrence of the polymerization reaction of C<sub>2</sub>H<sub>2</sub> resulting in the formation of C<sub>4</sub>H<sub>2</sub>:



Finally, the production of C<sub>3</sub>H<sub>6</sub> occurs mainly by electron impact dissociation of C<sub>3</sub>H<sub>8</sub> (i.e., reaction (R11) above) and to a lower extent also by the recombination of C<sub>3</sub>H<sub>5</sub> radicals with either C<sub>2</sub>H<sub>5</sub> or C<sub>2</sub>H<sub>3</sub>:



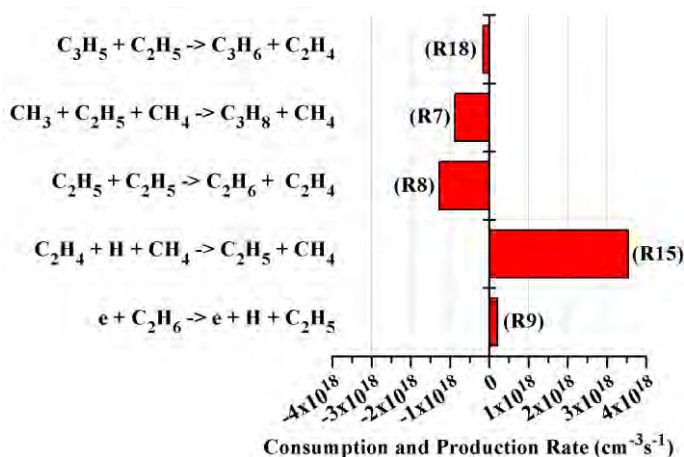
The loss of C<sub>3</sub>H<sub>6</sub> is mainly attributed to electron impact dissociation reactions, leading to the formation of either C<sub>2</sub>H<sub>2</sub> (reaction (R14) above) or C<sub>3</sub>H<sub>5</sub>:



#### **(d) The role of C<sub>2</sub>H<sub>5</sub>: an important radical in the conversion process**

Our calculations predict that C<sub>2</sub>H<sub>5</sub> is present in the discharge at rather high density (see Figure 7), and it plays a significant role in the production and loss of the various hydrocarbon molecules. Therefore, the most important pathways for the production and consumption of this radical are illustrated in Figure 11. C<sub>2</sub>H<sub>5</sub> is mainly (94%) formed by hydrogen attachment to C<sub>2</sub>H<sub>4</sub> (reaction (R15)) and to a lower extent (6%) also by electron impact dissociation of C<sub>2</sub>H<sub>6</sub> (reaction (R9)). The loss of C<sub>2</sub>H<sub>5</sub> is mainly attributed to

radical recombination by reactions (R8), (R7) and (R18), which contribute for 51%, 35% and 6%, respectively. As these reactions result in the formation of C<sub>2</sub>H<sub>4</sub>, C<sub>2</sub>H<sub>6</sub>, C<sub>3</sub>H<sub>6</sub> and C<sub>3</sub>H<sub>8</sub>, this means that the equilibrium established between C<sub>2</sub>H<sub>4</sub>, C<sub>2</sub>H<sub>5</sub>, and C<sub>2</sub>H<sub>6</sub>, which relies on the accuracy of the rate coefficients considered, plays a crucial role.

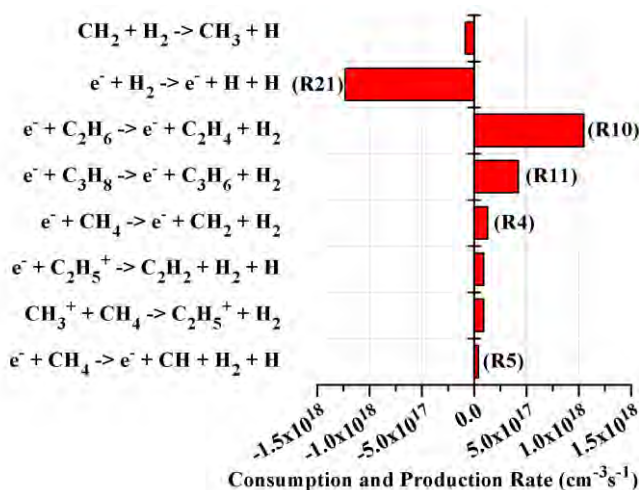


**Figure 11.** The dominant reaction pathways for the production and consumption of C<sub>2</sub>H<sub>5</sub>. The time-averaged production rates are plotted as positive values (i.e., right-hand side of the figure), whereas the time-averaged consumption rates are defined as negative values (i.e., left-hand side of the figure). The most important pathways are labeled, and the labels correspond to the reactions given in the text.

### (e) The formation and loss of H<sub>2</sub>

The most important pathways for the production and consumption of H<sub>2</sub> are illustrated in Figure 12. H<sub>2</sub> is mainly used for the processing of fossil fuels, the production of ammonia and methanol, and as fuel in fuel cells. As appears from Figure 12, H<sub>2</sub> is mainly produced by electron impact dissociation of hydrocarbon molecules. The dissociation reaction of C<sub>2</sub>H<sub>6</sub> (reaction (R10)) appears to be the dominant production mechanism, with a contribution of 56%, whereas the dissociation of C<sub>3</sub>H<sub>8</sub> (reaction (R11)) and CH<sub>4</sub> (reaction (R4))

contribute for 23% and 7%, respectively. Electron impact dissociation is also the dominant loss process for H<sub>2</sub>:

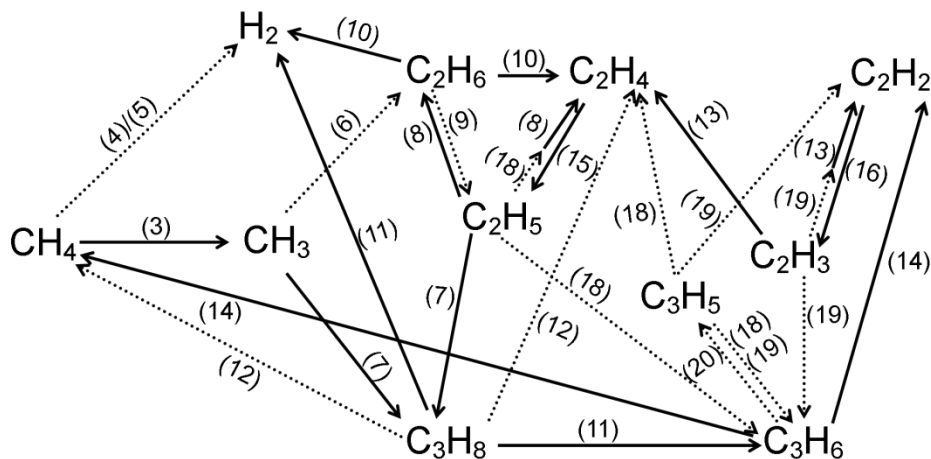


**Figure 12.** The dominant reaction pathways for the production and consumption of H<sub>2</sub>. The time-averaged production rates are plotted as positive values (i.e., right-hand side of the figure), whereas the time-averaged consumption rates are defined as negative values (i.e., left-hand side of the figure). The most important pathways are labeled, and the labels correspond to the reactions given in the text.

#### (f) Summary of the dominant pathways governing the conversion of CH<sub>4</sub> into C<sub>x</sub>H<sub>y</sub> and H<sub>2</sub>

Finally, Figure 13 gives a schematic overview of the dominant reaction pathways for the conversion of CH<sub>4</sub> into higher hydrocarbons and hydrogen gas. Electron impact dissociation of CH<sub>4</sub> resulting in the formation of the methyl radical (CH<sub>3</sub>) starts the conversion process (R3). This methyl radical will initiate recombination reactions towards higher hydrocarbons such as C<sub>2</sub>H<sub>6</sub> and C<sub>3</sub>H<sub>8</sub> (R6, R7). Subsequently, a play of dissociation and recombination

leads to the conversion towards the other, unsaturated hydrocarbons. Finally, dissociation of CH<sub>4</sub> and the higher hydrocarbons also results in the formation of H<sub>2</sub>.



**Figure 13.** Schematic overview of the dominant reaction pathways for the conversion of CH<sub>4</sub> into higher hydrocarbons and hydrogen gas. The most important pathways are depicted with a solid line, less important channels are represented by a dashed line. The labels correspond to the reactions given in the text. Note that C<sub>4</sub>H<sub>2</sub> is not mentioned as it is considered as the sum of all higher polymerized species and also no loss mechanism for it is included in the model.

## 4.6. Conclusion

In this chapter, a detailed plasma chemistry is presented for the conversion of CH<sub>4</sub> into higher hydrocarbon molecules in a DBD reactor. The densities of the various plasma species have been studied as a function of the residence time. The spatially averaged densities of the electrons, ions and radicals show a periodic behavior as a function of time, following the applied voltage. The spatially averaged densities of the molecules do not exhibit a periodic behavior. Indeed, their densities are characterized by a gradual reduction (CH<sub>4</sub>) or increase (higher hydrocarbon molecules and H<sub>2</sub>) each half period

following the maximum of the applied voltage, which results in a more notable decreasing or increasing trend over a longer time-scale.

The density of the background gas, methane, is decreasing due to dissociation (and ionization) reactions governing the conversion process. The calculated and measured conversions of CH<sub>4</sub> as a function of the residence time are illustrated. The dissociation of CH<sub>4</sub> leads to the formation of CH<sub>3</sub>, which is the most important radical in the gas phase chemistry. This methyl radical will initiate the recombination reactions towards higher hydrocarbons. As a result, these molecules are also present in the discharge at high densities.

The calculated and measured yields and selectivities of these higher hydrocarbons (C<sub>2</sub>H<sub>6</sub>, C<sub>2</sub>H<sub>4</sub>, C<sub>2</sub>H<sub>2</sub>, C<sub>3</sub>H<sub>8</sub> and C<sub>3</sub>H<sub>6</sub>) and of H<sub>2</sub> are depicted and a reasonable agreement between our calculation results and the measurements is established. C<sub>2</sub>H<sub>6</sub> and H<sub>2</sub> are the main reaction products of the conversion of CH<sub>4</sub>.

Furthermore, the underlying plasma chemistry of the conversion process is analyzed and the dominant reaction pathways for the consumption of CH<sub>4</sub> and for the production and loss of the various end products are pointed out. It is found that electron impact dissociation of CH<sub>4</sub> resulting in the formation of the methyl radical (CH<sub>3</sub>) initiates the conversion process. Recombination of CH<sub>3</sub> with either another CH<sub>3</sub> radical or with a C<sub>2</sub>H<sub>5</sub> radical will lead to the formation of C<sub>2</sub>H<sub>6</sub> and C<sub>3</sub>H<sub>8</sub>. Dissociation of these higher hydrocarbons leads directly to the formation of other hydrocarbons, but also indirectly by the formation of new radicals, which can subsequently also recombine towards these higher order hydrocarbons. In other words, the conversion of CH<sub>4</sub> is a play of dissociation and recombination reactions leading to a diverse mixture of higher hydrocarbons.



# Chapter 5

## The Conversion of $\text{CH}_4/\text{O}_2$ and $\text{CH}_4/\text{CO}_2$ into Oxygenates and Syngas

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The fluid model described in Chapter 3 is applied here to describe the gas phase chemistry for partial oxidation and for dry reforming of methane. The spatially averaged densities of the various plasma species are presented as a function of time and initial gas mixing ratio. Besides, the conversion of the inlet gases and the selectivities of the reaction products are calculated. Syngas, higher hydrocarbons and higher oxygenates are typically found to be important reaction products. Furthermore, the main underlying reaction pathways for the formation of syngas, methanol, formaldehyde and other higher oxygenates are determined.

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## 5.1. Introduction

In order to convert CH<sub>4</sub> into oxygenates and syngas, the presence of a co-reactant is required. This co-reactant has an important influence on the selectivities of the desired end products. Co-reactants reported in literature for the conversion of methane are oxygen<sup>13, 25, 64-67, 85, 99, 105-106, 120-134</sup>, carbon dioxide<sup>14, 20-21, 64, 93, 107-109, 135-184</sup>, hydrogen<sup>67, 185-186</sup>, steam<sup>165, 168, 187</sup>, nitrogen<sup>188</sup> and others<sup>104, 189-192</sup>. When focusing on the formation of oxygenates and syngas, most research is performed on the partial oxidation with oxygen<sup>13, 25, 65-67, 85, 99, 105-106, 120-134</sup> and on dry reforming (CO<sub>2</sub> reforming)<sup>14, 20-21, 93, 107-109, 135-164, 166-167, 169-184</sup>. In this chapter a modeling study for the conversion of CH<sub>4</sub> in the presence of O<sub>2</sub> or CO<sub>2</sub> into higher oxygenates and syngas will be discussed.

Of course, oxygen is very effective for low temperature plasma activation of methane. However, a possible drawback is an excessive oxidation, resulting in the formation of CO<sub>2</sub> and a wide variety of oxygenates. Therefore, the use of CO<sub>2</sub> as a milder oxidant can sometimes be more preferable, depending on the desired end product(s). Moreover, with CO<sub>2</sub> as a co-reactant the two most important greenhouse gases are converted in the process. Current interests in CO<sub>2</sub> utilization include hydrogenation of CO<sub>2</sub> (see also Chapter 6) and the reforming of CH<sub>4</sub> by CO<sub>2</sub>.

Experimental results on the conversion in CH<sub>4</sub>/O<sub>2</sub><sup>13, 25, 65-67, 85, 99, 105-106, 120-134</sup> and CH<sub>4</sub>/CO<sub>2</sub><sup>14, 20-21, 93, 107-108, 135-164, 166-167, 169-170, 173-176, 180, 182-184</sup> plasmas show that the typical end products are C<sub>x</sub>H<sub>y</sub>, H<sub>2</sub> and CO, and to a lower extent also CH<sub>3</sub>OH, CH<sub>2</sub>O and other higher oxygenates (acids, alcohols, aldehydes, esters, ketones, ...). The H<sub>2</sub>/CO ratio and the yield of higher hydrocarbons and oxygenates seems to be very dependent on the CH<sub>4</sub>/O<sub>2</sub> or CH<sub>4</sub>/CO<sub>2</sub> feed ratio.

In most papers the focus is largely on the formation of C<sub>x</sub>H<sub>y</sub> and syngas. Only a few papers explicitly focus on the formation of CH<sub>3</sub>OH, CH<sub>2</sub>O and other higher oxygenates.<sup>14, 25, 64-67, 105-107, 121-122, 126-127, 129, 133-134, 137, 143, 147, 158, 162, 173, 175</sup>

Modeling results on the plasma chemistry in CH<sub>4</sub>/O<sub>2</sub> and CH<sub>4</sub>/CO<sub>2</sub> mixtures reported in literature mostly originate from zero-dimensional simulations, largely based on specific empirical input, which is only valid for the experimental set-up under study.<sup>20, 25, 85-86, 89, 93, 99, 101, 104-107, 109</sup> Zhou et al. used a semi-empirical kinetic model to simulate the accumulated chemical action of many microdischarges in CH<sub>4</sub>/O<sub>2</sub><sup>85</sup> and CH<sub>4</sub>/CO<sub>2</sub><sup>20</sup> gas mixtures. Besides the densities of the inlet gases and main products, the pathways for formation of methanol in CH<sub>4</sub>/O<sub>2</sub> and syngas in CH<sub>4</sub>/CO<sub>2</sub> were briefly discussed. Nair et al.<sup>99</sup>, Matin et al.<sup>101</sup>, Agiral et al.<sup>25</sup>, Goujard et al.<sup>105</sup> and Zhou et al.<sup>106</sup> used a semi-empirical kinetic model to simulate the conversion in a CH<sub>4</sub>/O<sub>2</sub> non-thermal plasma. Agiral et al.<sup>25</sup> briefly discussed the mechanisms of the gas-to-liquid process governing the formation of oxygenates. Goujard et al.<sup>105</sup> performed calculations for two different temperatures and discussed the main underlying pathways for the formation of higher oxygenates at these temperatures. Kraus et al.<sup>104</sup> and Luche et al.<sup>89</sup> used a semi-empirical kinetic model to simulate the conversion in a CH<sub>4</sub>/CO<sub>2</sub> and a CH<sub>4</sub>/air non-thermal plasma, respectively. Goujard et al. applied a simplified global kinetic model to study the helium dilution effect on CO<sub>2</sub> reforming of CH<sub>4</sub> in a DBD.<sup>107</sup> Within our group PLASMANT, Snoeckx et al. performed a computational study ranging from the nanoseconds to seconds time-scale for the conversion of CH<sub>4</sub> and CO<sub>2</sub> into value-added chemicals in a DBD.<sup>109</sup> A zero-dimensional chemical kinetics model was applied to study the plasma chemistry in a 1:1 CH<sub>4</sub>/CO<sub>2</sub> gas mixture. The calculations were first

performed for one microdischarge pulse and its afterglow. Subsequently, long time-scale simulations were carried out, corresponding to real residence times in the plasma, assuming a large number of consecutive microdischarge pulses. The conversion of CH<sub>4</sub> and CO<sub>2</sub> as well as the selectivity of the formed products were calculated and compared to experiments for a range of different powers and gas flow rates. In a follow-up paper, this model was applied to a wide range of conditions, including gas mixing ratio, gas residence time, power and frequency, to investigate which conditions give rise to the best conversion and energy efficiency.<sup>181</sup> Machrafi et al. performed calculations for a 1:1 CH<sub>4</sub>/CO<sub>2</sub> gas mixture<sup>108</sup> by means of a so-called 3D “Incompressible Navier-Stokes” model with strongly reduced kinetic mechanism, in order to determine the velocity fields. This model was combined with a convection-diffusion model in order to study the behavior of the inlet gases. Qualitative densities were shown, as it was not possible to have a huge kinetic precision using a 3D model. Wang et al. conducted a density functional theory (DFT) study to investigate the reaction mechanisms for the synthesis of oxygenates and higher hydrocarbons from CH<sub>4</sub> and CO<sub>2</sub> using cold plasmas.<sup>94</sup> The main dissociation routes of the reactants were analyzed and the formation of various products, including syngas, higher hydrocarbons and oxygenates, was discussed. Istadi et al. developed a hybrid artificial neural network-genetic algorithm to simulate and optimize a catalytic-DBD plasma reactor in a CH<sub>4</sub>/CO<sub>2</sub> gas mixture.<sup>97</sup> The effects of the CH<sub>4</sub>/CO<sub>2</sub> feed ratio, total feed flow rate, discharge voltage and reactor wall temperature on the conversion of the inlet gases and the selectivities of the main products were investigated. Recently, Janeco et al.<sup>178</sup> performed a study on the electron kinetics in He/CH<sub>4</sub>/CO<sub>2</sub> mixtures, including the contribution of H<sub>2</sub> and CO formed in the discharge, as an initial step to model the reforming

of natural gas for syngas production in a DBD. The electron Boltzmann equation for a swarm in the hydrodynamic regime was solved in mixtures of  $\text{He}/\text{CH}_4/\text{CO}_2/\text{CO}/\text{H}_2$ . The method used in this work takes into account nonconservative terms and the full angular dependency of the electron velocity distribution function.

In order to achieve our goal, i.e., to describe in detail the plasma chemistry in an atmospheric pressure DBD in different  $\text{CH}_4/\text{O}_2$  and  $\text{CH}_4/\text{CO}_2$  gas mixtures, the 1D fluid model used to describe the plasma chemistry for an atmospheric pressure DBD in pure methane (see Chapter 4) was extended. Unlike in most of the above-cited papers, we focus in detail on the main underlying pathways governing the conversion to higher oxygenates, and moreover, we make a comparison of those pathways between a mixture with  $\text{O}_2$  and a mixture with  $\text{CO}_2$ .

In this chapter we present the most important results on the partial oxidation and the dry reforming of  $\text{CH}_4$  into syngas, higher oxygenates and higher hydrocarbons. First, the spatially averaged electron and radical densities as a function of time will be illustrated. Furthermore, the densities of the reaction products for a range of different initial gas mixing ratios, as well as the conversion of the inlet gases, will be discussed. Finally, the main underlying reaction pathways for the formation of syngas, methanol and formaldehyde, which appear to be the main oxygenates produced, will be pointed out.

## 5.2. Species Included in the Model

The chemistry in a CH<sub>4</sub>/O<sub>2</sub> and CH<sub>4</sub>/CO<sub>2</sub> gas mixture is described by 75 species (electrons, molecules, ions and radicals). As mentioned above, the model for pure CH<sub>4</sub> (see Chapter 4) is extended. O<sub>2</sub> and CO<sub>2</sub> are included as extra feed gases. Furthermore, CO, H<sub>2</sub>O, CH<sub>2</sub>O, CH<sub>3</sub>OH and some other higher oxygenates are considered in the model, as they might be formed in the plasma. Note that formic acid (HCOOH) and acetic acid (CH<sub>3</sub>COOH), which were experimentally found, are not included in the model as the rate constants for the formation and loss processes for these molecules are not well known. Similar to the model for pure CH<sub>4</sub>, the radical and ionic species corresponding to the formation products of dissociation, ionization and attachment reactions of the molecules are also taken into account. Although some vibrational and electronic excitation reactions are included in the model, vibrationally and electronically excited species are not taken into account separately, in order to limit the number of species and reactions (see also Chapter 4). Also rotationally excited species are not taken into account in the model. Indeed, the electron energy required for rotational excitations is negligible compared with this for vibrational excitations.<sup>70, 110</sup> Table 5 presents an overview of the different species taken into account in the model.

**Table 5. Overview of the species included in the model, besides the electrons.**

Molecules	CH <sub>4</sub> , C <sub>2</sub> H <sub>6</sub> , C <sub>2</sub> H <sub>4</sub> , C <sub>2</sub> H <sub>2</sub> , C <sub>2</sub> , C <sub>3</sub> H <sub>8</sub> , C <sub>3</sub> H <sub>6</sub> , C <sub>4</sub> H <sub>2</sub> , H <sub>2</sub> , O <sub>3</sub> , O <sub>2</sub> , CO <sub>2</sub> , CO, H <sub>2</sub> O, H <sub>2</sub> O <sub>2</sub> , CH <sub>2</sub> O, CH <sub>3</sub> OH, C <sub>2</sub> H <sub>5</sub> OH, CH <sub>3</sub> CHO, CH <sub>2</sub> CO, CH <sub>3</sub> OOH, C <sub>2</sub> H <sub>5</sub> OOH
Ions	CH <sub>5</sub> <sup>+</sup> , CH <sub>4</sub> <sup>+</sup> , CH <sub>3</sub> <sup>+</sup> , CH <sub>2</sub> <sup>+</sup> , CH <sup>+</sup> , C <sup>+</sup> , C <sub>2</sub> H <sub>6</sub> <sup>+</sup> , C <sub>2</sub> H <sub>5</sub> <sup>+</sup> , C <sub>2</sub> H <sub>4</sub> <sup>+</sup> , C <sub>2</sub> H <sub>3</sub> <sup>+</sup> , C <sub>2</sub> H <sub>2</sub> <sup>+</sup> , C <sub>2</sub> H <sup>+</sup> , C <sub>2</sub> <sup>+</sup> , H <sub>3</sub> <sup>+</sup> , H <sub>2</sub> <sup>+</sup> , H <sup>+</sup> , O <sub>4</sub> <sup>+</sup> , O <sub>2</sub> <sup>+</sup> , O <sup>+</sup> , O <sub>4</sub> <sup>-</sup> , O <sub>3</sub> <sup>-</sup> , O <sub>2</sub> <sup>-</sup> , O <sup>-</sup> , CO <sub>2</sub> <sup>+</sup> , CO <sup>+</sup> , H <sub>3</sub> O <sup>+</sup> , H <sub>2</sub> O <sup>+</sup> , OH <sup>+</sup> , H <sup>-</sup> , OH <sup>-</sup>
Radicals	CH <sub>3</sub> , CH <sub>2</sub> , CH, C, C <sub>2</sub> H <sub>5</sub> , C <sub>2</sub> H <sub>3</sub> , C <sub>2</sub> H, C <sub>3</sub> H <sub>7</sub> , C <sub>3</sub> H <sub>5</sub> , H, O, OH, HO <sub>2</sub> , CHO, CH <sub>2</sub> OH, CH <sub>3</sub> O, C <sub>2</sub> H <sub>5</sub> O, C <sub>2</sub> HO, CH <sub>3</sub> CO, CH <sub>2</sub> CHO, CH <sub>3</sub> O <sub>2</sub> , C <sub>2</sub> H <sub>5</sub> O <sub>2</sub>

### 5.3. Reactions Included in the Model

The 75 species can interact with each other through a large number of reactions. 1019 gas phase reactions, including 157 electron-neutral, 48 electron-ion, 476 neutral-neutral and 338 ion-ion or ion-neutral reactions, are considered. An overview of the reactions is given in the Appendices.

Like in Chapter 4, the rates of the different reactions are calculated from the densities of the colliding species and the corresponding reaction rate coefficients. The electron-neutral and electron-ion reactions are again treated by energy dependent reaction rate coefficients. The rate coefficients of the electron-neutral reactions are obtained from look-up tables calculated with the Boltzmann solver Bolsig+<sup>74</sup>, based on the energy dependent collision cross sections for these reactions. The references for the cross sections can also be found in Table A.1. of the Appendices. The lookup tables for the electron-ion dissociative recombination reactions are built using the functions in combination with the branching ratios for the different channels, of which a detailed overview is given in Table A.2. of the Appendices. The neutral-neutral and ion-neutral reactions are again defined in the model with a constant reaction rate coefficient at a pressure and temperature of 1 atm and 300 K, respectively. These rate coefficients and their corresponding references are summarized in Table A.3. and Table A.4. of the Appendices, respectively.

### 5.4. Operating Conditions

The calculations are carried out for a gas residence time up to 20s, at a fixed applied voltage of 5 kV and a frequency of 10 kHz. The  $\text{CH}_4/\text{CO}_2$  molar ratio is

varied in the range of 5-80%  $\text{CO}_2$ , while the  $\text{CH}_4/\text{O}_2$  molar ratio is varied from 10 to 30%  $\text{O}_2$ . The  $\text{CH}_4/\text{CO}_2$  molar ratio can be varied in a much wider range than the  $\text{CH}_4/\text{O}_2$  molar ratio, because the latter approaches the upper flammability or explosion limit when the mole fraction of  $\text{CH}_4$  in pure  $\text{O}_2$  reaches 61 mole%.<sup>193</sup>

## 5.5. Results and Discussion

### 5.5.1. Densities of the Plasma Species

Figure 14 illustrates the periodic behavior as a function of time of the spatially averaged electron density for a 70/30 (a) and 90/10 (b)  $\text{CH}_4/\text{O}_2$  gas mixture and for a 70/30 (c) and 90/10 (d)  $\text{CH}_4/\text{CO}_2$  gas mixture, on a logarithmic scale, for four periods of the applied voltage. The applied voltage as a function of time is also plotted, for the sake of clarity. In the 70/30  $\text{CH}_4/\text{O}_2$  mixture, breakdown in the gas appears once each period following the applied voltage, while in the 90/10  $\text{CH}_4/\text{O}_2$  mixture and the 70/30  $\text{CH}_4/\text{CO}_2$  mixture, a breakdown appears each half period, and in the 90/10  $\text{CH}_4/\text{CO}_2$  mixture, even more breakdowns occur (see below). The electron density behavior is different for the positive and the negative polarity of the applied voltage, which is due to the dissimilarity in surface dimensions and properties of the inner and outer electrode (i.e., only the outer electrode is covered by a dielectric), as was also discussed in Section 4.5.1. above.

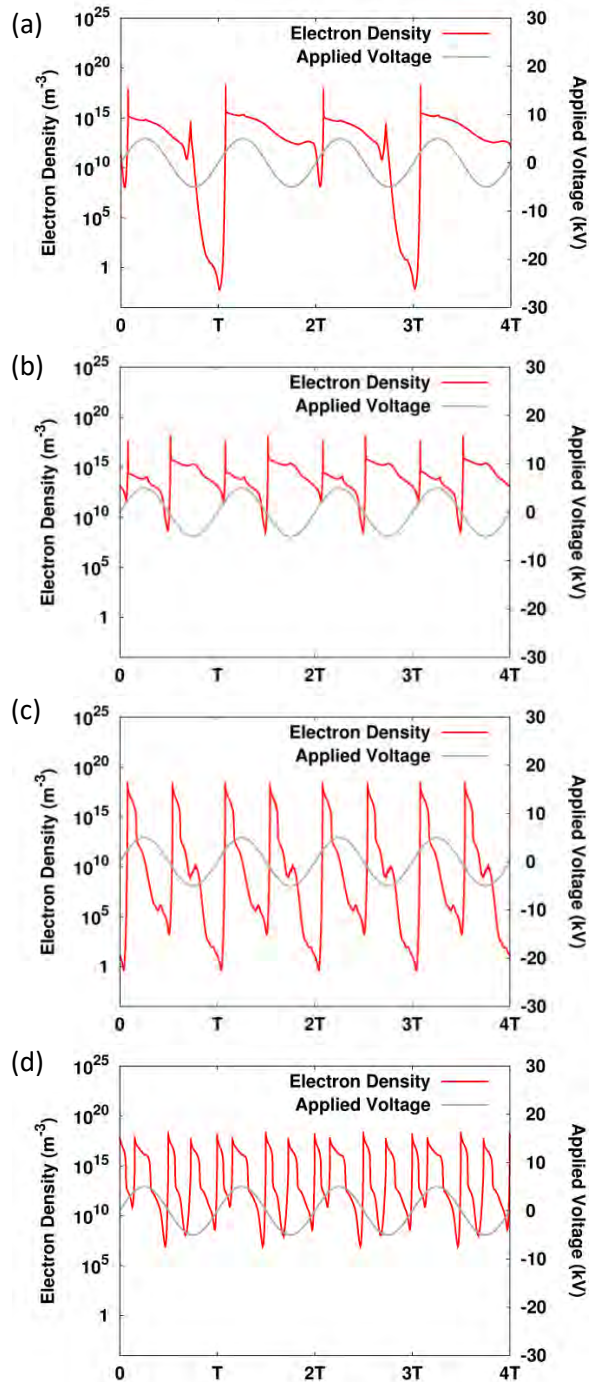


Figure 14. Spatially averaged electron density on a logarithmic scale for a 70/30 (a) and 90/10 (b)  $\text{CH}_4/\text{O}_2$  gas mixture and for a 70/30 (c) and 90/10 (d)  $\text{CH}_4/\text{CO}_2$  gas mixture, as a function of time, for four periods of the applied voltage. The applied sinusoidal voltage is also presented, for the sake of clarity.



As mentioned above, in the mixtures with CO<sub>2</sub> twice as many breakdowns appear, compared to the corresponding mixtures with O<sub>2</sub>. The figures (a ↔ c, b ↔ d) also illustrate the different periodical behavior. Furthermore, the number of breakdowns is also twice as large for the mixtures with 90 % CH<sub>4</sub> (b and d) compared to the corresponding mixtures with 70 % CH<sub>4</sub> (a and c). The same behavior was also observed for the current profiles and the charging of the electrodes, and can be attributed to the different degree of electronegativity of the various gas mixtures and mixing ratios (see below).

It is also clear from the figures that for the mixtures with 90 % CH<sub>4</sub> (b and d) the minimum electron density is much higher than for the mixtures with 70 % CH<sub>4</sub> (a and c). Nevertheless, the overall spatially and time averaged electron density is almost the same for either 90% or 70% CH<sub>4</sub>, and amounts to ca.  $10^{15} \text{ m}^{-3}$  for the CH<sub>4</sub>/O<sub>2</sub> mixture and to ca.  $10^{16} \text{ m}^{-3}$  for the CH<sub>4</sub>/CO<sub>2</sub> mixture. This is one and two orders of magnitude lower than the calculated value of  $10^{17} \text{ m}^{-3}$  for a pure CH<sub>4</sub> plasma (see Section 4.5.1.), and the reason for this is given below.

The overall spatially and time averaged mean electron energy in the CH<sub>4</sub>/O<sub>2</sub> and CH<sub>4</sub>/CO<sub>2</sub> gas mixtures was calculated to be about 1.6 eV and 2.1 eV, respectively, compared to about 2 eV in pure CH<sub>4</sub> (see Section 4.5.1.). These differences in electron density and mean electron energy between CH<sub>4</sub>/O<sub>2</sub> and CH<sub>4</sub>/CO<sub>2</sub> can be attributed to the fact that CH<sub>4</sub>/O<sub>2</sub> gives rise to an electronegative plasma in contrast to CH<sub>4</sub>/CO<sub>2</sub> and pure CH<sub>4</sub>. Indeed, the (positive and negative) ion density is three orders of magnitude higher than the electron density in CH<sub>4</sub>/O<sub>2</sub>, while in CH<sub>4</sub>/CO<sub>2</sub> the electron density is in the same order of magnitude as the positive ion density and one order of magnitude higher than the negative ion density. This can be explained

because in  $\text{CH}_4/\text{O}_2$  the electrons are more easily trapped by attachment reactions with  $\text{O}_2$ , and moreover, the higher energy electrons are more frequently consumed in ionization and dissociation reactions, as the threshold energies for these reactions are much lower in  $\text{CH}_4/\text{O}_2$ <sup>194-195</sup> than in  $\text{CH}_4/\text{CO}_2$ <sup>196</sup>. Thus, the  $\text{CH}_4/\text{O}_2$  plasma is most electronegative, containing the highest negative ion density, and this explains the lower (spatially and time averaged) electron density than in the  $\text{CH}_4/\text{CO}_2$  plasma (which still contains some negative ions), and especially compared to the pure  $\text{CH}_4$  plasma (which virtually does not contain negative ions).

The number densities of the radicals and ions, produced by collisions of the electrons with the gas molecules, exhibit the same periodic behavior as the electron density, as is illustrated in Figure 15 for the radicals, for a 70/30  $\text{CH}_4/\text{O}_2$  (a, b) gas mixture and a 70/30  $\text{CH}_4/\text{CO}_2$  (c, d) gas mixture. However, this periodic trend is superimposed on a rising or declining trend, acting over a longer time-scale until periodic steady state is reached.

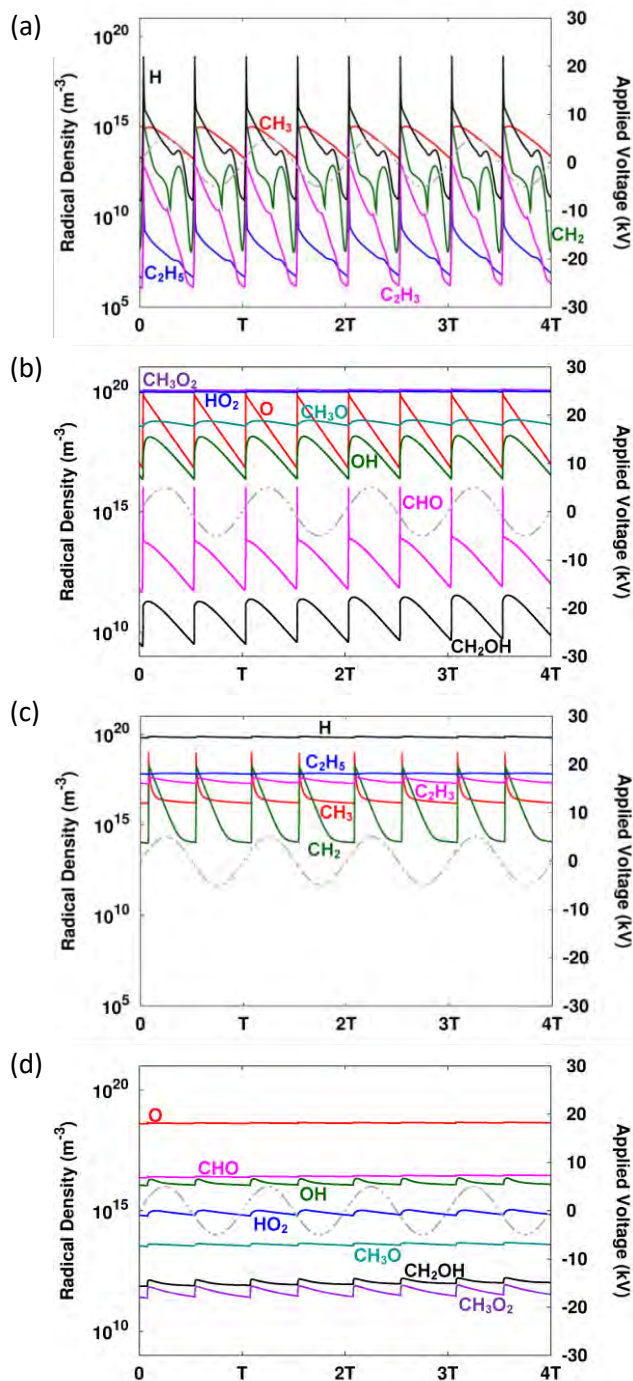


Figure 15. Spatially averaged radical densities (left axis) as a function of time for a 70/30  $\text{CH}_4/\text{O}_2$  (a, b) gas mixture and for a 70/30  $\text{CH}_4/\text{CO}_2$  (c, d) gas mixture, as well as the applied sinusoidal voltage (gray, right axis) for four periods of the applied voltage.

It is clear from Figure 15 that the densities of some radicals, such as O, OH, CHO, CH<sub>2</sub>OH, C<sub>2</sub>H<sub>5</sub>, C<sub>2</sub>H<sub>3</sub> and H in the CH<sub>4</sub>/O<sub>2</sub> gas mixture, and CH<sub>3</sub> and CH<sub>2</sub> in both gas mixtures, vary over several orders of magnitude throughout a period. This is because their formation or loss (e.g., H radicals are consumed in reactions with O<sub>2</sub>) is strongly dependent on electron impact dissociation of one of the inlet gases. On the other hand, the densities of radicals which are not directly formed by electron impact dissociation of one of the inlet gases, such as C<sub>2</sub>H<sub>5</sub>, C<sub>2</sub>H<sub>3</sub>, H, O, OH, CHO, CH<sub>2</sub>OH in the CH<sub>4</sub>/CO<sub>2</sub> gas mixture, and HO<sub>2</sub>, CH<sub>3</sub>O and CH<sub>3</sub>O<sub>2</sub> in both gas mixtures, vary by less than one order of magnitude throughout a period. The overall spatially and time averaged radical densities vary from about 10<sup>8</sup> m<sup>-3</sup> for the less abundant radicals, to about 10<sup>19</sup> m<sup>-3</sup> for the most abundant radicals. The most abundant radicals in the CH<sub>4</sub>/O<sub>2</sub> gas mixture are O, OH, HO<sub>2</sub>, CH<sub>3</sub>O and CH<sub>3</sub>O<sub>2</sub>, while H, O, CH<sub>3</sub>, CH<sub>2</sub>, C<sub>2</sub>H<sub>5</sub> and C<sub>2</sub>H<sub>3</sub> are mostly abundant in the CH<sub>4</sub>/CO<sub>2</sub> gas mixture (see also below). This will determine the different reaction pathways for the formation of the oxygenates in the CH<sub>4</sub>/O<sub>2</sub> and CH<sub>4</sub>/CO<sub>2</sub> gas mixtures, as will be elaborated in Section 5.5.3. below.

Figure 16 shows the spatially and time averaged radical densities as a function of the initial gas mixing ratio in both the CH<sub>4</sub>/O<sub>2</sub> and CH<sub>4</sub>/CO<sub>2</sub> gas mixtures. It is clear that the mixtures with CO<sub>2</sub>, at an identical initial fraction of CH<sub>4</sub>, yield higher densities of C<sub>x</sub>H<sub>y</sub>, H, CHO and CH<sub>2</sub>OH radicals than the mixtures with O<sub>2</sub>, while the densities of O, OH, HO<sub>2</sub>, CH<sub>3</sub>O and CH<sub>3</sub>O<sub>2</sub> are higher in the mixtures with O<sub>2</sub> than in the mixtures with CO<sub>2</sub>. This can be explained because the net formation of C<sub>x</sub>H<sub>y</sub> directly or indirectly from CH<sub>4</sub> is higher in the mixtures with CO<sub>2</sub>. Furthermore, the formed H, CHO and CH<sub>2</sub>OH radicals immediately react with O<sub>2</sub> into HO<sub>2</sub>, CO and CH<sub>2</sub>O, respectively, and

therefore the net formation of H, CHO and CH<sub>2</sub>OH is higher in the mixtures with CO<sub>2</sub>. Likewise, the O, OH, HO<sub>2</sub>, CH<sub>3</sub>O and CH<sub>3</sub>O<sub>2</sub> radicals are directly or indirectly formed from O<sub>2</sub> (see Section 5.5.3. below), which explains their higher density in the CH<sub>4</sub>/O<sub>2</sub> mixtures. Upon rising initial fraction of CO<sub>2</sub> between 5 and 80 %, the densities of the C<sub>x</sub>H<sub>y</sub> radicals and of the H atoms drop by half an order to one order of magnitude, due to the fact that these radicals are directly or indirectly formed out of CH<sub>4</sub>. A similar trend is observed upon rising fraction of O<sub>2</sub>. On the other hand, the densities of O, OH and other O-containing radicals increase by half an order to several orders of magnitude upon rising fraction of CO<sub>2</sub> in the gas mixture, which can be explained by the fact that these radicals are directly or indirectly formed out of CO<sub>2</sub>. For the same reason, the densities of the O and OH radicals slightly increase upon rising fraction of O<sub>2</sub> in the gas mixture, while the other O-containing radicals decrease by half an order to several orders of magnitude. The latter can be explained by the fact that a higher inlet fraction of O<sub>2</sub> leads towards full oxidation of CH<sub>4</sub> (see also Figure 17 below).

The ion densities also exhibit a similar periodic behavior as the electrons, which is logical, as they are mostly formed by electron impact ionization or by (dissociative) attachment from the inlet gases, for the positive and negative ions, respectively. The most abundant ions in the CH<sub>4</sub>/O<sub>2</sub> gas mixtures are CH<sub>5</sub><sup>+</sup>, C<sub>2</sub>H<sub>5</sub><sup>+</sup>, O<sub>4</sub><sup>+</sup>, H<sub>3</sub>O<sup>+</sup>, O<sub>2</sub><sup>-</sup>, O<sub>4</sub><sup>-</sup> and OH<sup>-</sup>, while CH<sub>5</sub><sup>+</sup>, C<sub>2</sub>H<sub>5</sub><sup>+</sup> and OH<sup>-</sup> are the most abundant ions in the CH<sub>4</sub>/CO<sub>2</sub> gas mixtures. Their spatially and time averaged densities are in the order of 10<sup>17</sup> m<sup>-3</sup> and 10<sup>16</sup> m<sup>-3</sup> for the CH<sub>4</sub>/O<sub>2</sub> and CH<sub>4</sub>/CO<sub>2</sub> gas mixtures, respectively. This is typically 2 or 3 orders of magnitude lower than the spatially and time averaged densities of the most abundant radicals in both gas mixtures, indicating that the ions play a minor role in the plasma

chemistry (see Section 5.5.3. below). Therefore, we do not go in further detail on the ion densities.

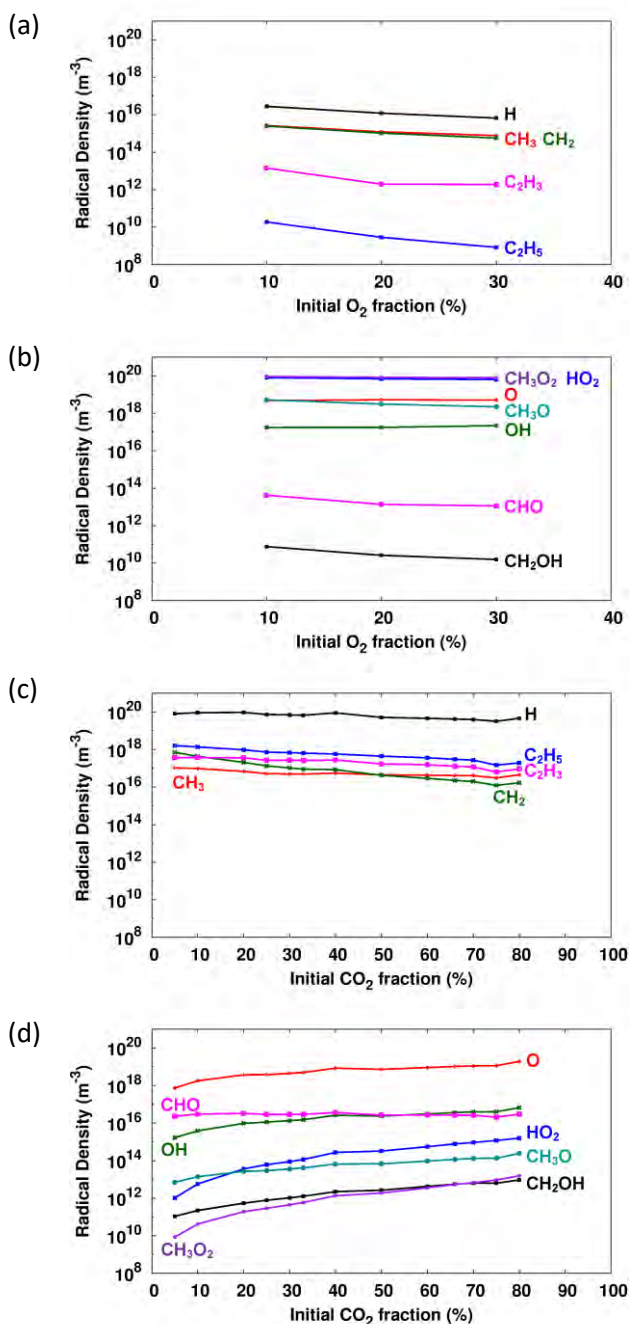
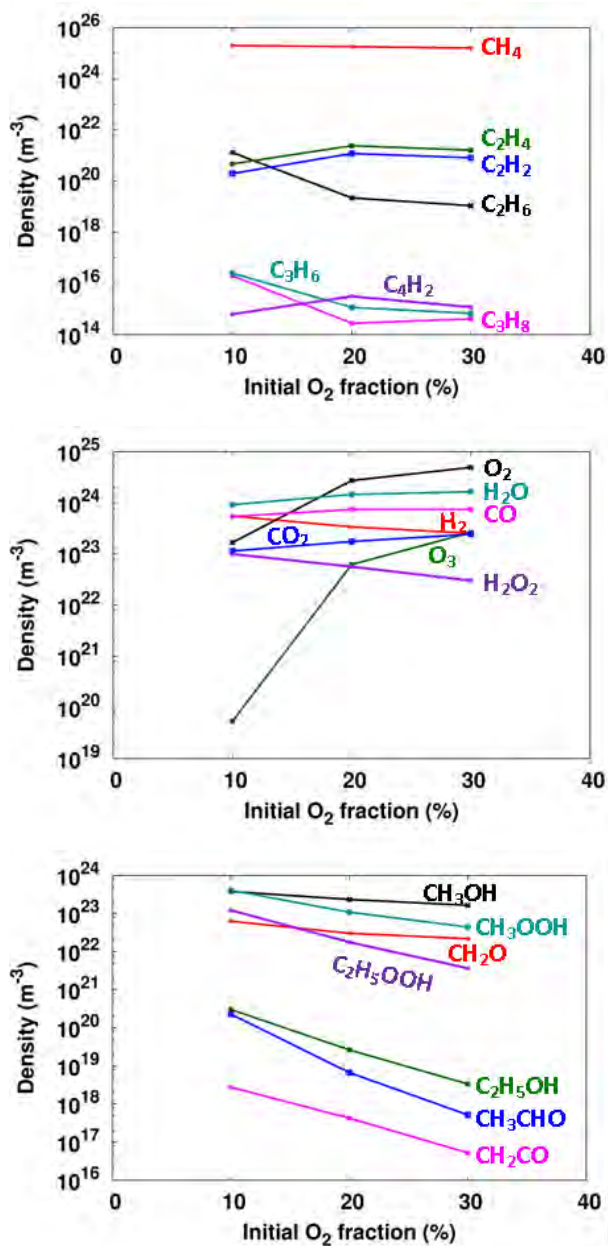


Figure 16. Spatially and time averaged radical densities as a function of the initial gas mixing ratio for the  $\text{CH}_4/\text{O}_2$  (a, b) and  $\text{CH}_4/\text{CO}_2$  (c, d) gas mixtures.

$\text{CH}_4/\text{O}_2$ 

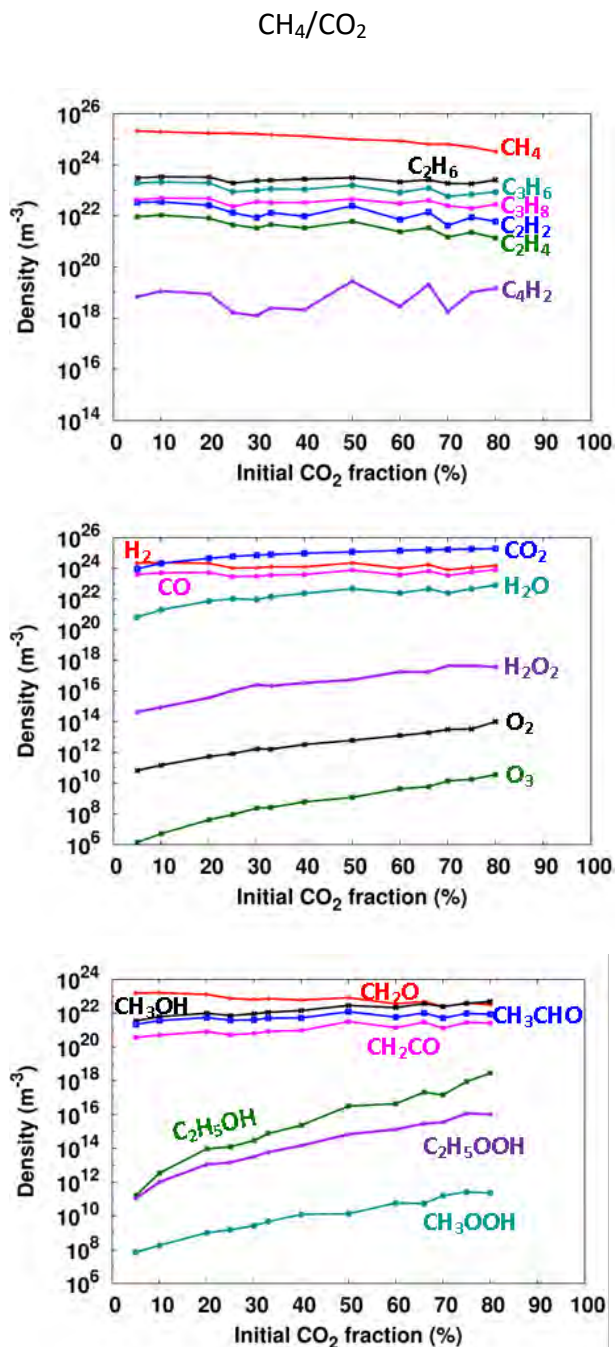


Figure 17. Spatially averaged molecule densities as a function of the initial gas mixing ratio, after a residence time of 5 seconds, for the  $\text{CH}_4/\text{O}_2$  (left panel) and  $\text{CH}_4/\text{CO}_2$  (right panel) gas mixtures.



The molecules do not exhibit such a periodic behavior as the electrons, as they are not directly correlated with the electron density and electron energy, because they are typically formed by recombination of the radicals (see Section 5.5.3. below). The densities of the molecules formed from the inlet gases, i.e.,  $\text{H}_2$ ,  $\text{CO}$ , higher order hydrocarbons and oxygenates, exhibit a rising trend as a function of time, during each half period of the applied voltage, because their net production is higher than their net consumption. The inlet gases, on the other hand, have a higher net consumption, so they are characterized by a gradual decrease in their densities during each half period. It appears that the conversion is most pronounced in the first few seconds and that the densities of the molecules do not significantly change anymore for a longer residence time. Below, we present the densities as a function of time, but here we first focus on the densities of the different end products as a function of the initial gas mixing ratio after a certain residence time.

Figure 17 illustrates the densities of the various molecules as a function of the initial gas mixing ratio, after a residence time of 5 seconds, for the  $\text{CH}_4/\text{O}_2$  (left panel) and  $\text{CH}_4/\text{CO}_2$  (right panel) gas mixtures. A residence time of 5 s corresponds to a gas flow rate of  $0.2 \text{ L}\cdot\text{min}^{-1}$  for the plasma reactor under study. It is clear that the densities of the higher hydrocarbons ( $\text{C}_x\text{H}_y$ ), as well as  $\text{H}_2$ ,  $\text{CH}_2\text{O}$  (formaldehyde),  $\text{CH}_3\text{CHO}$  (acetaldehyde) and  $\text{CH}_2\text{CO}$  (ketene or ethenone) are higher in the mixtures with  $\text{CO}_2$ , while the densities of  $\text{O}_3$ ,  $\text{H}_2\text{O}$ ,  $\text{H}_2\text{O}_2$  (hydrogen peroxide),  $\text{CH}_3\text{OH}$  (methanol),  $\text{C}_2\text{H}_5\text{OH}$  (ethanol),  $\text{CH}_3\text{OOH}$  (methyl hydroperoxide) and  $\text{C}_2\text{H}_5\text{OOH}$  (ethyl hydroperoxide) are higher in the mixtures with  $\text{O}_2$ .  $\text{CO}$  is formed at high density in both gas mixtures and therefore the  $\text{H}_2/\text{CO}$  ratio is higher than 1 in the mixtures with  $\text{CO}_2$  and lower

than 1 in the mixtures with  $\text{O}_2$ . Note that in the gas mixtures with  $\text{O}_2$  as a co-reactant also a significant amount of undesired  $\text{CO}_2$  is formed.

These results are in good agreement with reported results in literature on the formation of oxygenates in  $\text{CH}_4/\text{O}_2$  and  $\text{CH}_4/\text{CO}_2$  in discharges at similar conditions. Larkin et al.<sup>64-67</sup> discussed the formation of  $\text{CO}$ ,  $\text{CO}_2$ ,  $\text{CH}_3\text{OH}$ ,  $\text{CH}_2\text{O}$ ,  $\text{HCOOH}$  (formic acid) and  $\text{CH}_3\text{COOH}$  (acetic acid) in  $\text{CH}_4/\text{O}_2$  in a plasma reactor surrounded by a water cooling jacket to increase the formation of liquid oxygenates. They also showed that in the presence of enough  $\text{O}_2$  the selectivity of  $\text{C}_x\text{H}_y$  will remain low. Okumoto et al.<sup>121-122</sup> made use of dilution gases to enhance the formation of oxygenates in  $\text{CH}_4/\text{O}_2$  and reported the formation of  $\text{C}_x\text{H}_y$ ,  $\text{CO}$ ,  $\text{CO}_2$ ,  $\text{H}_2$ ,  $\text{H}_2\text{O}$ ,  $\text{CH}_3\text{OH}$ ,  $\text{CH}_2\text{O}$  and  $\text{CH}_3\text{CHO}$ . Nozaki et al.<sup>126, 133-134</sup>, Goujard et al.<sup>105</sup> and Agiral et al.<sup>25</sup> carried out experiments for  $\text{CH}_4/\text{O}_2$  gas mixtures in a microplasma reactor, which was immersed into a water bath maintained near room temperature, to enhance the condensation of liquid components on the cooled reactor wall. Furthermore, they intermittently injected distilled water in addition to the inlet gases in order to wash out these liquid components and they collected all condensable components at the end of the reactor by a cold trap. They found that if oxygen was totally consumed, so after a long residence time, or when the inlet oxygen fraction was excessively high, the main products were  $\text{CO}$ ,  $\text{CO}_2$  and  $\text{H}_2\text{O}$ . Besides, also the formation of  $\text{H}_2$ ,  $\text{C}_x\text{H}_y$ ,  $\text{HCOOH}$ ,  $\text{H}_2\text{O}_2$ ,  $\text{CH}_3\text{OOH}$ ,  $\text{CH}_3\text{OH}$  and  $\text{CH}_2\text{O}$  were reported, and the concentration of  $\text{CH}_3\text{OH}$  was much higher than that of  $\text{CH}_2\text{O}$  without the cooling, which is in good agreement with our results. However, the selectivity of  $\text{CH}_2\text{O}$  and  $\text{HCOOH}$  drastically increased when cooling the reactor. Indarto et al.<sup>127, 129</sup> discussed the formation of  $\text{H}_2$ ,  $\text{CO}$ ,  $\text{CO}_2$ ,  $\text{H}_2\text{O}$ ,  $\text{C}_x\text{H}_y$  and  $\text{CH}_3\text{OH}$  in  $\text{CH}_4/\text{O}_2$  and found that a

proper selection of catalyst can drastically enhance the yield and selectivity of CH<sub>3</sub>OH. Our results are also in reasonable agreement with the results reported by Zhou et al.<sup>106</sup> comparing the use of a single and a double dielectric plasma reactor for the direct oxidation of CH<sub>4</sub> to H<sub>2</sub>O<sub>2</sub> and oxygenates, where the double dielectric reactor favored the formation of these products.

The conversion of CH<sub>4</sub> in the presence of CO<sub>2</sub> is much less reported. Zou et al.<sup>14</sup> discussed the formation of CO, H<sub>2</sub>, C<sub>x</sub>H<sub>y</sub>, H<sub>2</sub>O, CH<sub>2</sub>O, CH<sub>3</sub>OH, C<sub>2</sub>H<sub>5</sub>OH, HCOOH, CH<sub>3</sub>COOH and other alcohols, acids, aldehydes, ketones and esters in CH<sub>4</sub>/CO<sub>2</sub> in the presence of starch. It was shown that the selectivity of C<sub>x</sub>H<sub>y</sub> was much higher than for the oxygenates, which is in good agreement with our results. Kozlov et al.<sup>137</sup>, Zhang et al.<sup>147</sup> and Scarduelli et al.<sup>162</sup> reported the formation of a variety of hydrocarbons and oxygenates in CH<sub>4</sub>/CO<sub>2</sub>. Li et al.<sup>143</sup> found that CH<sub>3</sub>COOH and C<sub>2</sub>H<sub>5</sub>OH were the major oxygenates among other alcohols and acids formed in CH<sub>4</sub>/CO<sub>2</sub>, but of course their selectivities were much lower than those for C<sub>x</sub>H<sub>y</sub> and CO. Sentek et al.<sup>158</sup> discussed the formation of H<sub>2</sub>, CO, C<sub>x</sub>H<sub>y</sub> and alcohols in a CH<sub>4</sub>/CO<sub>2</sub> plasma in the presence of a catalyst. Finally, Goujard et al.<sup>107</sup> studied the effect of helium dilution on the formation of CO, C<sub>x</sub>H<sub>y</sub>, CH<sub>2</sub>O and CH<sub>3</sub>OH in CH<sub>4</sub>/CO<sub>2</sub>.

The flexible adaptation of the H<sub>2</sub>/CO ratio in a DBD by altering the inlet gas mixing ratio is an advantage compared to classical processes, including steam reforming, partial oxidation, and CO<sub>2</sub> reforming, which typically produce syngas with H<sub>2</sub>/CO molar ratio greater than 3, less than 2 and less than 1, respectively.<sup>20-21</sup> The H<sub>2</sub>/CO molar ratio from steam reforming (>3) is much higher than that required by the stoichiometry for many synthesis processes. A low H<sub>2</sub>/CO molar ratio (in the order of 2) is desirable for many industrial

synthesis processes, such as the Fischer Tropsch synthesis or the synthesis of valuable oxygenated chemicals. Methanol can even be produced from syngas with a  $\text{H}_2/\text{CO}$  molar ratio as low as 0.5, when the system can simultaneously carry out methanol synthesis and the water-gas-shift reaction.<sup>20-21</sup>

If the initial fraction of  $\text{O}_2$  increases from 10 to 30%, the densities of  $\text{C}_2\text{H}_6$ ,  $\text{C}_3\text{H}_6$ ,  $\text{C}_3\text{H}_8$ ,  $\text{H}_2$ ,  $\text{H}_2\text{O}_2$ ,  $\text{CH}_2\text{O}$ ,  $\text{CH}_3\text{OH}$  and  $\text{CH}_3\text{OOH}$  decrease up to one order of magnitude, and the densities of  $\text{C}_2\text{H}_5\text{OH}$ ,  $\text{CH}_3\text{CHO}$ ,  $\text{CH}_2\text{CO}$  and  $\text{C}_2\text{H}_5\text{OOH}$  decrease even with several orders of magnitude. Meanwhile, the densities of  $\text{C}_2\text{H}_4$ ,  $\text{C}_2\text{H}_2$ ,  $\text{C}_4\text{H}_2$ ,  $\text{CO}_2$ ,  $\text{CO}$  and  $\text{H}_2\text{O}$  increase up to one order of magnitude and the density of  $\text{O}_3$  increases with several orders of magnitude, pointing towards full oxidation of  $\text{CH}_4$ . In other words, if higher oxygenates, such as  $\text{CH}_2\text{O}$  and  $\text{CH}_3\text{OH}$ , are the desired end products of the gas conversion of  $\text{CH}_4$ , it is appropriate to make use of  $\text{CH}_4/\text{O}_2$  gas mixtures with a not too high fraction of  $\text{O}_2$ . These results are in reasonable agreement with reported research on the effect of the initial gas mixing ratio in similar discharges in  $\text{CH}_4/\text{O}_2$  by Larkin et al.<sup>65-66</sup>, Okumoto et al.<sup>122</sup> and Zhou et al.<sup>106</sup>.

Likewise, increasing the initial fraction of  $\text{CO}_2$  from 5 to 80% results in a drop of the densities of  $\text{C}_x\text{H}_y$ ,  $\text{H}_2$ , and  $\text{CH}_2\text{O}$  up to one order of magnitude, while the densities of  $\text{CO}$ ,  $\text{CH}_3\text{OH}$ ,  $\text{CH}_3\text{CHO}$  and  $\text{CH}_2\text{CO}$  increase up to one order of magnitude and the densities of  $\text{O}_2$ ,  $\text{O}_3$ ,  $\text{H}_2\text{O}$ ,  $\text{H}_2\text{O}_2$ ,  $\text{C}_2\text{H}_5\text{OH}$ ,  $\text{CH}_3\text{OOH}$  and  $\text{C}_2\text{H}_5\text{OOH}$  increase even with several orders of magnitude. In other words, the ideal gas mixing ratio for  $\text{CH}_4/\text{CO}_2$  gas mixtures depends on the desired higher oxygenate to be formed. Since the  $\text{H}_2$  density drops and the  $\text{CO}$  density increases upon rising initial fractions of  $\text{O}_2$  and  $\text{CO}_2$ , the  $\text{H}_2/\text{CO}$  molar ratio will significantly decrease, which is interesting, in view of the desired stoichiometry for industrial synthesis processes (cf. above). These results are

again in reasonable agreement with literature studies on the effect of the initial gas mixing ratio in similar discharges in  $\text{CH}_4/\text{CO}_2$  by Zou et al.<sup>14</sup>, Li et al.<sup>143</sup> and Zhang et al.<sup>147</sup>.

Note that the trends illustrated in Figure 17 correspond to a residence time of 5 seconds; however, the different molecules might have their maximum densities at a different residence time for the different gas mixtures studied, so the trends depicted in Figure 17 are not necessarily the same at other residence times. Besides, the gas composition in the  $\text{CH}_4/\text{O}_2$  gas mixtures completely changes at the moment when  $\text{O}_2$  is fully consumed, which happens after 5.6s and 15.2s, in the case of 10 and 20%  $\text{O}_2$ , respectively (see Figure 19 below). To make this more clear, we show in Figure 18 the characteristic density profiles as a function of the residence time, as we have observed for the different molecules, for a 90/10  $\text{CH}_4/\text{O}_2$  (a) and a 90/10  $\text{CH}_4/\text{CO}_2$  (b) gas mixture.

In the mixture with  $\text{O}_2$  we can distinguish six different density profiles:

1.  $\text{H}_2$  and CO show a continuously rising trend.
2. The higher hydrocarbons ( $\text{C}_x\text{H}_y$ ), ethanol ( $\text{C}_2\text{H}_5\text{OH}$ ) and ketene ( $\text{CH}_2\text{CO}$ ) have negligible values up to 5.6s, followed by a strong increase up to an equilibrium value after 10s.
3.  $\text{O}_3$  exhibits a maximum within 1s, and then reacts away within 3 s.
4.  $\text{CO}_2$ ,  $\text{H}_2\text{O}$  and methanol ( $\text{CH}_3\text{OH}$ ) show a steady increase to a maximum at around 6-8s, followed by a very slow decrease.
5. Hydrogen peroxide ( $\text{H}_2\text{O}_2$ ), methyl hydroperoxide ( $\text{CH}_3\text{OOH}$ ) and ethyl hydroperoxide ( $\text{C}_2\text{H}_5\text{OOH}$ ) go over a maximum at 4-6s and then decrease rapidly.

6. Finally, formaldehyde ( $\text{CH}_2\text{O}$ ) and acetaldehyde ( $\text{CH}_3\text{CHO}$ ) also reach a maximum at 4-6s, but after a fast drop, their density increases again after 8s.

Except for the profile of  $\text{O}_3$  (no. 3), which has already reacted away after 4s, the effect of  $\text{O}_2$  being fully consumed after 5.6s can be observed in the changes of the density profiles of all different molecules at this moment of time. Indeed, the densities of the higher hydrocarbons, for instance, start rising at that time, because in the absence of  $\text{O}_2$ , the  $\text{CH}_4$  will mainly be converted into higher hydrocarbons, while the densities of the oxygenates typically show a (sharp) drop in time, when  $\text{O}_2$  is fully depleted.

In the mixture with  $\text{CO}_2$  four different density profiles can be distinguished:

1.  $\text{H}_2$ ,  $\text{CO}$ , ethane ( $\text{C}_2\text{H}_6$ ) and methanol ( $\text{CH}_3\text{OH}$ ) exhibit a steady rise as a function of time.
2. Ethylene ( $\text{C}_2\text{H}_4$ ), acetylene ( $\text{C}_2\text{H}_2$ ),  $\text{C}_4\text{H}_2$ ,  $\text{H}_2\text{O}$ , formaldehyde ( $\text{CH}_2\text{O}$ ), acetaldehyde ( $\text{CH}_3\text{CHO}$ ) and ketene ( $\text{CH}_2\text{CO}$ ) go over a maximum at around 6-8s.
3. Propane ( $\text{C}_3\text{H}_8$ ), propene ( $\text{C}_3\text{H}_6$ ) and ethanol ( $\text{C}_2\text{H}_5\text{OH}$ ) rise rapidly, but reach an equilibrium density after 2s.
4.  $\text{O}_2$ ,  $\text{O}_3$ , hydrogen peroxide ( $\text{H}_2\text{O}_2$ ), methyl hydroperoxide ( $\text{CH}_3\text{OOH}$ ) and ethyl hydroperoxide ( $\text{C}_2\text{H}_5\text{OOH}$ ) reach a maximum within 5 ms, and then react rapidly away.

Thus it is clear that the higher hydrocarbons and oxygenates (no. 2 and no. 3) can be formed at rather high density, but they react away again after a longer residence time towards  $\text{H}_2$  and  $\text{CO}$ , respectively, which explains why  $\text{H}_2$  and  $\text{CO}$  show a continuously rising trend. Besides  $\text{H}_2$  and  $\text{CO}$ , also  $\text{C}_2\text{H}_6$  and  $\text{CH}_3\text{OH}$  exhibit a steady rise (no. 1) as their formation is strongly connected to

the dissociation products of  $\text{CH}_4$ , in particular the  $\text{CH}_3$  and  $\text{CH}_2$  radicals. Finally,  $\text{O}_2$ ,  $\text{O}_3$  and the different peroxides are only present at very low densities, and for a very short time, as they are formed as an intermediate in the direct or indirect formation of  $\text{CO}$ .

An identical behavior is observed for all these species in the other gas mixing ratios of  $\text{CH}_4$  with  $\text{O}_2$  and  $\text{CO}_2$ .

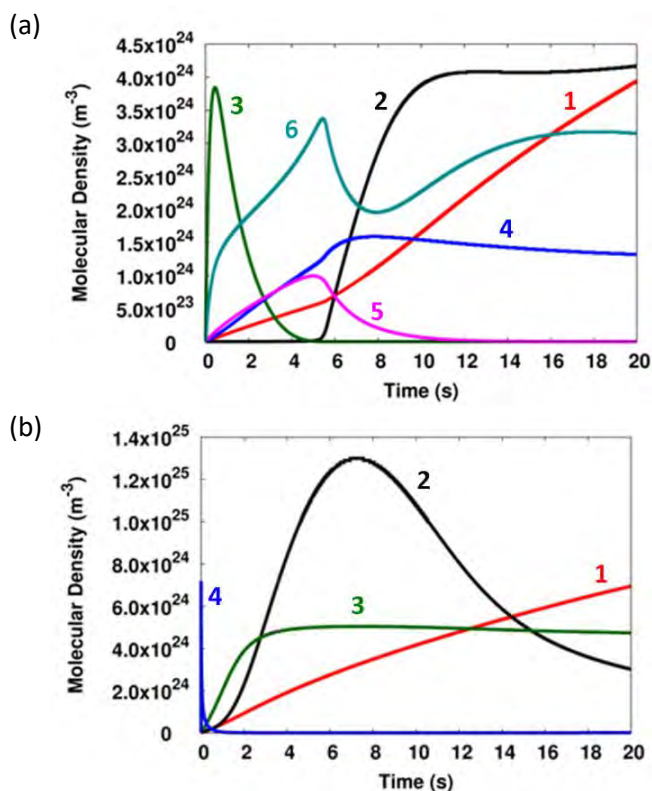


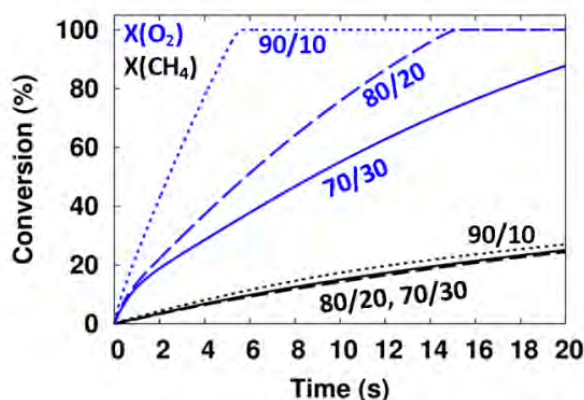
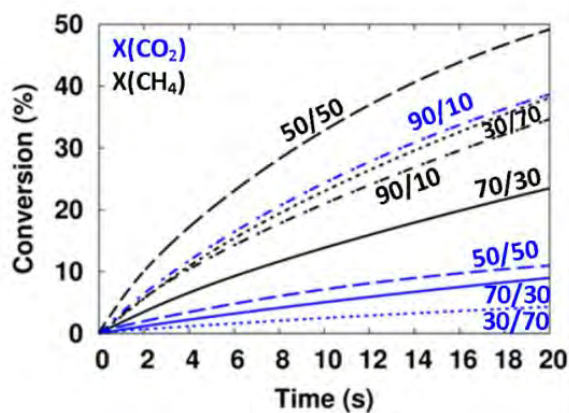
Figure 18. Spatially averaged molecule densities as a function of the residence time, for the 90/10  $\text{CH}_4/\text{O}_2$  gas mixture (a) and the 90/10  $\text{CH}_4/\text{CO}_2$  gas mixture (b). The labels of the curves characterize some specific molecules (see text). For panel (a): 1 =  $\text{H}_2$  (density divided by 10), 2 =  $\text{C}_2\text{H}_6$ , 3 =  $\text{O}_3$  (density multiplied by 10), 4 =  $\text{CO}_2$ , 5 =  $\text{H}_2\text{O}_2$ , 6 =  $\text{CH}_2\text{O}$  (density multiplied by 5). For panel (b): 1 =  $\text{H}_2$ , 2 =  $\text{C}_2\text{H}_4$  (density multiplied by 1000), 3 =  $\text{C}_3\text{H}_8$  (density multiplied by 100), 4 =  $\text{O}_2$  (density multiplied by  $10^{10}$ ).

### 5.5.2. Conversion, Yields and Selectivities

Figure 19 shows the conversion of  $\text{CH}_4$  and  $\text{O}_2$  (a) and of  $\text{CH}_4$  and  $\text{CO}_2$  (b) as a function of residence time for different gas mixing ratios. The conversion of  $\text{CH}_4$  after 20s is around 20% in all considered mixtures with  $\text{O}_2$ , while in pure  $\text{CH}_4$ , a conversion of 40% was calculated after 20s (see Section 4.5.2.). This is logical, because in the  $\text{CH}_4/\text{O}_2$  mixture a considerable fraction of the energy is also consumed by  $\text{O}_2$ .  $\text{O}_2$  is indeed converted very quickly, and the time for full conversion depends on the initial fraction of  $\text{O}_2$ , i.e., full conversion is reached faster in the case of a lower  $\text{O}_2$  initial fraction (see Figure 19(a)), which is logical.

In the  $\text{CH}_4/\text{CO}_2$  gas mixture, the conversion of both  $\text{CH}_4$  and  $\text{CO}_2$  strongly depends on the initial gas mixing ratio. No clear trend can be observed from Figure 19(b), because the initial gas mixing ratio strongly affects the discharge characteristics and therefore the conversion of the inlet gases. The effect of the initial gas mixing ratio on the conversion will be discussed below. Our calculations predict a maximum conversion of 68% for  $\text{CH}_4$  and 55% for  $\text{CO}_2$  after a residence time of 20s in a 20/80 and a 95/5  $\text{CH}_4/\text{CO}_2$  gas mixture, respectively (not shown in Figure 19(b)). It is logical that a higher  $\text{CH}_4$  conversion is reached at a lower initial  $\text{CH}_4$  fraction in the gas mixture, and vice versa for  $\text{CO}_2$ , because these conditions yield a higher co-reactant concentration, which contributes to a more efficient conversion.



(a)  $\text{CH}_4/\text{O}_2$ (b)  $\text{CH}_4/\text{CO}_2$ 

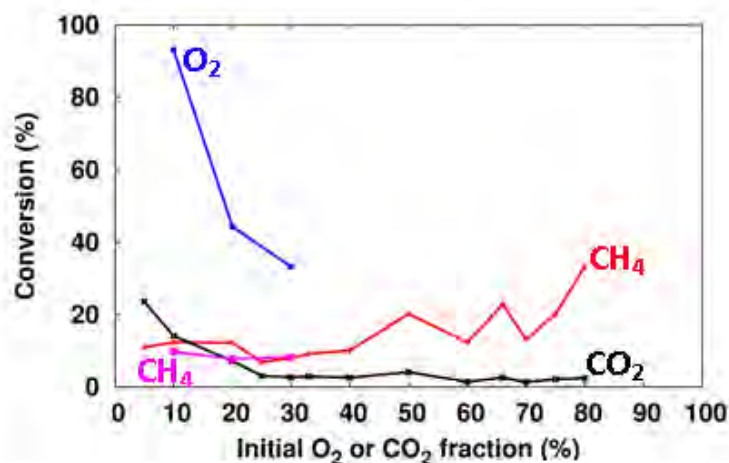
**Figure 19.** Conversion of  $\text{CH}_4$  (black) and  $\text{O}_2$  (a, blue) or  $\text{CO}_2$  (b, blue) as a function of residence time.

When comparing the conversion of  $\text{CH}_4$  in both the  $\text{CH}_4/\text{O}_2$  and the  $\text{CH}_4/\text{CO}_2$  gas mixtures with the same gas mixing ratios, it is clear that at a 70/30 gas mixing ratio, the  $\text{CH}_4$  conversion is equal (i.e., around 20%) in both gas mixtures, while at the 80/20 and 90/10 gas mixing ratios, the  $\text{CH}_4$  conversion was found to be slightly higher in the mixtures with  $\text{CO}_2$  than in the mixtures with  $\text{O}_2$ . This can be explained because the loss (by electron impact dissociation and ionization) of  $\text{CH}_4$  is about a factor 2 higher in  $\text{CH}_4/\text{CO}_2$  than in  $\text{CH}_4/\text{O}_2$  due to the fact that much more electrons are consumed by electron impact reactions with  $\text{O}_2$  than with  $\text{CO}_2$  (cf. the electronegative character,

explained in Section 5.5.1. above). However, the lower consumption of  $\text{CH}_4$  in the  $\text{CH}_4/\text{O}_2$  gas mixture is partially compensated by the increasing importance of the reaction with OH when the initial fraction of  $\text{O}_2$  in the gas mixture increases. Furthermore, in the  $\text{CH}_4/\text{CO}_2$  gas mixture, the production (or regeneration) of  $\text{CH}_4$  is around 50% of the  $\text{CH}_4$  consumption when the initial fraction of  $\text{CO}_2$  is in the range of 10-30%, while in the  $\text{CH}_4/\text{O}_2$  mixture, the  $\text{CH}_4$  production is decreasing with increasing  $\text{O}_2$  initial fraction, from 30% of the  $\text{CH}_4$  consumption in 90/10  $\text{CH}_4/\text{O}_2$  to 8% in 70/30  $\text{CH}_4/\text{O}_2$  (i.e. one order of magnitude lower than in 70/30  $\text{CH}_4/\text{CO}_2$ ). In other words, the much lower regeneration of  $\text{CH}_4$  in the 70/30  $\text{CH}_4/\text{O}_2$  mixture than in the 70/30  $\text{CH}_4/\text{CO}_2$  mixture compensates enough for the lower consumption of  $\text{CH}_4$  in the 70/30  $\text{CH}_4/\text{O}_2$  mixture than in the 70/30  $\text{CH}_4/\text{CO}_2$  mixture. This effect, together with the increasing importance of the reaction with OH radicals, results in an almost equal net conversion of  $\text{CH}_4$  in both gas mixtures at a 70/30 gas mixing ratio (see more details in Section 5.5.3. and Figure 21 below).

Figure 20 shows the conversion of  $\text{CH}_4$ ,  $\text{O}_2$  and  $\text{CO}_2$  as a function of the initial gas mixing ratio, for both the  $\text{CH}_4/\text{O}_2$  and  $\text{CH}_4/\text{CO}_2$  gas mixtures, after a residence time of 5s. The  $\text{CH}_4$  conversion is roughly independent from the initial  $\text{O}_2$  or  $\text{CO}_2$  fraction up to 30-40%, with a value of about 10%, but it increases for higher initial  $\text{CO}_2$  fractions, especially above 70%. Indeed, at higher initial  $\text{CO}_2$  fractions, the conversion of  $\text{CH}_4$  rises due to the increasing importance of the reaction of  $\text{CH}_4$  with  $\text{CO}_2^+$ , which becomes the most important channel for consumption of  $\text{CH}_4$ , while at lower initial  $\text{CO}_2$  fractions electron impact dissociation of  $\text{CH}_4$  is the most important loss channel (see also Section 5.5.3. and Figure 21 below). For the same reason, the conversion of  $\text{O}_2$  and  $\text{CO}_2$  increases with decreasing initial  $\text{O}_2$  or  $\text{CO}_2$  fraction, because of

the additional loss reactions with  $\text{CH}_4$  molecules (or  $\text{CH}_4$ -derived species). For instance, in the 70/30  $\text{CH}_4/\text{O}_2$  mixture, a three-body reaction with O radicals is the most important loss process for  $\text{O}_2$ , while in the 90/10  $\text{CH}_4/\text{O}_2$  mixture, the most important loss processes for  $\text{O}_2$  are three-body reactions with  $\text{CH}_3$  or H radicals (see also Section 5.5.3. and Figure 22 below). Likewise, in the  $\text{CH}_4/\text{CO}_2$  mixtures with high initial  $\text{CO}_2$  fractions, electron impact ionization of  $\text{CO}_2$  is the most important loss channel, while at lower initial  $\text{CO}_2$  fractions, the reaction of  $\text{CO}_2$  with  $\text{CH}_2$  radicals is the most important loss channel for  $\text{CO}_2$  (see again Section 5.5.3. and Figure 22 below).



**Figure 20.** Conversion of  $\text{CH}_4$ ,  $\text{O}_2$  and  $\text{CO}_2$  as a function of the initial  $\text{O}_2$  or  $\text{CO}_2$  fraction in the gas mixture, for a residence time of 5 seconds. The  $\text{CH}_4$  conversion in the  $\text{CH}_4/\text{CO}_2$  mixture is depicted in red, while the  $\text{CH}_4$  conversion in the  $\text{CH}_4/\text{O}_2$  mixture is presented in pink.

As was also clear from Figure 19, the  $\text{O}_2$  conversion is much higher than the  $\text{CO}_2$  conversion, which is only in the order of 20% at low  $\text{CO}_2$  fractions, and even below 3% at higher  $\text{CO}_2$  fractions. This is because the threshold energies for electron impact ionization and dissociation are much lower for  $\text{O}_2$  than for

$\text{CO}_2$ . The  $\text{CH}_4$  conversion is comparable to the  $\text{CO}_2$  conversion at low  $\text{CO}_2$  fractions, i.e., around 10%, but it rises to 35% at high  $\text{CO}_2$  fractions. Finally, it is worth to mention that Figure 20 illustrates the conversion, relative to the amount of  $\text{CH}_4$ ,  $\text{CO}_2$  or  $\text{O}_2$  present in the mixture. The absolute (or effective) conversion of  $\text{CH}_4$  is of course higher at a higher initial  $\text{CH}_4$  fraction, and vice versa for the absolute  $\text{CO}_2$  and  $\text{O}_2$  conversions, which is logical, as there is more of these gases initially present in the gas mixture.

Besides the conversion of  $\text{CH}_4$ ,  $\text{CO}_2$  and  $\text{O}_2$ , we are especially interested in the yields and selectivities of the formed value-added chemicals. Table 6 shows the maximum yields of  $\text{H}_2$ ,  $\text{CO}$ , formaldehyde ( $\text{CH}_2\text{O}$ ) and methanol ( $\text{CH}_3\text{OH}$ ), as well as the gas mixtures and residence times for which these maximum values were obtained. Also the corresponding selectivities are presented. Note that the sum of the selectivities does not have to be equal to 100%, because in the  $\text{CH}_4/\text{CO}_2$  mixture, the selectivities of  $\text{CO}$ ,  $\text{CH}_2\text{O}$  and  $\text{CH}_3\text{OH}$  are calculated with respect to both the  $\text{CH}_4$  and  $\text{CO}_2$  conversion, while the  $\text{H}_2$  selectivity is only calculated with respect to the  $\text{CH}_4$  conversion. Similarly in the case of the  $\text{CH}_4/\text{O}_2$  mixture, the selectivities of  $\text{CO}$ ,  $\text{CH}_2\text{O}$  and  $\text{CH}_3\text{OH}$  are calculated with respect to the  $\text{CH}_4$  conversion, while the  $\text{H}_2$  selectivity is calculated with respect to twice the  $\text{CH}_4$  conversion, resulting in a difference of a factor 2 (see Section 3.6.).

**Table 6. Overview of the maximum yields for some important end products in both the  $\text{CH}_4/\text{O}_2$  and  $\text{CH}_4/\text{CO}_2$  gas mixtures, as well as the corresponding gas mixing ratio and residence time at which these maximum yields are obtained. The corresponding selectivities of these end products are also listed.**

		$\text{H}_2$	CO	$\text{CH}_2\text{O}$	$\text{CH}_3\text{OH}$
$\text{CH}_4/\text{O}_2$	Yield (%)	9	10	0.3	4
	Mixture	90/10	70/30	90/10 and 80/20	80/20
	Residence Time (s)	20	20	5.4 and 14.9	20
	Selectivity (%)	33	39	3 and 2	15
$\text{CH}_4/\text{CO}_2$	Yield (%)	34	10	0.9	0.4
	Mixture	20/80	20/80	90/10	25/75
	Residence Time (s)	20	20	10.3	20
	Selectivity (%)	50	52	4	2

It is clear that syngas is the main product in both gas mixtures, but the  $\text{H}_2/\text{CO}$  molar ratio is somewhat different, as was also discussed in Section 5.5.1. above. In the  $\text{CH}_4/\text{O}_2$  mixture, the  $\text{H}_2$  yield reaches a maximum at 10%  $\text{O}_2$  fraction, while the CO yield reaches a maximum at 30%  $\text{O}_2$  fraction, which is logical. In the  $\text{CH}_4/\text{CO}_2$  mixture, the maximum  $\text{H}_2$  and CO yields are both reached at 80%  $\text{CO}_2$ . For  $\text{H}_2$ , this can be explained because, although the absolute formation of  $\text{H}_2$  is of course lower at a higher initial  $\text{CO}_2$  fraction, its yield becomes higher as the latter is calculated with respect to the initial  $\text{CH}_4$  density, which is obviously lower at higher initial  $\text{CO}_2$  fraction. For CO, electron impact dissociation of  $\text{CO}_2$  is the most important production channel, and the highest density and yield of CO are found at the highest initial  $\text{CO}_2$  fraction. Note that at lower initial  $\text{CO}_2$  fractions, the most important production channel of CO is the reaction of  $\text{CH}_2$  radicals with  $\text{CO}_2$ , but this

reaction does not lead to a higher CO density (see also Section 5.5.3. and Figure 24 below). The  $\text{H}_2/\text{CO}$  molar ratio in the case of the 20/80  $\text{CH}_4/\text{CO}_2$  gas mixture is around 1.5, which is desirable for many industrial synthesis processes (cf. above). At higher  $\text{CH}_4/\text{CO}_2$  gas mixing ratios, the  $\text{H}_2/\text{CO}$  molar ratio rises to about 5, because the  $\text{H}_2$  density increases, while the CO density decreases upon higher  $\text{CH}_4$  fraction in the mixture.

The maximum yields of  $\text{CH}_2\text{O}$  and  $\text{CH}_3\text{OH}$  are clearly lower than the maximum  $\text{H}_2$  and CO yields. This is especially true in the  $\text{CH}_4/\text{CO}_2$  mixtures, where both yields are below 1%. In this case, the highest  $\text{CH}_2\text{O}$  yield is obtained at 90%  $\text{CH}_4$  fraction, while the highest  $\text{CH}_3\text{OH}$  yield is reached at 25%  $\text{CH}_4$ . In the  $\text{CH}_4/\text{O}_2$  mixtures, the highest  $\text{CH}_2\text{O}$  yield is also below 1%, but the maximum  $\text{CH}_3\text{OH}$  yield reaches a value of 4%, which is not negligible. Nevertheless, a really selective production process towards  $\text{CH}_2\text{O}$  or  $\text{CH}_3\text{OH}$  seems not feasible in a DBD plasma, at least not at the conditions under study. For this purpose, a catalyst will need to be integrated into the plasma region.

Finally, it is clear from Table 6 that the highest yields are not necessarily reached at the longest residence time. Indeed, the  $\text{H}_2$ , CO and  $\text{CH}_3\text{OH}$  yields reach their maximum at 20s residence time, pointing out that their densities are still rising as a function of time (cf. Figure 18 above), while the  $\text{CH}_2\text{O}$  yield clearly reaches its maximum at a shorter residence time (see also Figure 18 above), and the exact value depends on the gas mixture and gas mixing ratio, as appears from Table 6. This indicates that, when the production of formaldehyde is targeted, the optimal residence time should be carefully selected.

Indeed, similar results were reported in literature. Okumoto et al.<sup>122</sup> stated that  $\text{CH}_3\text{OH}$  and  $\text{CH}_2\text{O}$  are in fact intermediate products in the oxidation of  $\text{CH}_4$  and are easily decomposed or converted to  $\text{CO}$ ,  $\text{CO}_2$  and  $\text{H}_2\text{O}$ . In other words, the formation of oxygenates is strongly dependent on the initial gas mixing ratio, the residence time and a variety of other parameters. Okumoto et al. found that 15 vol.% of  $\text{O}_2$  showed optimum performance for the formation of  $\text{CH}_3\text{OH}$  and  $\text{CH}_2\text{O}$  in  $\text{CH}_4/\text{O}_2$ .<sup>122</sup> Note that the authors made use of dilution gases to enhance the formation of oxygenates. Also Zou et al.<sup>14</sup> discussed the existence of an optimum feed composition to attain the maximum selectivity of the desired oxygenates. They obtained the highest total selectivity of oxygenates at a  $\text{CH}_4$  concentration of 35 vol.% in  $\text{CH}_4/\text{CO}_2$  in the presence of starch with the highest selectivities of alcohols, such as  $\text{CH}_3\text{OH}$ , and acids when the  $\text{CO}_2$  fraction in the feed increases to 74 vol.%, and the highest selectivity of  $\text{CH}_2\text{O}$  at a higher  $\text{CH}_4$  concentration of about 50 vol.%. These findings are in reasonable agreement with our results.

### 5.5.3. Dominant Reaction Pathways

We will now discuss the dominant reaction pathways for the conversion of the inlet gases into syngas, higher order hydrocarbons and oxygenates for a 70/30  $\text{CH}_4/\text{CO}_2$  gas mixture and for a 70/30  $\text{CH}_4/\text{O}_2$  gas mixture.

#### **(a) Electron impact dissociation of $\text{CH}_4$ , $\text{CO}_2$ and $\text{O}_2$ : initiating the conversion process**

As soon as the discharge is ignited, electron impact ionization and dissociation of the inlet gases occurs, resulting in the creation of new species (electrons, ions, radicals), as discussed in Section 5.5.1. above. The formation of new electrons and ions in the plasma enables to sustain the discharge, while the formation of radicals is important for the production of syngas, higher order hydrocarbons and oxygenates.

The dominant reactions for  $\text{CH}_4$  consumption (and production) for a 70/30  $\text{CH}_4/\text{CO}_2$  gas mixture and a 70/30  $\text{CH}_4/\text{O}_2$  gas mixture are depicted in Figure 21(a) and Figure 21(b), respectively. Electron impact dissociation, yielding the formation of  $\text{CH}_3$ ,  $\text{CH}_2$  or  $\text{CH}$  radicals, are important channels for  $\text{CH}_4$  consumption in both gas mixtures, with relative contributions of about 33%, 6% and 2% in  $\text{CH}_4/\text{CO}_2$  and 34%, 7% and 2% in  $\text{CH}_4/\text{O}_2$ . In the 70/30  $\text{CH}_4/\text{O}_2$  gas mixture, the reaction with OH radicals, forming  $\text{CH}_3$  radicals and  $\text{H}_2\text{O}$ , also contributes for about 19% to the loss of  $\text{CH}_4$ . This reaction is negligible in the  $\text{CH}_4/\text{CO}_2$  mixture, due to the much lower OH radical density in that case (see Figure 15 above). Furthermore, also electron impact ionization and reactions with ions or radicals contribute to the loss of  $\text{CH}_4$ , accounting in total for about 20%, 31% and 6%, respectively, in  $\text{CH}_4/\text{CO}_2$  and for about 15%, 21% and 22% (including the 19% of the reaction with OH), respectively, in  $\text{CH}_4/\text{O}_2$ .



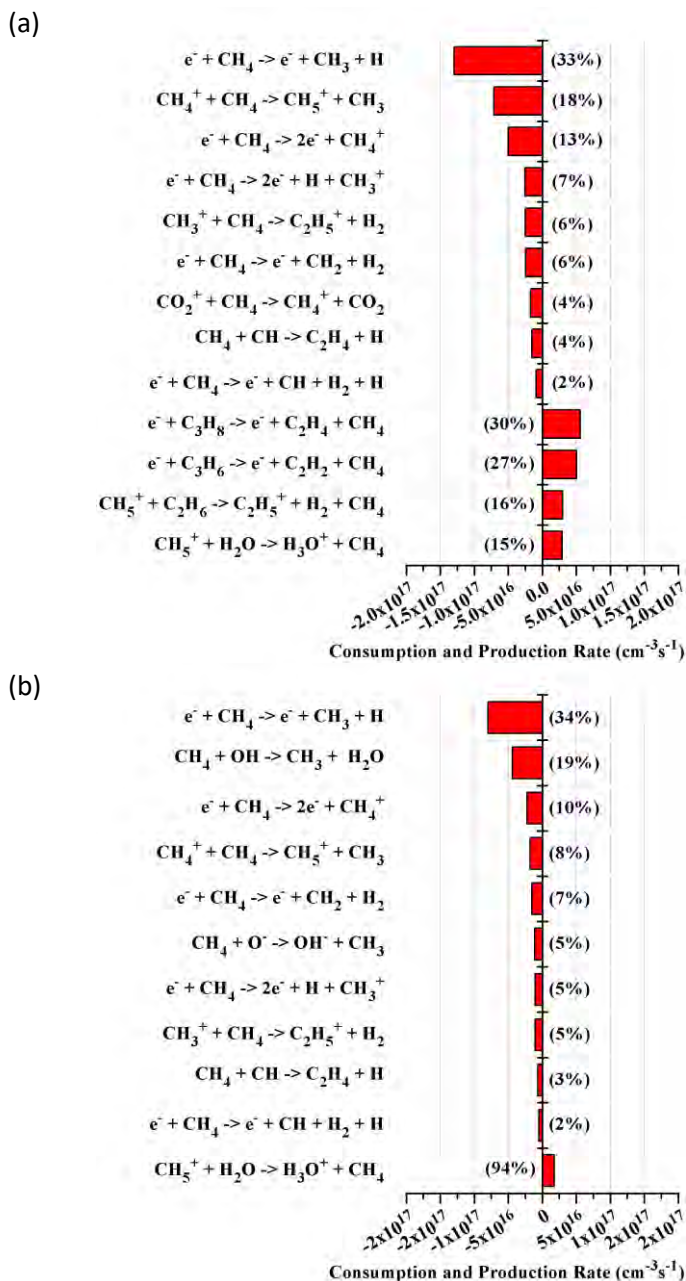


Figure 21. Time-averaged reaction rates of the dominant reaction pathways for the consumption and production of CH<sub>4</sub>, for a 70/30 CH<sub>4</sub>/CO<sub>2</sub> gas mixture (a) and a 70/30 CH<sub>4</sub>/O<sub>2</sub> gas mixture (b). The consumption rates are defined as negative values (i.e., left-hand side of the figures), while the production rates are plotted as positive values (i.e., right-hand side of the figures). The relative contributions of these consumption and production processes to the overall consumption and production of CH<sub>4</sub> are also indicated.

It should be noted that electron impact vibrational excitation of CH<sub>4</sub> is also important, but this process is only considered in our model as an energy loss for the electrons, and not as a chemical loss process for CH<sub>4</sub>, because the vibrationally excited species are not taken into account separately in our model (see Section 5.2.).

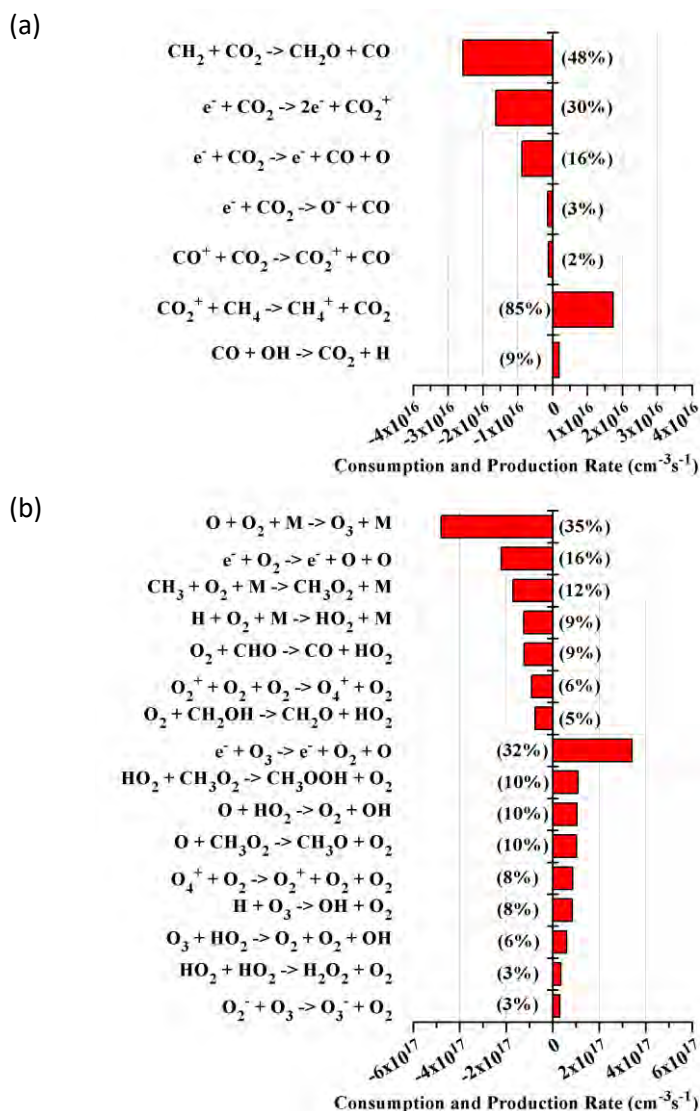
The most important pathways for the production (or regeneration) of CH<sub>4</sub> in the mixture with CO<sub>2</sub> are based on electron impact dissociation of higher hydrocarbons, such as C<sub>3</sub>H<sub>8</sub> and C<sub>3</sub>H<sub>6</sub>, while in the mixture with O<sub>2</sub> these reactions appear negligible, and a charge transfer process of CH<sub>5</sub><sup>+</sup> with H<sub>2</sub>O is the most important production process.

Finally, it is clear from Figure 21 that the total production (or regeneration) rate of CH<sub>4</sub> in the 70/30 CH<sub>4</sub>/CO<sub>2</sub> gas mixture is almost one order of magnitude higher than in the 70/30 CH<sub>4</sub>/O<sub>2</sub> gas mixture, while the consumption rate in both gas mixtures is in the same order of magnitude. However, the total loss rate is still a factor 2 higher than the total production rate in the CH<sub>4</sub>/CO<sub>2</sub> mixture, and even a factor 12 higher in the CH<sub>4</sub>/O<sub>2</sub> mixture, resulting in a clear loss of CH<sub>4</sub>.

At a higher initial CO<sub>2</sub> fraction, the reactions of CH<sub>4</sub> with CO<sub>2</sub><sup>+</sup> and CH<sub>4</sub><sup>+</sup> become the most important channels for the consumption of CH<sub>4</sub> (see also Section 5.5.2.), accounting both for about 29% in 20/80 CH<sub>4</sub>/CO<sub>2</sub>, while the electron impact dissociation reaction yielding the formation of CH<sub>3</sub> only contributes for about 15% at these conditions. The most important pathway for the production (or regeneration) of CH<sub>4</sub> then becomes the charge transfer process of CH<sub>5</sub><sup>+</sup> with H<sub>2</sub>O, with a contribution of 32%. A decrease of the initial fraction of CO<sub>2</sub> results in an increase of the contributions of the electron impact dissociation reactions for the consumption of CH<sub>4</sub> and also an increase

of the contributions of the electron impact dissociations of  $\text{C}_3\text{H}_8$  and  $\text{C}_3\text{H}_6$  for the regeneration of  $\text{CH}_4$ . A decrease of the initial fraction of  $\text{O}_2$  to 10% results in a drastic decrease of the contribution of the reaction with OH radicals (3%). Electron impact dissociation yielding the formation of  $\text{CH}_3$  remains the most important loss channel in this case, with a contribution of 42%. Meanwhile, the contribution of the charge transfer process of  $\text{CH}_5^+$  with  $\text{H}_2\text{O}$ , the most important production process of  $\text{CH}_4$ , decreases from 94% in 70/30  $\text{CH}_4/\text{O}_2$  to 38% in 90/10  $\text{CH}_4/\text{O}_2$ , as electron impact dissociation of  $\text{C}_3\text{H}_8$  and  $\text{C}_3\text{H}_6$  becomes more important, like in the mixtures with  $\text{CO}_2$ .

The dominant reactions for  $\text{CO}_2$  consumption (and production) for a 70/30  $\text{CH}_4/\text{CO}_2$  gas mixture and for  $\text{O}_2$  consumption (and production) for a 70/30  $\text{CH}_4/\text{O}_2$  gas mixture are depicted in Figure 22(a) and Figure 22(b), respectively. The most important channel for consumption of  $\text{CO}_2$  at this gas mixing ratio is the reaction with  $\text{CH}_2$  radicals, contributing for about 48% to the  $\text{CO}_2$  loss, followed by electron impact dissociation and ionization, which contribute for 16% and 30% to the total consumption of  $\text{CO}_2$ , respectively. At lower  $\text{CO}_2$  fractions, the contribution of the first process will even increase to 77% for a 90/10  $\text{CH}_4/\text{CO}_2$  gas mixture. On the other hand, at higher  $\text{CO}_2$  fractions in the gas mixture, the latter two processes will become gradually more important. For a 20/80  $\text{CH}_4/\text{CO}_2$  gas mixture, electron impact ionization and dissociation contribute for 52% and 27%, respectively, while the reaction with  $\text{CH}_2$  radicals contributes for 9%. It is worth to mention that the reaction with  $\text{CH}_2$  radicals is also the most important pathway for the production of  $\text{CH}_2\text{O}$  and CO in the 70/30  $\text{CH}_4/\text{CO}_2$  gas mixture (see below).



**Figure 22.** Time-averaged reaction rates of the dominant reaction pathways for the consumption and production of  $\text{CO}_2$  for a 70/30  $\text{CH}_4/\text{CO}_2$  gas mixture (a) and for the consumption and production of  $\text{O}_2$  for a 70/30  $\text{CH}_4/\text{O}_2$  gas mixture (b).

The most important channels for consumption of  $\text{O}_2$  are three-body collisions with O,  $\text{CH}_3$  or H radicals, with either  $\text{CH}_4$ ,  $\text{O}_2$ ,  $\text{H}_2\text{O}$  or  $\text{CO}_2$  as third body (denoted as M in Figure 22(b)), as well as electron impact dissociation of  $\text{O}_2$  and a chemical reaction with CHO radicals. The three-body reaction with O

radicals, forming  $\text{O}_3$ , is the most important loss process, with a contribution of 36%. However, almost all the  $\text{O}_3$  will be decomposed back to  $\text{O}_2$  by electron impact dissociation, so that the net contribution of this reaction will be lower.

Electron impact dissociation of  $\text{O}_2$  yields the formation of O radicals, while the reactions with  $\text{CH}_3$ , H and CHO yield among others the formation of  $\text{CH}_3\text{O}_2$  and  $\text{HO}_2$ . The O and  $\text{HO}_2$  radicals will react further into OH (see below), which is an important species for the consumption of  $\text{CH}_4$  (see above), while  $\text{CH}_3\text{O}_2$  plays an important role in the formation of  $\text{CH}_3\text{OH}$  and  $\text{CH}_3\text{OOH}$  (see below). When the initial fraction of  $\text{O}_2$  decreases to 10%, the three-body collisions with  $\text{CH}_3$  and H radicals become more important for the consumption of  $\text{O}_2$ , with contributions of 29% and 25%, respectively. Meanwhile, the contribution of electron impact dissociation of  $\text{O}_2$  decreases to 11% and the three-body collision with O radicals decreases drastically to 10%.

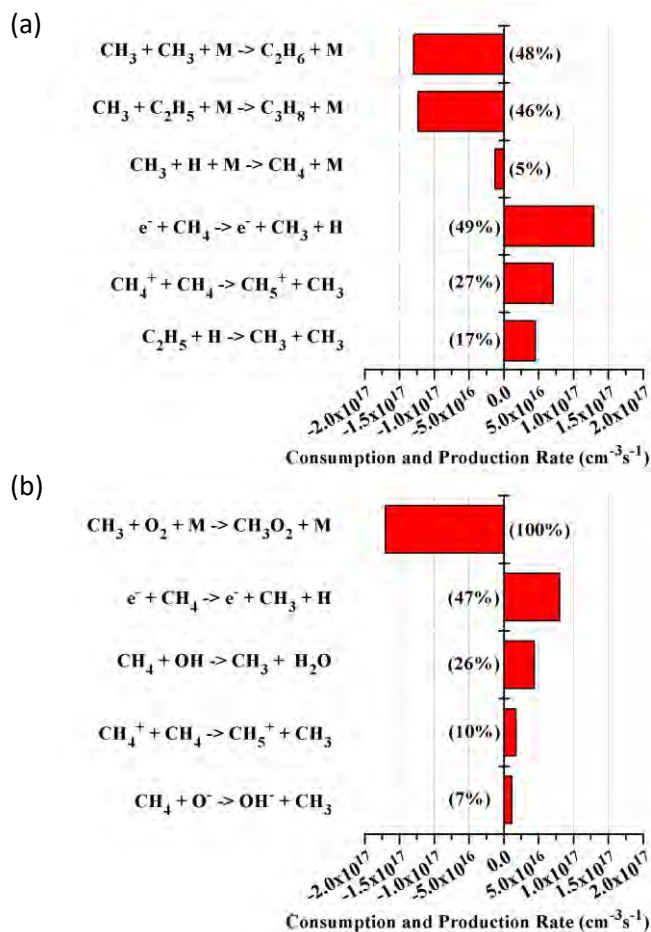
The most important production mechanism for  $\text{CO}_2$  in the  $\text{CH}_4/\text{CO}_2$  gas mixtures is a charge transfer process between  $\text{CO}_2^+$  and  $\text{CH}_4$ , while electron impact dissociation of  $\text{O}_3$  (see above) is the most important production process for  $\text{O}_2$  in a 70/30  $\text{CH}_4/\text{O}_2$  gas mixture. As a result of the lower production of  $\text{O}_3$  (see above) in a 90/10  $\text{CH}_4/\text{O}_2$  gas mixture, the reaction of  $\text{HO}_2$  radicals with  $\text{CH}_3\text{O}_2$  radicals towards  $\text{CH}_3\text{OOH}$  is the most important process for regeneration of  $\text{O}_2$  in this mixture, with a contribution of 33%. However, the rates for regeneration of  $\text{CO}_2$  and  $\text{O}_2$  are again a factor 2.6 and 1.3 lower than their corresponding loss rates, so that there is a net consumption of  $\text{CO}_2$  and  $\text{O}_2$ .

**(b) Recombination of  $\text{CH}_3$  radicals: the formation of  $\text{C}_x\text{H}_y$  vs. the formation of  $\text{CH}_3\text{O}_2$** 

The most important species produced from  $\text{CH}_4$  are the  $\text{CH}_3$  radicals (see above). Figure 23(a) and Figure 23(b) show the dominant reactions for  $\text{CH}_3$  consumption and production, again for a 70/30  $\text{CH}_4/\text{CO}_2$  gas mixture and a 70/30  $\text{CH}_4/\text{O}_2$  gas mixture, respectively. In the 70/30  $\text{CH}_4/\text{CO}_2$  mixture, the  $\text{CH}_3$  radicals will mainly recombine towards higher hydrocarbons, such as  $\text{C}_2\text{H}_6$  and  $\text{C}_3\text{H}_8$ , which contribute for 48% and 46% to the consumption of  $\text{CH}_3$ , respectively. On the other hand, in the 70/30  $\text{CH}_4/\text{O}_2$  gas mixture, these reactions are negligible compared to the three-body recombination reaction with  $\text{O}_2$  molecules, forming  $\text{CH}_3\text{O}_2$  radicals (see Figure 23(b)). This is in good agreement with Nozaki et al.<sup>134</sup> and Goujard et al.<sup>105</sup>, who also discussed the importance of the formation of  $\text{CH}_3\text{O}_2$  in the methane partial oxidation mechanism towards the formation of  $\text{CH}_3\text{OH}$ . Furthermore, this result explains the lower densities for the higher hydrocarbons in the gas mixtures with  $\text{O}_2$  as co-reactant (see Figure 17 (a, b) above). The formation and loss mechanisms of the higher hydrocarbon molecules in both gas mixtures are similar to the case of pure  $\text{CH}_4$  (see Section 4.5.3.), and will therefore not be discussed here.

At higher initial fraction of  $\text{CO}_2$ , the recombination of  $\text{CH}_3$  towards  $\text{C}_2\text{H}_6$ ,  $\text{C}_3\text{H}_8$  and  $\text{CH}_4$  will contribute for 57%, 22% and 19% to the consumption of  $\text{CH}_3$ , respectively. On the other hand, at a lower initial fraction of  $\text{CO}_2$ , the recombination towards  $\text{C}_3\text{H}_8$  will become more important than the recombination to  $\text{C}_2\text{H}_6$ . In a 90/10  $\text{CH}_4/\text{O}_2$  gas mixture, thus a lower  $\text{O}_2$  content, the recombination towards  $\text{C}_2\text{H}_6$  and  $\text{C}_3\text{H}_8$  becomes more important, with contributions of 38% and 30%, respectively, while the three-body

recombination with  $\text{O}_2$  molecules, forming  $\text{CH}_3\text{O}_2$  radicals, contributes for 29% to the consumption of  $\text{CH}_3$ .



**Figure 23.** Time-averaged reaction rates of the dominant reaction pathways for the consumption and production of  $\text{CH}_3$ , for a 70/30  $\text{CH}_4/\text{CO}_2$  gas mixture (a) and for a 70/30  $\text{CH}_4/\text{O}_2$  gas mixture (b).

**(c) Formation of syngas**

In Figure 24(a) and Figure 24(b) the most important channels for production and loss of CO in a 70/30  $\text{CH}_4/\text{CO}_2$  and a 70/30  $\text{CH}_4/\text{O}_2$  gas mixture are illustrated, respectively.

As already mentioned above, the reaction of  $\text{CO}_2$  with  $\text{CH}_2$  radicals is the most important channel for the production of CO in a 70/30  $\text{CH}_4/\text{CO}_2$  gas mixture, with a relative contribution of 37% (see Figure 24(a)). Two other important production mechanisms are the reaction of  $\text{C}_2\text{H}_5$  with CHO, as well as electron impact dissociation of  $\text{CO}_2$ , which contribute for 28% and 13% to the total formation of CO in a 70/30  $\text{CH}_4/\text{CO}_2$  gas mixture. In the 70/30  $\text{CH}_4/\text{O}_2$  gas mixture, on the other hand, 90% of the CO formation occurs through the reaction of  $\text{O}_2$  molecules with CHO radicals. It is thus clear that the chemistry yielding CO formation is completely different in both gas mixtures. Note that in a 20/80  $\text{CH}_4/\text{CO}_2$  gas mixture, electron impact dissociation of  $\text{CO}_2$  becomes the most important channel for the production of CO.

The same applies to the loss of CO. Indeed, electron impact dissociation and ionization, as well as reactions with H radicals, are the most important loss processes for CO in the  $\text{CH}_4/\text{CO}_2$  gas mixture, while the reaction with OH radicals is the most important loss process for CO in the  $\text{CH}_4/\text{O}_2$  gas mixture. However, it is clear from Figure 24 that the total rate for CO formation is a factor 5 and 2.6 higher than the total loss rate, in the  $\text{CH}_4/\text{CO}_2$  and  $\text{CH}_4/\text{O}_2$  gas mixtures, respectively.



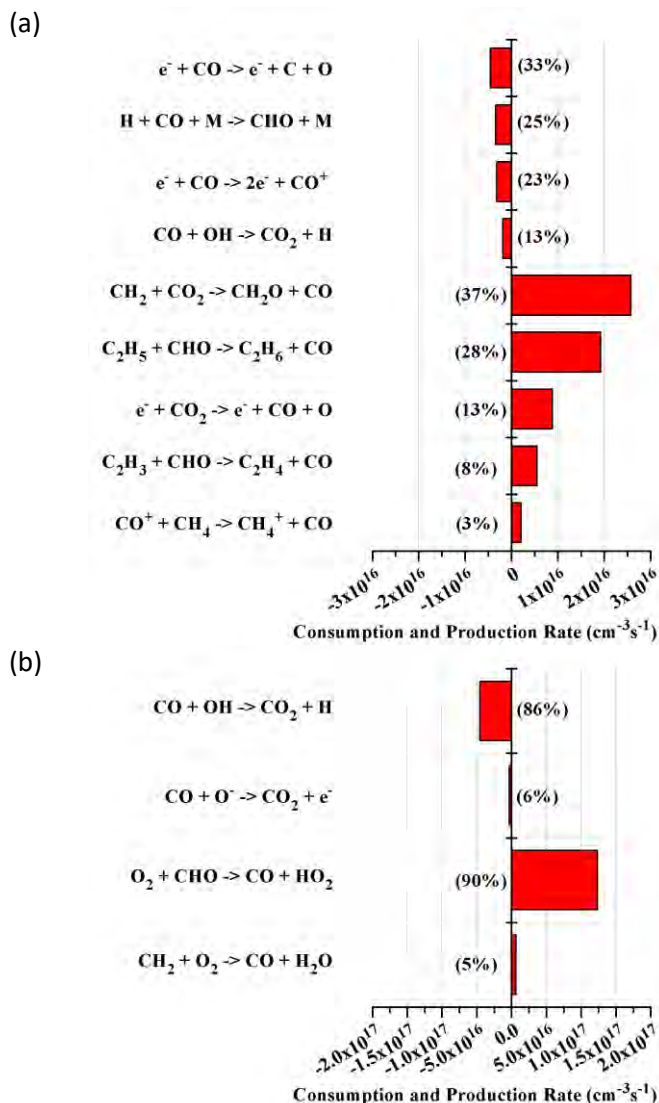


Figure 24. Time-averaged reaction rates of the dominant reaction pathways for the consumption and production of CO, for a 70/30  $\text{CH}_4/\text{CO}_2$  gas mixture (a) and a 70/30  $\text{CH}_4/\text{O}_2$  gas mixture (b).

Figure 25(a) and Figure 25(b) show the dominant reactions for production and loss of  $\text{H}_2$  in a 70/30  $\text{CH}_4/\text{CO}_2$  and a 70/30  $\text{CH}_4/\text{O}_2$  gas mixture, respectively.

In the 70/30  $\text{CH}_4/\text{CO}_2$  gas mixture, electron impact dissociation of  $\text{C}_2\text{H}_6$  and  $\text{C}_3\text{H}_8$  are the most important formation channels of  $\text{H}_2$ , while electron impact dissociation of  $\text{CH}_4$  only contributes for 12% (i.e., 8% (towards  $\text{CH}_2 + \text{H}_2$ ) + 3% (towards  $\text{CH} + \text{H}_2 + \text{H}$ ) + 1% (towards  $\text{C} + 2\text{H}_2$ , not shown in Figure 25(a)). In the 70/30  $\text{CH}_4/\text{O}_2$  gas mixture, however, electron impact dissociation of  $\text{CH}_4$  is clearly most important. Indeed, the higher hydrocarbons are of lower importance in this case (see Figure 17(a, b) above). However, when the initial fraction of  $\text{O}_2$  decreases, electron impact dissociation of  $\text{C}_2\text{H}_6$  and  $\text{C}_3\text{H}_8$  become the most important formation channels of  $\text{H}_2$ . Furthermore, electron impact dissociation is the most important loss process for  $\text{H}_2$  in both the  $\text{CH}_4/\text{CO}_2$  and the  $\text{CH}_4/\text{O}_2$  gas mixture. In the  $\text{CH}_4/\text{CO}_2$  mixture, the total loss rate is a factor 2 lower than the total production rate, while in the  $\text{CH}_4/\text{O}_2$  mixture, it is a factor 4 lower. Nevertheless, the overall  $\text{H}_2$  production is still much more pronounced in the  $\text{CH}_4/\text{CO}_2$  mixture than in the  $\text{CH}_4/\text{O}_2$  mixture (with a total rate of  $1.8 \times 10^{17} \text{ cm}^{-3}\text{s}^{-1}$  vs  $4.5 \times 10^{16} \text{ cm}^{-3}\text{s}^{-1}$ ; see Figure 25), and this explains the higher  $\text{H}_2$  density, as well as the higher  $\text{H}_2/\text{CO}$  molar ratio, in the  $\text{CH}_4/\text{CO}_2$  mixture. The reason for the higher  $\text{H}_2$  production in the  $\text{CH}_4/\text{CO}_2$  mixture is the higher formation of higher hydrocarbons (see above), which represent additional formation channels for  $\text{H}_2$ , as is clear from Figure 25(a).

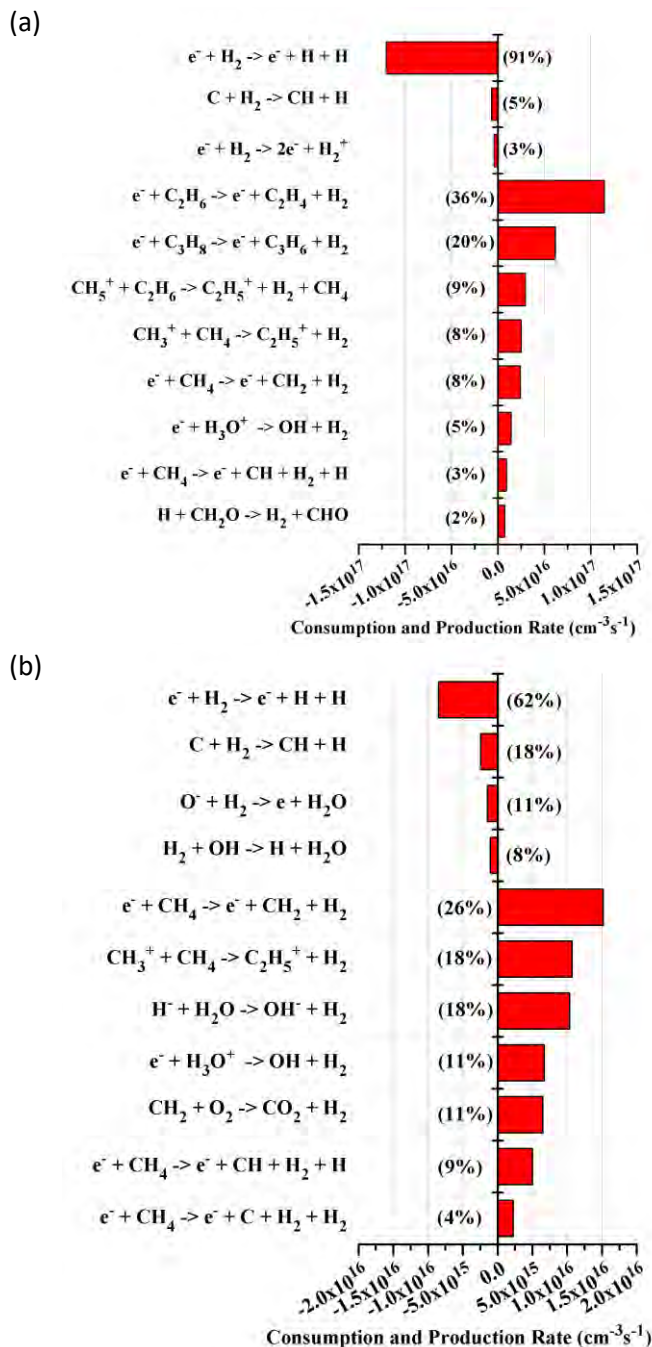


Figure 25. Time-averaged reaction rates of the dominant reaction pathways for the consumption and production of H<sub>2</sub>, for a 70/30 CH<sub>4</sub>/CO<sub>2</sub> gas mixture (a) and a 70/30 CH<sub>4</sub>/O<sub>2</sub> gas mixture (b).

**(d) Formation of methanol and formaldehyde**

Figure 26(a) and Figure 26(b) illustrate the dominant reactions for production and loss of CH<sub>3</sub>OH in a 70/30 CH<sub>4</sub>/CO<sub>2</sub> and a 70/30 CH<sub>4</sub>/O<sub>2</sub> gas mixture, respectively, while in Figure 27(a) and Figure 27(b) the dominant reactions for production and loss of CH<sub>2</sub>O in a 70/30 CH<sub>4</sub>/CO<sub>2</sub> and a 70/30 CH<sub>4</sub>/O<sub>2</sub> gas mixture are illustrated, respectively.

In the 70/30 CH<sub>4</sub>/CO<sub>2</sub> gas mixture, the production of methanol occurs almost entirely through the three-body reaction between the CH<sub>3</sub> and OH radicals, while in the 70/30 CH<sub>4</sub>/O<sub>2</sub> gas mixture, methanol is almost entirely formed by the reaction between H<sub>2</sub>O and CH<sub>3</sub>O radicals. Indeed, the rate of the three-body reaction between the CH<sub>3</sub> and OH radicals is one order of magnitude higher in CH<sub>4</sub>/CO<sub>2</sub> than in CH<sub>4</sub>/O<sub>2</sub> ( $1.1 \times 10^{15} \text{ cm}^{-3} \text{ s}^{-1}$  vs  $1.6 \times 10^{14} \text{ cm}^{-3} \text{ s}^{-1}$ ), but the rate of the reaction between H<sub>2</sub>O and CH<sub>3</sub>O radicals is four orders of magnitude higher in CH<sub>4</sub>/O<sub>2</sub> than in CH<sub>4</sub>/CO<sub>2</sub> ( $8.5 \times 10^{16} \text{ cm}^{-3} \text{ s}^{-1}$  vs  $1.4 \times 10^{12} \text{ cm}^{-3} \text{ s}^{-1}$ ). When comparing the overall production rates in Figure 26, it is clear that the total CH<sub>3</sub>OH production rate is almost two orders of magnitude higher in the CH<sub>4</sub>/O<sub>2</sub> mixture than in the CH<sub>4</sub>/CO<sub>2</sub> mixture, explaining the higher CH<sub>3</sub>OH density and yield in the CH<sub>4</sub>/O<sub>2</sub> mixture (see Figure 17 and Table 6 above).

As already mentioned above, the reaction between CO<sub>2</sub> and CH<sub>2</sub> radicals is the most important channel for the production of formaldehyde in the 70/30 CH<sub>4</sub>/CO<sub>2</sub> gas mixture, while in the 70/30 CH<sub>4</sub>/O<sub>2</sub> gas mixture, formaldehyde is mainly produced by the reactions of O<sub>2</sub> with CH<sub>2</sub>OH and CH<sub>3</sub>O, with relative contributions of 64% and 23%, respectively. The total production rate of CH<sub>2</sub>O is a factor 4 higher in the CH<sub>4</sub>/O<sub>2</sub> mixture than in the CH<sub>4</sub>/CO<sub>2</sub> mixture, but the total loss rate of CH<sub>2</sub>O is a factor 4.6 higher in the CH<sub>4</sub>/O<sub>2</sub> mixture than in the

CH<sub>4</sub>/CO<sub>2</sub> mixture, explaining the higher CH<sub>2</sub>O density and yield in the CH<sub>4</sub>/CO<sub>2</sub> mixture (see Figure 17 and Table 6 above).

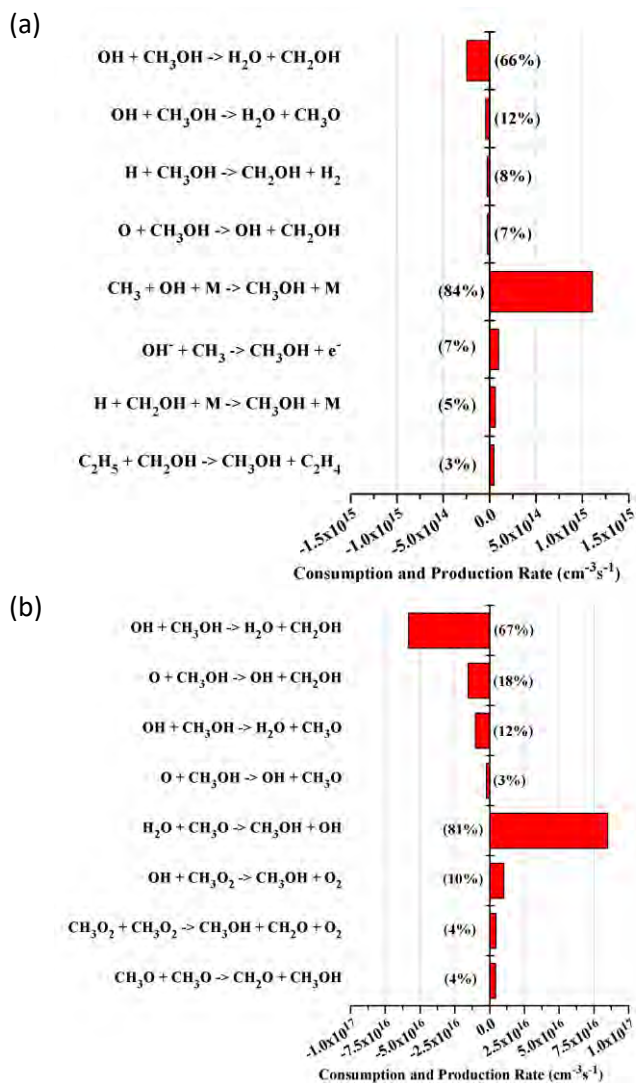
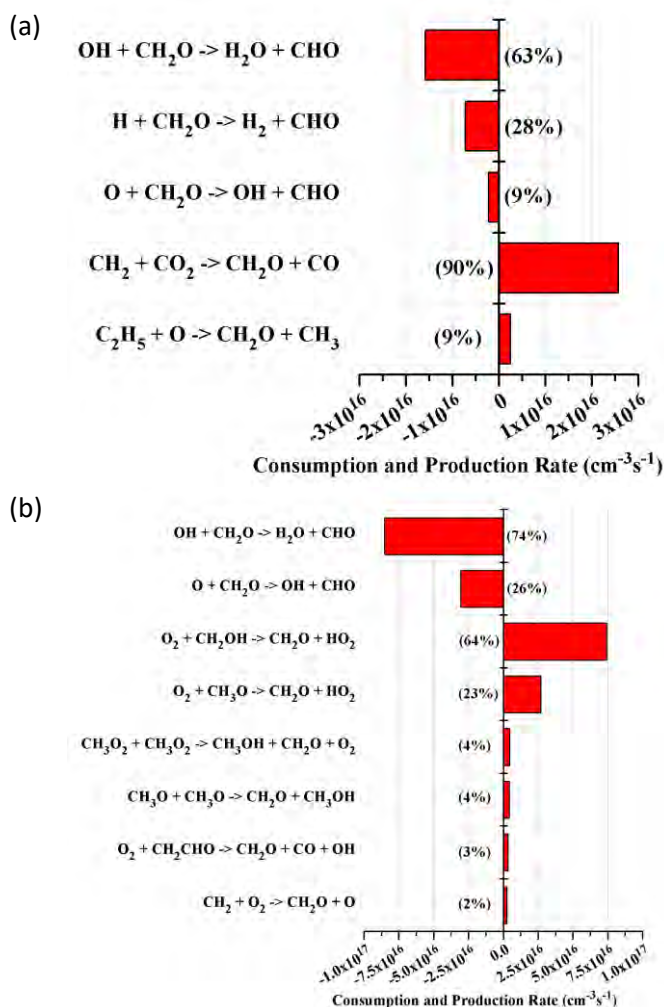


Figure 26. Time-averaged reaction rates of the dominant reaction pathways for the consumption and production of CH<sub>3</sub>OH, for a 70/30 CH<sub>4</sub>/CO<sub>2</sub> gas mixture (a) and a 70/30 CH<sub>4</sub>/O<sub>2</sub> gas mixture (b).



**Figure 27. Time-averaged reaction rates of the dominant reaction pathways for the consumption and production of  $\text{CH}_2\text{O}$ , for a 70/30  $\text{CH}_4/\text{CO}_2$  gas mixture (a) and a 70/30  $\text{CH}_4/\text{O}_2$  gas mixture (b).**

The most important loss process in both gas mixtures for both methanol and formaldehyde is the reaction with OH radicals. The overall loss rates are again typically lower than the overall production rates.

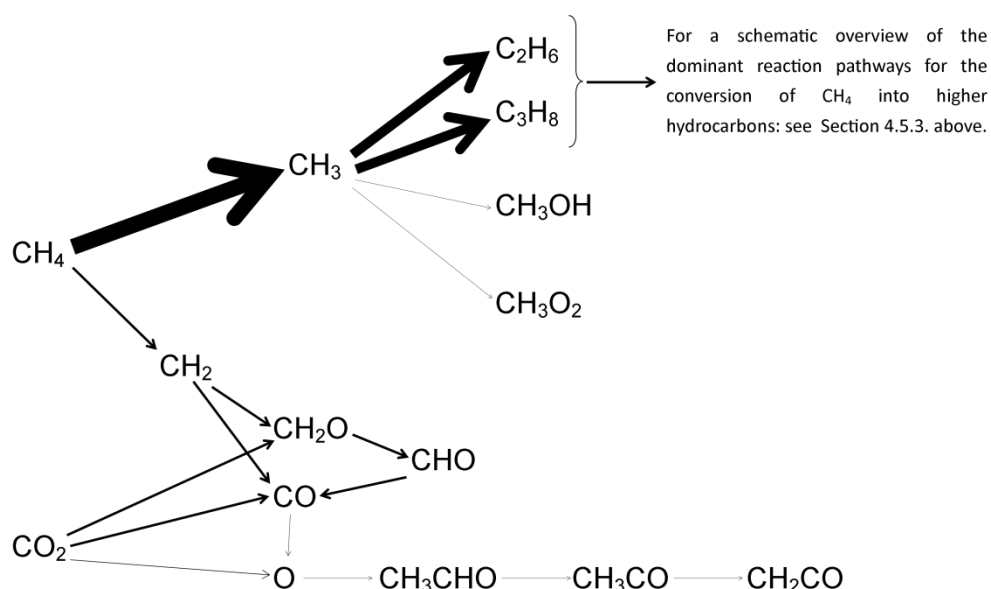
Note that for the 70/30  $\text{CH}_4/\text{O}_2$  gas mixture the degradation of methanol leads to the formation of  $\text{CH}_2\text{OH}$  (Figure 26(b)), which subsequently reacts to

formaldehyde (Figure 27(b)). The degradation of formaldehyde leads to the formation of  $\text{CHO}$ , which is subsequently converted to  $\text{CO}$  (Figure 24(b)). In other words, the formation processes of three of the desired end products ( $\text{CH}_3\text{OH}$ ,  $\text{CH}_2\text{O}$  and  $\text{CO}$ ) are dependent on each other in the 70/30  $\text{CH}_4/\text{O}_2$  gas mixture, which is in good agreement with the findings of Larkin et al.<sup>65</sup>. The development of a catalyst that activates or inhibits one of the reactions influencing the balance between these molecules should make it possible to favor selectively the formation of one of them.

#### **(e) Summary of the dominant pathways governing the conversion of $\text{CH}_4$ into higher oxygenates**

Figure 28 summarizes the dominant reaction pathways for the conversion of  $\text{CH}_4$  and  $\text{CO}_2$  into higher oxygenates in a 70/30  $\text{CH}_4/\text{CO}_2$  gas mixture. The conversion process starts with electron impact dissociation of  $\text{CH}_4$ , yielding the formation of the  $\text{CH}_3$  radicals. The  $\text{CH}_3$  radicals will recombine towards higher hydrocarbons, such as  $\text{C}_2\text{H}_6$  and  $\text{C}_3\text{H}_8$ . Subsequently, a number of dissociation and recombination reactions leads to the conversion towards the other, unsaturated hydrocarbons, and dissociation of  $\text{CH}_4$  and the higher hydrocarbons also yields the formation of  $\text{H}_2$ . The reaction mechanisms towards  $\text{H}_2$  and the higher hydrocarbons in the  $\text{CH}_4/\text{CO}_2$  mixture are exactly the same as in the case of pure  $\text{CH}_4$ , and thus, more details can be found in Section 4.5.3. above. However, in the  $\text{CH}_4/\text{CO}_2$  mixture, the  $\text{CH}_3$  radicals can also form methanol ( $\text{CH}_3\text{OH}$ ) and  $\text{CH}_3\text{O}_2$  radicals, albeit to a lower extent. Moreover, the  $\text{CH}_2$  radicals, which are also formed by electron impact dissociation of  $\text{CH}_4$ , react with the  $\text{CO}_2$  molecules, to form formaldehyde ( $\text{CH}_2\text{O}$ ) and  $\text{CO}$ . Finally, the  $\text{O}$  atoms, created from electron impact

dissociation of  $\text{CO}_2$ , initiate the formation of other oxygenates, like acetaldehyde ( $\text{CH}_3\text{CHO}$ ), which also reacts further into  $\text{CH}_3\text{CO}$  radicals, which can subsequently be converted into ketene ( $\text{CH}_2\text{CO}$ ). However, this reaction path is not so important, because of the limited formation of O radicals compared to CO and  $\text{CH}_2\text{O}$  out of the  $\text{CO}_2$  molecules.  $\text{H}_2$ , CO, ethane ( $\text{C}_2\text{H}_6$ ), propene ( $\text{C}_3\text{H}_6$ ) and  $\text{CH}_2\text{O}$  are the main end products of the conversion of  $\text{CH}_4$  and  $\text{CO}_2$  in a 70/30  $\text{CH}_4/\text{CO}_2$  gas mixture (see also Figure 17 above).



**Figure 28. Schematic overview of the dominant reaction pathways for the conversion of  $\text{CH}_4$  and  $\text{CO}_2$  into higher oxygenates in a 70/30  $\text{CH}_4/\text{CO}_2$  gas mixture. The thickness of the arrows is linearly proportional to the rate of the net reaction.**

The dominant reaction pathways for the conversion of  $\text{CH}_4$  and  $\text{O}_2$  into higher oxygenates in a 70/30  $\text{CH}_4/\text{O}_2$  gas mixture are schematically illustrated in Figure 29. Again, electron impact dissociation of  $\text{CH}_4$  results in the formation of  $\text{CH}_3$  radicals. The latter can recombine into methanol or higher hydrocarbons, but more important is the recombination into  $\text{CH}_3\text{O}_2$  radicals,



which form either  $\text{CH}_3\text{O}$  radicals or methyl hydroperoxide ( $\text{CH}_3\text{OOH}$ ). The  $\text{CH}_3\text{O}$  radicals yield the formation of methanol, which can react further into formaldehyde through the  $\text{CH}_2\text{OH}$  radicals, and formaldehyde can further be converted into  $\text{CO}$  through the  $\text{CHO}$  radicals (see above). Furthermore, formaldehyde is also partially converted into water. The  $\text{O}_2$  molecules are converted into  $\text{HO}_2$  radicals,  $\text{O}$  atoms and  $\text{CO}$ . They are also converted into  $\text{O}_3$  molecules, but the  $\text{O}$  atoms and  $\text{O}_3$  molecules quickly react back into  $\text{O}_2$  molecules at a somewhat larger rate, so there is a net formation of  $\text{O}_2$  molecules out of  $\text{O}_3$  (see the direction of the arrow in Figure 29). This delicate balance between  $\text{O}_2$ ,  $\text{O}$  and  $\text{O}_3$  was also discussed in detail in Aerts et al.<sup>197</sup>  $\text{CO}$  can be further oxidized into  $\text{CO}_2$ , which is of course undesired. The  $\text{O}$  atoms are also converted into  $\text{CH}_3\text{O}$  and  $\text{OH}$  radicals, which can again form water. The most important products in this  $\text{CH}_4/\text{O}_2$  mixture are  $\text{H}_2\text{O}$ ,  $\text{CO}$ ,  $\text{CO}_2$ ,  $\text{H}_2$ ,  $\text{O}_3$ ,  $\text{CH}_3\text{OH}$ , methyl hydroperoxide ( $\text{CH}_3\text{OOH}$ ) and hydrogen peroxide ( $\text{H}_2\text{O}_2$ ) (see also Figure 17 above). The reaction scheme revealed by our model for the conversion of  $\text{CH}_4$  and  $\text{O}_2$  into higher oxygenates is in good agreement with the proposed mechanisms for partial oxidation of  $\text{CH}_4$  by Goujard et al.<sup>105</sup> and Zhou et al.<sup>106</sup>.

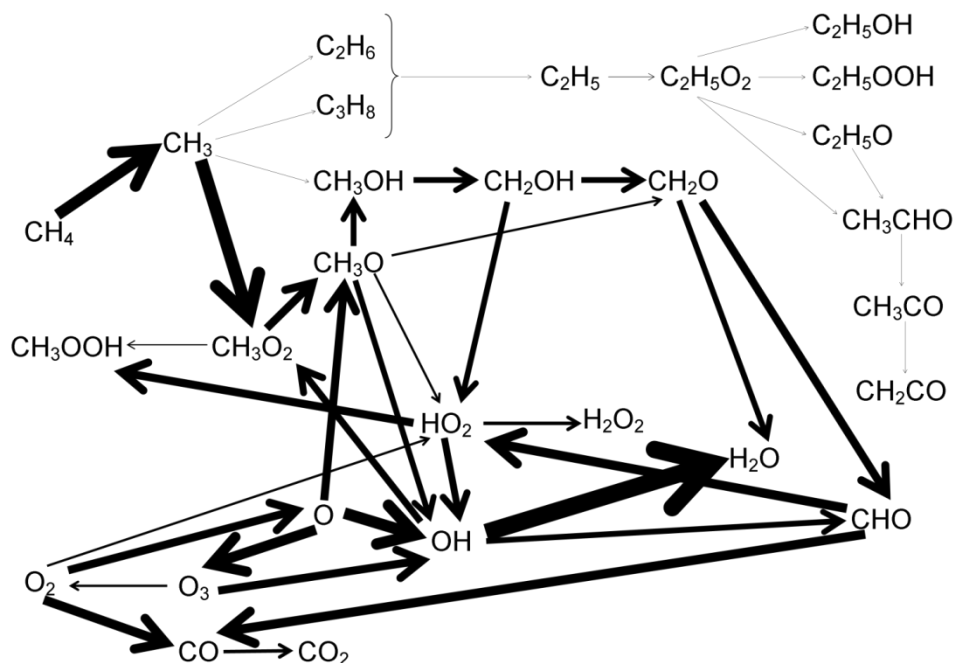


Figure 29. Schematic overview of the dominant reaction pathways for the conversion of  $\text{CH}_4$  and  $\text{O}_2$  into higher oxygenates in a 70/30  $\text{CH}_4/\text{O}_2$  gas mixture. The thickness of the arrows is linearly proportional to the rate of the net reaction.

## 5.6. Conclusion

In this chapter, we have presented the detailed plasma chemistry in a DBD plasma for the conversion of  $\text{CH}_4$  in the presence of  $\text{O}_2$  or  $\text{CO}_2$  into syngas, higher hydrocarbons and higher oxygenates. We have studied the densities of the various plasma species as a function of residence time and gas mixing ratio. The spatially averaged densities of the electrons, ions and radicals exhibit a periodic behavior as a function of time, following the sinusoidal applied voltage, while the spatially averaged molecule densities do not show a periodic behavior. While the densities of some molecules steadily rise as a function of residence time, the densities of other molecules go over a

maximum, or show a plateau after some time. This is important to realize, as a careful selection of the residence time can entail a higher production of some targeted molecules. We have also presented the densities of all molecules as a function of the initial gas mixing ratio. The mixtures with CO<sub>2</sub> favor the formation of H<sub>2</sub>, CH<sub>2</sub>O, CH<sub>3</sub>CHO and CH<sub>2</sub>CO, while the densities of H<sub>2</sub>O<sub>2</sub>, CH<sub>3</sub>OH, C<sub>2</sub>H<sub>5</sub>OH, CH<sub>3</sub>OOH and C<sub>2</sub>H<sub>5</sub>OOH are higher in the mixtures with O<sub>2</sub>. CO is formed at high density in both gas mixtures. Note that in the gas mixtures with O<sub>2</sub> as co-reactant also a significant amount of undesired CO<sub>2</sub> is formed.

The calculated conversions of the inlet gases as a function of residence time and initial gas mixing ratio are also illustrated. The conversion of CH<sub>4</sub> is roughly independent from the initial O<sub>2</sub> or CO<sub>2</sub> fraction (up to 30-40% CO<sub>2</sub>), but it increases for higher initial CO<sub>2</sub> fractions, especially above 70%. The conversion of O<sub>2</sub> and CO<sub>2</sub> both decrease with increasing initial O<sub>2</sub> or CO<sub>2</sub> fraction. However, the O<sub>2</sub> conversion is much higher than the CO<sub>2</sub> conversion.

Finally, the underlying plasma chemistry of the conversion process is analyzed in detail, and the dominant reaction pathways for the consumption of CH<sub>4</sub>, O<sub>2</sub> and CO<sub>2</sub> and the production and loss of the dominant end products, i.e., CO, H<sub>2</sub>, CH<sub>3</sub>OH and CH<sub>2</sub>O, are discussed. Electron impact dissociation of the inlet gases initiates the conversion process. The recombination of CH<sub>3</sub> radicals plays a crucial role and it was shown that this recombination leads to the formation of higher hydrocarbons in the mixtures with CO<sub>2</sub>, while CH<sub>3</sub>O<sub>2</sub> radicals are favored in the mixtures with O<sub>2</sub>. In the CH<sub>4</sub>/CO<sub>2</sub> mixture, also CH<sub>2</sub> radicals play a role, which can be converted into formaldehyde and CO molecules. In the CH<sub>4</sub>/O<sub>2</sub> mixture, the CH<sub>3</sub>O<sub>2</sub> radicals lead among others to the formation of methanol, which can react further into formaldehyde and the latter can form CO.

Our results are in reasonable agreement with reported results from literature for similar  $\text{CH}_4/\text{O}_2$  and  $\text{CH}_4/\text{CO}_2$  discharges. Moreover, our model provides additional information, mainly on the comparison between the formed end products in  $\text{CH}_4/\text{O}_2$  and  $\text{CH}_4/\text{CO}_2$  gas mixtures and on the different pathways leading to these products. In this way, the model can help to determine the most suitable feed gas ratio, residence time, co-reactant and other plasma parameters, to obtain the highest yield and/or selectivity of a desired oxygenate. However, as a lot of different products are typically formed in a plasma, the development of a catalyst, which increases the selective formation of some desired oxygenates, will be crucial. Furthermore, besides the conversion, yield and selectivity of specific products, also the energy efficiency of the discharge is critical, to determine whether or not plasma technology can compete with conventional technologies.



# Chapter 6

## The Hydrogenation of CO<sub>2</sub>

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The fluid model described in Chapter 3 is applied here to describe the plasma chemistry governing the hydrogenation of carbon dioxide. The spatially averaged densities of the most important end products formed in the CO<sub>2</sub>/H<sub>2</sub> mixture are determined as a function of the initial gas mixing ratio. CO and H<sub>2</sub>O are found to be present at the highest densities, and to a lower content also CH<sub>4</sub>, C<sub>2</sub>H<sub>6</sub>, CH<sub>2</sub>O, CH<sub>3</sub>OH, O<sub>2</sub> and some other higher hydrocarbons and oxygenates. The main underlying reaction pathways for the conversion of the inlet gases and the formation of CO, CH<sub>4</sub>, CH<sub>2</sub>O and CH<sub>3</sub>OH are pointed out for various gas mixing ratios. The CO<sub>2</sub> conversion and the production of value-added products is found to be quite low, also in comparison to a CO<sub>2</sub>/CH<sub>4</sub> mixture, and this can be explained by the model.

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## 6.1. Introduction

Current research on the use of plasma for CO<sub>2</sub> conversion includes the splitting of pure CO<sub>2</sub> into CO and O<sub>2</sub><sup>38, 68, 111, 197-218</sup>, and the direct synthesis of higher hydrocarbons, syngas and oxygenates through the reforming of CH<sub>4</sub> by CO<sub>2</sub><sup>14, 20-21, 64, 93, 107-109, 135-184</sup> (see Chapter 5) or the hydrogenation of CO<sub>2</sub><sup>219-222</sup>. However, application of the latter is up to now limited because of the high cost of hydrogen.<sup>136</sup>

Recently, the interest in the development of new sustainable industrial processes for the direct hydrogenation of CO<sub>2</sub> into CH<sub>3</sub>OH is increasing because of the potential of CH<sub>3</sub>OH in a growing hydrogen economy. Moreover, this hydrogenation process is a well-known reaction in catalysis research. In this chapter a modeling study for the hydrogenation of CO<sub>2</sub> in a DBD plasma will be discussed.

Experimental and modeling investigations on the plasma chemistry in CO<sub>2</sub>/H<sub>2</sub> mixtures reported in literature are very rare. Eliasson et al.<sup>219</sup> investigated the hydrogenation of CO<sub>2</sub> to CH<sub>3</sub>OH in a DBD with and without the presence of a catalyst. Experimentally the effects of combining a catalyst with a discharge on the yield of CH<sub>3</sub>OH were analyzed for different reaction parameters, such as the gas temperature, the pressure, the inlet gas mixing ratio, the electric power and the flow rate of the feed gas. Furthermore, a simplified semi-empirical kinetic model was used to simulate the accumulated chemical action of many microdischarges, in order to calculate the CH<sub>3</sub>OH yield in the CO<sub>2</sub>/H<sub>2</sub> discharge. A radical reaction mechanism was proposed for the formation of CH<sub>3</sub>OH. Liu et al.<sup>223</sup> discussed in a review paper the use of non-thermal plasmas for CO<sub>2</sub> utilization, including the hydrogenation of CO<sub>2</sub>

to form CH<sub>3</sub>OH in a DBD, referring thereby to the work of Eliasson et al.<sup>219</sup>. Hayashi et al.<sup>220</sup> discussed the decomposition of CO<sub>2</sub> in the presence of H<sub>2</sub> or water vapor by a non-thermal plasma, produced by a surface discharge at atmospheric pressure. CO, CH<sub>4</sub>, dimethyl ether (C<sub>2</sub>H<sub>6</sub>O), formic acid (HCOOH) and water vapor were detected as end products of a gas mixture of 50% CO<sub>2</sub> and 50% H<sub>2</sub>. Kano et al.<sup>221</sup> studied the reforming of CO<sub>2</sub> by H<sub>2</sub> to CH<sub>4</sub> and CH<sub>3</sub>OH by using a radio frequency impulse low-pressure discharge under different discharge parameters. CH<sub>4</sub>, CO, CH<sub>3</sub>OH and water vapor were found as end products. Recently Zeng et al.<sup>222</sup> investigated the plasma-catalytic CO<sub>2</sub> hydrogenation in a coaxial packed-bed DBD at low temperatures and atmospheric pressure. The performance of different  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> supported metal catalysts on the conversion of CO<sub>2</sub> was studied. The reverse water-gas shift reaction, i.e. the formation of CO and H<sub>2</sub>O, as well as carbon dioxide methanation, i.e. the formation of CH<sub>4</sub> and H<sub>2</sub>O, have been reported as the dominant reaction processes. The results also show that the H<sub>2</sub>/CO<sub>2</sub> molar ratio significantly affects the conversion of CO<sub>2</sub> and the yields of CO and CH<sub>4</sub>.

In this chapter we present the most important results on the conversion of CO<sub>2</sub>, in the presence of H<sub>2</sub>, into CO, higher hydrocarbons and higher oxygenates. The chemistry set is almost the same as used for the CH<sub>4</sub>/O<sub>2</sub> and CH<sub>4</sub>/CO<sub>2</sub> gas mixtures (see Chapter 5 above and Section 6.2. below). The formation of a variety of higher hydrocarbons and higher oxygenates in CO<sub>2</sub>/H<sub>2</sub> for different gas mixing ratios is calculated, as well as the conversion of the inlet gases. These results will be compared with the experimental observations from the papers mentioned above on CO<sub>2</sub>/H<sub>2</sub> gas discharges, as well as with earlier calculated results with the same model for a CH<sub>4</sub>/CO<sub>2</sub> gas mixture (see Chapter 5). Furthermore, the main underlying pathways



governing the conversion of CO<sub>2</sub> with H<sub>2</sub>, into the main reaction products, i.e., CO, CH<sub>4</sub>, CH<sub>2</sub>O and CH<sub>3</sub>OH, are discussed in order to explain the product formation in the different gas mixing ratios and to reveal why some oxygenates are formed while others seem not to be formed.

## 6.2. Species Included in the Model

As mentioned above, the chemistry set used for the CO<sub>2</sub>/H<sub>2</sub> gas mixture is almost identical to the one constructed for the CH<sub>4</sub>/O<sub>2</sub> and CH<sub>4</sub>/CO<sub>2</sub> gas mixture, except for some adaptations of the third body species in the neutral-neutral three-body collision reactions, where CO<sub>2</sub> and H<sub>2</sub> are now included as third body instead of CH<sub>4</sub>, O<sub>2</sub>, CO<sub>2</sub> and H<sub>2</sub>O, with the same rate coefficients. In total, 75 species (electrons, molecules, ions and radicals) are included in the model, as presented in Table 5 above. Note that dimethyl ether (CH<sub>3</sub>OCH<sub>3</sub>) and formic acid (HCOOH), which were experimentally found by Hayashi et al.<sup>220</sup>, as mentioned above, are not included in the model as the rate constants for the formation and loss processes for these molecules are not well known. As a consequence, our model will not be able to make predictions on the formation of these products. We expect that these species would anyway play a minor role in the chemistry, especially as intermediates. They might be potential end products, but we don't expect their densities to be higher than e.g., CH<sub>4</sub>, CH<sub>3</sub>OH and CH<sub>2</sub>O, and certainly much lower than e.g., CO.

## 6.3. Reactions Included in the Model

As mentioned in Chapter 5, the 75 species included in the model interact with each other in 963 gas phase reactions, including 157 electron-neutral, 48 electron-ion, 420 neutral-neutral and 338 ion-ion or ion-neutral reactions. Detailed information on the construction of the chemistry set and the transport coefficients and wall interaction coefficients used in the model can be found in Section 5.3. and Section 3.5., respectively.

## 6.4. Operating Conditions

The calculations are again carried out for a gas residence time up to 20s, at a fixed applied voltage of 5 kV and a frequency of 10 kHz, like in the previous chapter. The CO<sub>2</sub> fraction in the CO<sub>2</sub>/H<sub>2</sub> mixture is varied from 10 to 90%.

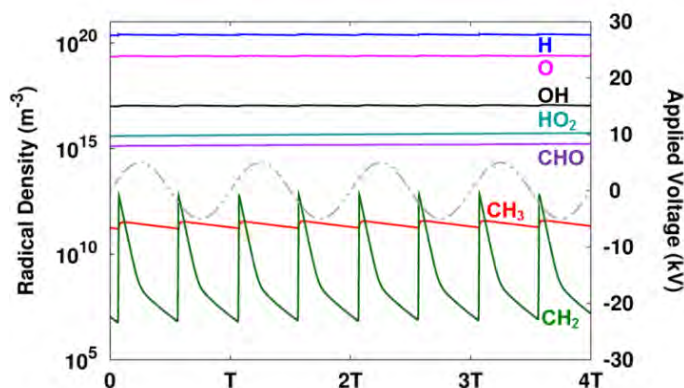
## 6.5. Results and Discussion

### 6.5.1. Densities of the Plasma Species

The spatially averaged electron density and the densities of the radicals and ions produced in the plasma exhibit periodic behavior as a function of time, following the period of the applied sinusoidal voltage. The overall spatially and time averaged electron density for all CO<sub>2</sub>/H<sub>2</sub> gas mixtures under study amounts to ca.  $10^{15} \text{ m}^{-3}$ , while the overall spatially and time averaged mean electron energy varies between 1.9eV and 2.7 eV. These results are similar to the values calculated in pure CH<sub>4</sub> (see Section 4.5.1.) and in the CH<sub>4</sub>/O<sub>2</sub> and

CH<sub>4</sub>/CO<sub>2</sub> gas mixtures (see Section 5.5.1.). More information on the periodic behavior of the electron density, and of the various ion densities, can thus be found in Section 4.5.1. and in Section 5.5.1. above.

Figure 30 illustrates the periodic behavior of the most important radical densities for a 50/50 CO<sub>2</sub>/H<sub>2</sub> gas mixture, on a logarithmic scale, for four periods of the applied voltage. The periodic trend is here superimposed on a rising or declining trend, acting over a longer time-scale until periodic steady state is reached. The most abundant radicals are H, O, OH, HO<sub>2</sub>, CHO, CH<sub>3</sub> and CH<sub>2</sub>, with overall spatially and time averaged densities up to about 10<sup>20</sup> m<sup>-3</sup>. Most of these radicals do not vary a lot as a function of time within one period, except for the CH<sub>2</sub> radicals. This is because the formation of all these radicals proceeds in a quite similar way, i.e. either directly or indirectly related to electron impact dissociation of the inlet gases. However, CH<sub>2</sub> is rapidly destructed in reactions with CO<sub>2</sub>, one of the inlet gases, which is thus present at high density, explaining the significant drop in the CH<sub>2</sub> density as a function of time, while H, O, OH, HO<sub>2</sub>, CHO and CH<sub>3</sub> react away through collisions with other radicals or molecules at lower densities. The most abundant radicals will determine the different reaction pathways for the formation of different end products (see below). Compared to our previous results for the CO<sub>2</sub>/CH<sub>4</sub> mixture (see Section 5.5.1.), the higher order hydrocarbon radicals, such as C<sub>2</sub>H<sub>5</sub> and C<sub>2</sub>H<sub>3</sub>, as well as the oxygenate radicals, such as CH<sub>3</sub>O, CH<sub>2</sub>OH and CH<sub>3</sub>O<sub>2</sub>, are formed to a lower extent in CO<sub>2</sub>/H<sub>2</sub>, which is logical, as there is no hydrocarbon precursor (CH<sub>4</sub>) in the inlet gas mixture, resulting in a lower overall carbon fraction than in CO<sub>2</sub>/CH<sub>4</sub>.

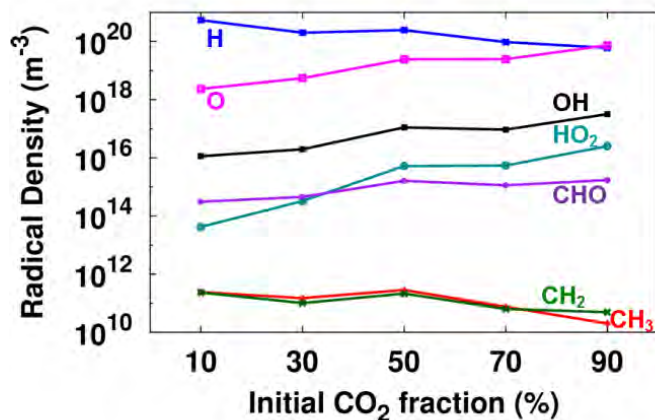


**Figure 30.** Spatially averaged radical densities (left axis) as a function of time for a 50/50 CO<sub>2</sub>/H<sub>2</sub> gas mixture, on a logarithmic scale, as well as the applied sinusoidal voltage (gray, right axis) for four periods of the applied voltage.

The spatially and time averaged densities of the most abundant radicals in CO<sub>2</sub>/H<sub>2</sub> are plotted in Figure 31 as a function of the initial CO<sub>2</sub> content in the mixture. Upon rising the initial fraction of CO<sub>2</sub> between 10 and 90 %, the densities of the H, CH<sub>3</sub> and CH<sub>2</sub> radicals drop by one order of magnitude, because these radicals are directly or indirectly formed out of H<sub>2</sub>. On the other hand, the densities of O, OH, HO<sub>2</sub> and CHO, as well as the other O-containing radicals (not shown), increase by one order to several orders of magnitude upon rising the inlet fraction of CO<sub>2</sub>, as they are directly or indirectly formed out of CO<sub>2</sub>.

The most abundant ion in the CO<sub>2</sub>/H<sub>2</sub> gas mixture is H<sub>3</sub>O<sup>+</sup>, with a spatially and time averaged density in the order of 10<sup>15</sup> m<sup>-3</sup>, hence comparable to the electron density (cf. above). The other ion densities are two or even more orders of magnitude lower, and thus the ion densities are much lower than the spatially and time averaged densities of the most abundant radicals, indicating that the ions play a minor role in the plasma chemistry (see also

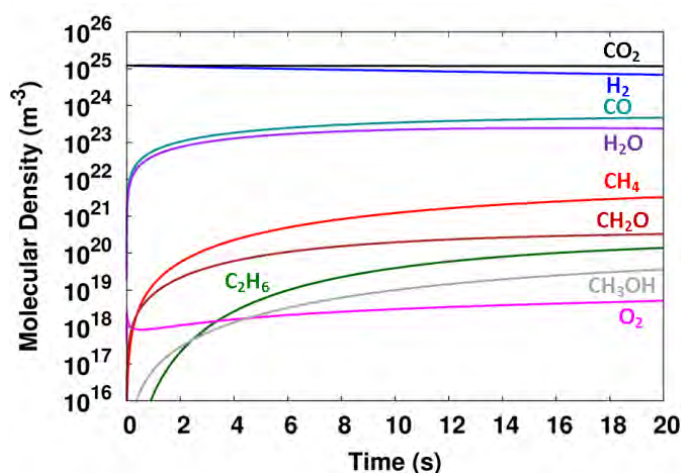
Section 6.5.3. below). Therefore, we do not go in further detail on the ion densities.



**Figure 31.** Spatially and time averaged radical densities as a function of the initial CO<sub>2</sub> fraction in the CO<sub>2</sub>/H<sub>2</sub> gas mixture.

The densities of the stable molecules do not exhibit a periodic behavior like the electrons and the radicals. The reason is that their formation rates are typically much larger than their loss rates, in contrast to the radicals and ions. The densities of the molecules formed during the hydrogenation of CO<sub>2</sub>, i.e., CO, higher order hydrocarbons and oxygenates, exhibit a rising trend as a function of time, because their net production is higher than their net consumption. This will continue until periodic steady state will be reached. Indeed, when the densities of the reaction products rise, the rates of their consumption reactions will rise as well, until a balance is reached between production and consumption. The inlet gases, on the other hand, have a higher net consumption, so their densities show a gradual decrease as a function of time again until periodic steady state will be reached. The

conversion is most pronounced in the first few seconds, and afterwards the densities of the molecules do not significantly change anymore for a longer residence time, as is clear from Figure 32, for both CO<sub>2</sub> and H<sub>2</sub>, and the most abundant products.



**Figure 32.** Spatially averaged molecular densities as a function of the residence time for a 50/50 CO<sub>2</sub>/H<sub>2</sub> gas mixture.

Figure 33 illustrates the densities of the various molecules in the CO<sub>2</sub>/H<sub>2</sub> gas mixture as a function of the initial CO<sub>2</sub> fraction, after a residence time of 5 seconds. The most abundant reaction products are CO, H<sub>2</sub>O, CH<sub>4</sub>, CH<sub>2</sub>O, C<sub>2</sub>H<sub>6</sub>, O<sub>2</sub> and CH<sub>3</sub>OH (more or less in order of decreasing density). This is in good agreement with the end products reported by Eliasson et al.<sup>219</sup>, i.e. CH<sub>4</sub> and CH<sub>3</sub>OH, Hayashi et al.<sup>220</sup>, i.e. CO and CH<sub>4</sub>, Kano et al.<sup>221</sup>, i.e. CO, CH<sub>4</sub> and CH<sub>3</sub>OH, and Zeng et al.<sup>222</sup>, i.e. CO and H<sub>2</sub>O as major products, a small amount of CH<sub>4</sub> and traces of C<sub>2</sub>H<sub>6</sub>, for similar CO<sub>2</sub>/H<sub>2</sub> discharges. Note that Hayashi et al.<sup>220</sup> also detected the formation of dimethyl ether and formic acid, which are not included in our model as mentioned above. However, our model provides

us more insight in the formation of other higher hydrocarbons and oxygenates. The densities of CO and H<sub>2</sub>O, which are by far the most abundant products, are almost not influenced by the inlet fraction of CO<sub>2</sub> (see Figure 33(a)). For H<sub>2</sub>O, a maximum is obtained at an initial CO<sub>2</sub> fraction of 50%. This can be explained because H<sub>2</sub>O is formed out of the collision of OH and H radicals. From Figure 31 it is clear that the H density decreases while the OH density increases with increasing initial CO<sub>2</sub> fraction, resulting in an optimum ratio at an inlet concentration of 50% CO<sub>2</sub>. Furthermore, as will be clear from Section 6.5.2. below, the CO<sub>2</sub> conversion drops upon increasing initial CO<sub>2</sub> fraction in the mixture, and thus, the same applies to the yield of CO. On the other hand, a higher initial CO<sub>2</sub> fraction in the mixture allows for more CO<sub>2</sub> to be converted, and as both effects compensate each other, the effective CO<sub>2</sub> conversion remains constant, explaining why the CO density is constant for all CO<sub>2</sub>/H<sub>2</sub> gas mixtures (see Figure 33(a)).

On the other hand, the densities of O<sub>2</sub>, H<sub>2</sub>O<sub>2</sub> and O<sub>3</sub> increase by several orders of magnitude upon increasing initial fraction of CO<sub>2</sub>, which is logical, as they are directly formed out of the CO<sub>2</sub> splitting products (O and O<sub>2</sub>). The densities of the higher hydrocarbons (C<sub>x</sub>H<sub>y</sub>) generally drop upon increasing initial fraction of CO<sub>2</sub>, which can be explained by the higher conversion of CO<sub>2</sub> at lower initial fraction of CO<sub>2</sub> (see Section 6.5.2. below) resulting in higher densities of CH<sub>2</sub> and CH<sub>3</sub> radicals, as is clear from Figure 31 above, which are the building blocks for the higher hydrocarbons. However, an optimum seems to be reached for the 50/50 CO<sub>2</sub>/H<sub>2</sub> gas mixture (see Figure 33(b)). Indeed, these higher hydrocarbons need the C from CO<sub>2</sub> as their building block, but they also need the H originating from H<sub>2</sub>, and therefore an equal presence of both inlet gases seems to be preferable.

The same is true for the densities of CH<sub>2</sub>O and CH<sub>3</sub>OH and the other oxygenates, as is clear from Figure 33(c), although the hydroperoxides (CH<sub>3</sub>OOH and C<sub>2</sub>H<sub>5</sub>OOH) generally increase with rising initial fraction of CO<sub>2</sub>. Compared to our previous results on the formation of higher hydrocarbons and oxygenates in CH<sub>4</sub>/O<sub>2</sub> and CH<sub>4</sub>/CO<sub>2</sub> mixtures (see Section 5.5.1.), it is clear that except for CO and H<sub>2</sub>O, the densities of the most important end products are now several orders of magnitude lower. The reason for this is that the conversion of CO<sub>2</sub> is very low in all gas mixtures (see Section 6.5.2. below), while CH<sub>4</sub> as C building block was more easily converted (see Section 5.5.2. above), and therefore, the crucial radicals in the formation process of higher hydrocarbons and oxygenates, such as CH<sub>2</sub> and CH<sub>3</sub>, can be produced at a much higher density in mixtures with CH<sub>4</sub> than in the CO<sub>2</sub>/H<sub>2</sub> mixture under study here. Note that the trends illustrated in Figure 33 correspond to a residence time of 5 seconds; however, the different molecules might have their maximum densities at a different residence time for the different gas mixing ratios studied (see also Section 5.5.1.); therefore the trends depicted in Figure 33 are not necessarily the same at other residence times.

Altering the inlet gas mixing ratio also affects the H<sub>2</sub>/CO (syngas) ratio. A variable H<sub>2</sub>/CO molar ratio is useful, as it allows the mixture to be used for various industrial synthesis processes (see Section 5.5.1.). The H<sub>2</sub>/CO ratio, as obtained from our calculations, decreases with increasing initial CO<sub>2</sub> fraction, which is logical. It ranges from 54 (at 10% CO<sub>2</sub>), which is not useful for industrial synthesis processes, to 3 (at 90% CO<sub>2</sub>), which can be of interest as this is similar to the molar ratio produced by steam reforming (see Section 5.5.1.).



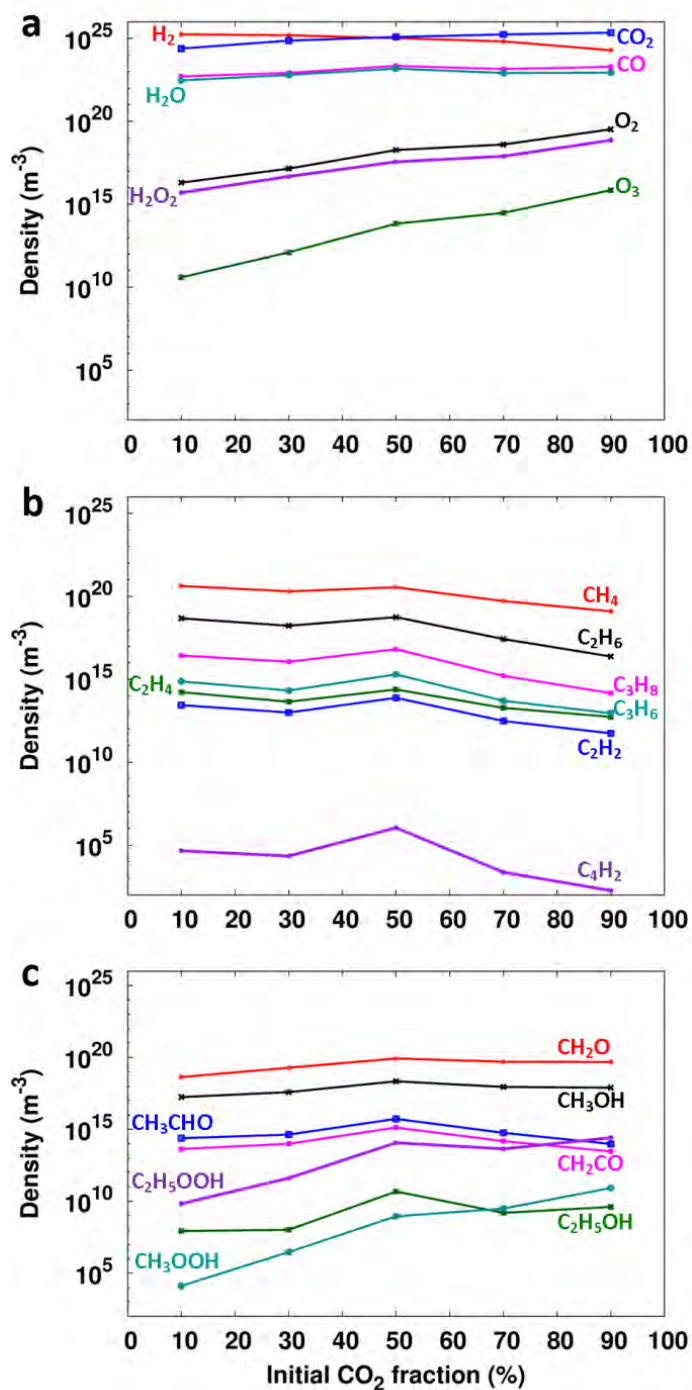


Figure 33. Spatially averaged molecule densities as a function of the initial CO<sub>2</sub> fraction in the CO<sub>2</sub>/H<sub>2</sub> gas mixture, after a residence time of 5 seconds.

### 6.5.2. Conversion, Yields and Selectivities

Table 7 shows the maximum conversions of the inlet gases, i.e. CO<sub>2</sub> and H<sub>2</sub>, and the maximum yields and corresponding selectivities of CO and CH<sub>4</sub>, for different CO<sub>2</sub>/H<sub>2</sub> gas mixtures. These maximum values are in all cases obtained for a residence time of 20s. The conversion of CO<sub>2</sub> clearly decreases with increasing initial CO<sub>2</sub> fraction in the mixture, from 7% at 10% CO<sub>2</sub> in the mixture to roughly 2% at 90% CO<sub>2</sub> in the mixture. This trend is in good agreement with the results of Zeng et al.<sup>222</sup>, who reported that the conversion of CO<sub>2</sub> increases almost linearly with the increase of the H<sub>2</sub>/CO<sub>2</sub> molar ratio at a fixed flow rate. A similar trend was also observed in CO<sub>2</sub>/CH<sub>4</sub> (see Section 5.5.2. above), but the conversion of CO<sub>2</sub> was a factor 3 higher at a high initial CH<sub>4</sub> fraction (i.e., 90%) compared to a high initial H<sub>2</sub> fraction of 90%. This can be explained because CH<sub>2</sub>, which is a direct dissociation product of CH<sub>4</sub>, is much more abundant in CO<sub>2</sub>/CH<sub>4</sub> than in CO<sub>2</sub>/H<sub>2</sub>, and thus provides an extra and very important loss process for CO<sub>2</sub> in a CO<sub>2</sub>/CH<sub>4</sub> mixture (see Section 5.5.). The H<sub>2</sub> conversion is significantly larger, i.e., between 30 and 60 %, but no clear trend can be observed as a function of gas mixing ratio, because the discharge characteristics are strongly affected by the initial gas mixing ratio. As CO is directly produced by electron impact dissociation of CO<sub>2</sub> (see Section 6.5.3. below), the yield of CO shows the same trend as the conversion of CO<sub>2</sub>, with values of only 2-6 %. Moreover, CO is the only C containing molecule directly produced out of CO<sub>2</sub> and therefore the selectivity of CO is in all cases around 90%. CH<sub>4</sub> is only formed with a selectivity above 1% at a low initial CO<sub>2</sub> fraction, i.e. a high initial H<sub>2</sub> fraction, which is logical. The yields of C<sub>2</sub>H<sub>6</sub>, CH<sub>2</sub>O and CH<sub>3</sub>OH are one or two orders of magnitude lower than the yield of CH<sub>4</sub>, while the yields of other higher hydrocarbons and oxygenates are even more

negligible, which is of course the direct result of the rather low conversion of CO<sub>2</sub> in all gas mixing ratios. Note that also some sticking of the C atoms and hydrocarbon species at the walls occurs, which explains why the sum of the selectivities is not equal to 100 %. This formation of a C-containing layer on the electrodes was indeed also experimentally observed in the DBD reactor under study for a pure CO<sub>2</sub> discharge.<sup>214, 224</sup>

**Table 7. Overview of the maximum conversions of the inlet gases, i.e. CO<sub>2</sub> and H<sub>2</sub>, and the maximum yields and corresponding selectivities of CO and CH<sub>4</sub> for different CO<sub>2</sub>/H<sub>2</sub> gas mixtures. All values are noted as percentage.**

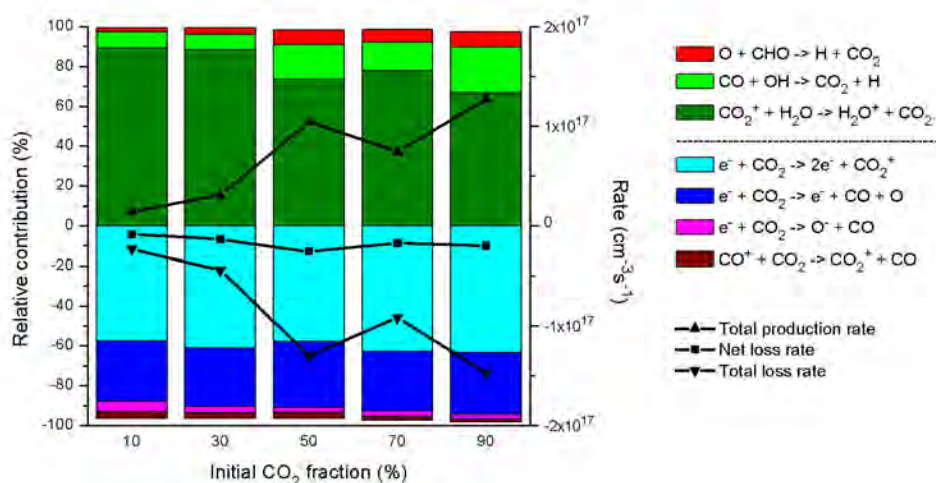
Initial CO <sub>2</sub> fraction	X (CO <sub>2</sub> )	X (H <sub>2</sub> )	Y (CO) - S (CO)	Y (CH <sub>4</sub> ) - S (CH <sub>4</sub> )
10	7.0	64	6 - 86	0.2 - 2.2
30	3.6	33	3 - 90	0.03 - 0.9
50	4.4	44	4 - 87	0.03 - 0.6
70	2.1	33	2 - 89	0.003 - 0.2
90	1.9	58	2 - 92	0.0003 - 0.02

### 6.5.3. Dominant Reaction Pathways

To better explain the above trends, and to find out how the densities of the most important products can be optimized, it is crucial to obtain a better insight in the underlying reaction chemistry. Therefore, we will now discuss the dominant reaction pathways for the conversion of the inlet gases into the most important value-added products, i.e., CO, CH<sub>4</sub>, CH<sub>3</sub>OH and CH<sub>2</sub>O, for the entire range of gas mixing ratios.

**(a) Dissociation of CO<sub>2</sub> and H<sub>2</sub>**

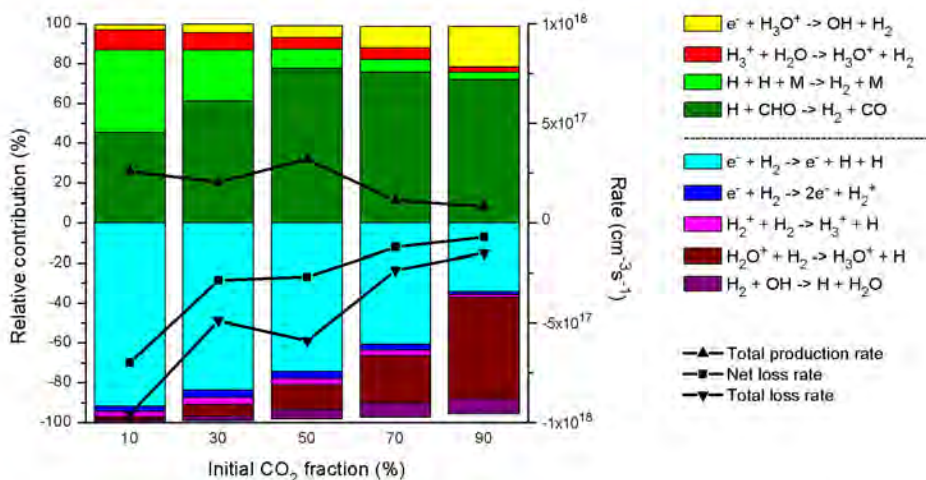
The dominant reactions for CO<sub>2</sub> consumption (and production), as well as the time-averaged total production rate, total loss rate and net loss rate, as a function of the initial CO<sub>2</sub> fraction in the gas mixture are depicted in Figure 34. Although the consumption of CO<sub>2</sub> is mostly relevant in this work, we also show the production processes, because part of the CO<sub>2</sub> dissociation products will again recombine into the formation of CO<sub>2</sub>. However, the total loss rate is larger than the total production rate, as is clear from Figure 34, thus leading to a net loss of CO<sub>2</sub> (i.e., conversion into other products). Furthermore, the total formation and loss rate generally increase upon larger initial CO<sub>2</sub> fraction in the mixture, which is logical. The most important channel for consumption of CO<sub>2</sub> is electron impact ionization towards CO<sub>2</sub><sup>+</sup>. However, CO<sub>2</sub><sup>+</sup> immediately reacts back towards CO<sub>2</sub> upon charge transfer with H<sub>2</sub>O molecules. Therefore, the most important reaction for consumption of CO<sub>2</sub> is effectively electron impact dissociation towards CO. This result was also obtained in earlier simulations carried out in our group for pure CO<sub>2</sub> splitting.<sup>197</sup> Furthermore, the relative importance of the various consumption and production processes is more or less independent from the gas mixing ratio, as is clear from Figure 34.



**Figure 34.** Relative contributions of the various production and consumption processes of CO<sub>2</sub> (left axis), as well as the time-averaged total production rate, total loss rate and net loss rate (right axis), as a function of the initial CO<sub>2</sub> fraction in the CO<sub>2</sub>/H<sub>2</sub> gas mixture. The production rates are defined as positive values, while the consumption rates are plotted as negative values.

In Figure 35 the most important reactions for consumption (and production) of H<sub>2</sub> are shown. At an initial CO<sub>2</sub> inlet fraction of 10%, electron impact dissociation is the most important loss process for H<sub>2</sub>, but part of the H atoms will recombine back into H<sub>2</sub>, or react with CHO radicals into H<sub>2</sub> and CO. At an inlet fraction of 90% CO<sub>2</sub> the reaction of H<sub>2</sub> with H<sub>2</sub>O<sup>+</sup> towards H<sub>3</sub>O<sup>+</sup> becomes the most important loss mechanism. However, the latter is not due to the high absolute rate of this reaction, but rather because the rate of electron impact dissociation drops. Indeed, it is clear from Figure 35 that the total loss rate of H<sub>2</sub> is much lower at 90% than at 10% CO<sub>2</sub> content, because there is of course less H<sub>2</sub> in the mixture. Nevertheless, from comparing Figure 34 and Figure 35 it is clear that the net consumption of H<sub>2</sub> is much higher than the net consumption of CO<sub>2</sub>. Indeed, the net loss rate of H<sub>2</sub> drops from

$7 \times 10^{17} \text{ cm}^{-3} \text{ s}^{-1}$  at 10% CO<sub>2</sub> to  $7 \times 10^{16} \text{ cm}^{-3} \text{ s}^{-1}$  at 90% CO<sub>2</sub>, while the net loss rate of CO<sub>2</sub> is virtually constant around  $10^{16} \text{ cm}^{-3} \text{ s}^{-1}$  for all gas mixing ratios. This explains also why the conversion of H<sub>2</sub> is much higher than the conversion of CO<sub>2</sub> (see Section 6.5.2. above).

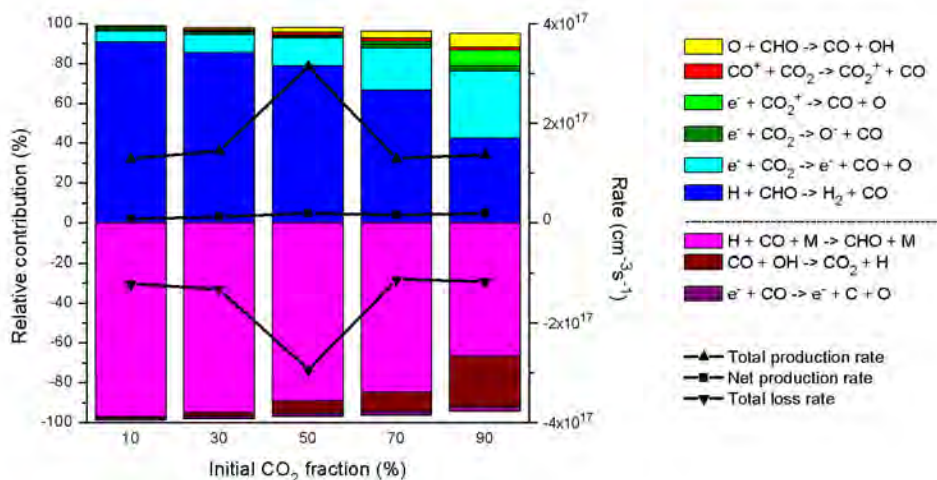


**Figure 35.** Relative contributions of the production and consumption processes of H<sub>2</sub> (left axis), as well as the time-averaged total production rate, total loss rate and net loss rate (right axis), as a function of the initial CO<sub>2</sub> fraction in the CO<sub>2</sub>/H<sub>2</sub> gas mixture.

### (b) Formation of CO, CH<sub>4</sub>, CH<sub>2</sub>O and CH<sub>3</sub>OH

In Figure 36 the most important channels for the production (and loss) of CO are illustrated as a function of the initial CO<sub>2</sub> fraction in the gas mixture. The most important production process appears to be the reaction between H atoms and CHO radicals, forming H<sub>2</sub> and CO, but this reaction is counterbalanced by the most important loss process, i.e., the recombination of H with CO into CHO radicals. Therefore the most important effective

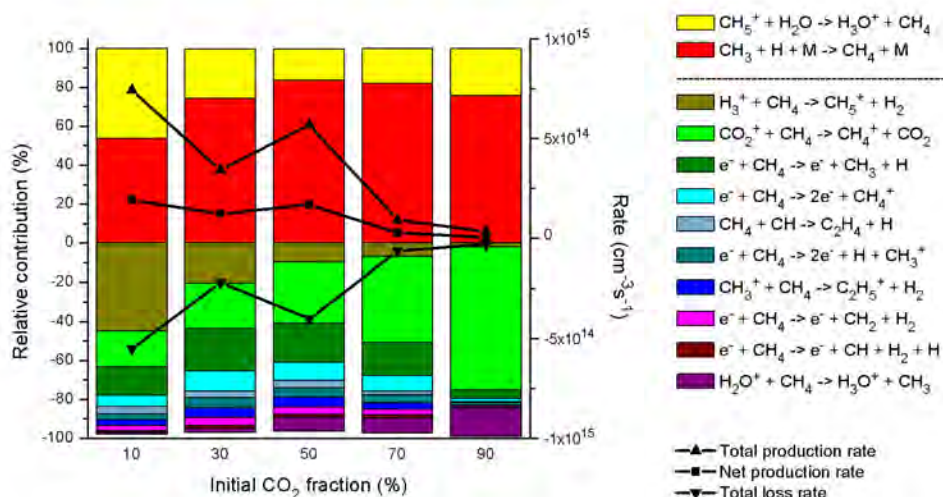
reaction for the formation of CO is electron impact dissociation of CO<sub>2</sub>. On average there is a net formation of CO, with a rate in the order of  $10^{16} \text{ cm}^{-3} \text{ s}^{-1}$ , slightly increasing upon higher initial CO<sub>2</sub> fraction in the mixture, which is logical.



**Figure 36.** Relative contributions of the production and consumption processes of CO (left axis), as well as the time-averaged total production rate, total loss rate and net production rate (right axis), as a function of the initial CO<sub>2</sub> fraction in the CO<sub>2</sub>/H<sub>2</sub> gas mixture.

The most important reactions for production (and loss) of CH<sub>4</sub> are depicted in Figure 37 as a function of the initial CO<sub>2</sub> fraction in the gas mixture. The production of CH<sub>4</sub> seems to be driven by only two reactions, i.e., the three-body recombination reaction between CH<sub>3</sub> and H radicals, and at a lower initial fraction of CO<sub>2</sub> also the charge transfer reaction between CH<sub>5</sub><sup>+</sup> and H<sub>2</sub>O. However, the latter reaction is partially balanced by the loss of CH<sub>4</sub> via a charge transfer reaction with H<sub>3</sub><sup>+</sup>. At a higher initial CO<sub>2</sub> fraction, the charge transfer reaction with CO<sub>2</sub><sup>+</sup> becomes the most important loss mechanism for

CH<sub>4</sub>. A similar trend is observed for the net production rate of CH<sub>4</sub> as a function of the initial CO<sub>2</sub> fraction as for the net loss rate of H<sub>2</sub> (see Figure 35 above). Indeed, the dissociation of H<sub>2</sub> leads to the formation of H radicals which are needed for the formation of CH<sub>4</sub>. An optimum is obtained for an initial CO<sub>2</sub> fraction of 10%, as is logical, and can be explained by the maximum densities found for the CH<sub>3</sub> and H radicals, as shown in Figure 31 above.



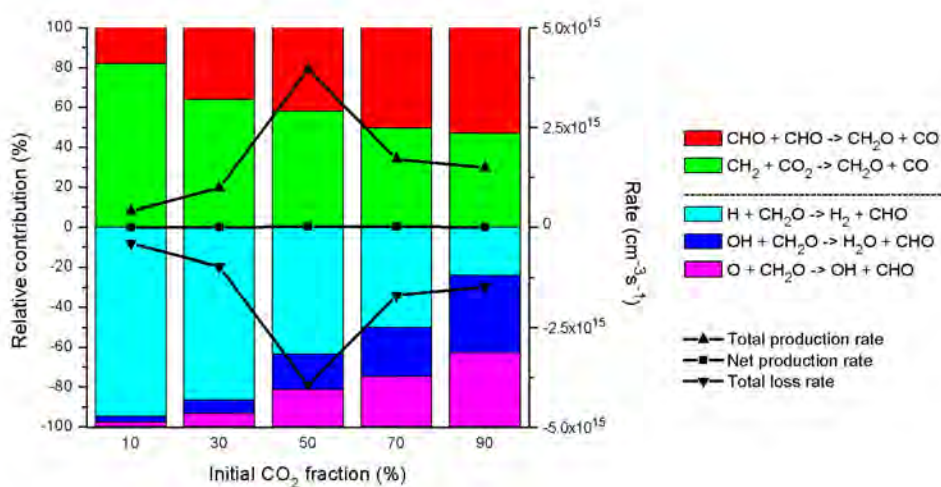
**Figure 37.** Relative contributions of the production and consumption processes of CH<sub>4</sub> (left axis), as well as the time-averaged total production rate, total loss rate and net production rate (right axis), as a function of the initial CO<sub>2</sub> fraction in the CO<sub>2</sub>/H<sub>2</sub> gas mixture.

Figure 38 and Figure 39 show the dominant reactions for production (and loss) of CH<sub>2</sub>O and CH<sub>3</sub>OH, respectively, as a function of the initial CO<sub>2</sub> fraction in the gas mixture. The reaction between CO<sub>2</sub> and CH<sub>2</sub> radicals appears to be the most important channel for the production of formaldehyde at low initial CO<sub>2</sub> fractions, as was also observed for a CO<sub>2</sub>/CH<sub>4</sub> mixture (see Section 5.5.3.). At higher initial CO<sub>2</sub> fractions, CH<sub>2</sub>O is also formed to some extent out of two



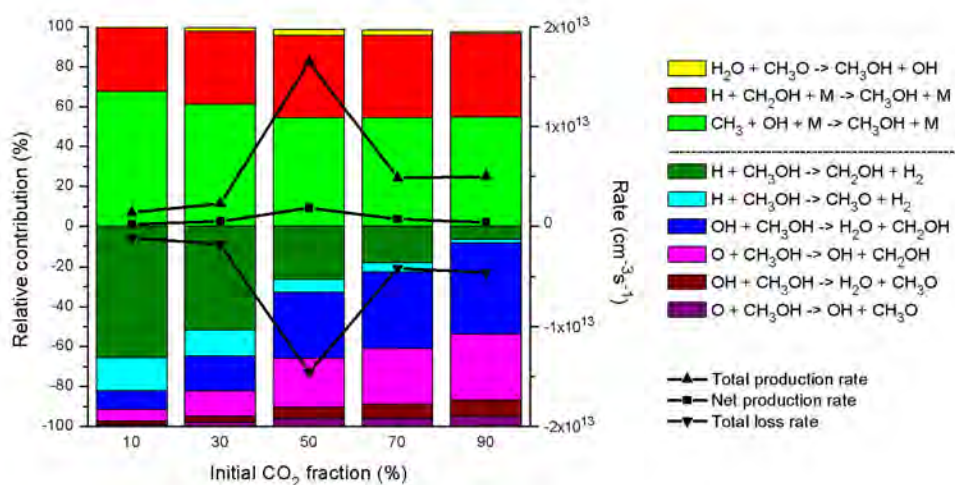
CHO radicals. Furthermore, CH<sub>2</sub>O is mainly lost upon collision with H atoms, yielding CHO and H<sub>2</sub>, although the collisions with O atoms or OH radicals, yielding CHO and OH or H<sub>2</sub>O, respectively, become gradually more important at higher CO<sub>2</sub> fractions, which is logical.

The total formation and loss rates reach a clear maximum at 50% CO<sub>2</sub> in the mixture, which is explained by the fact that at these conditions an optimum ratio of CH<sub>2</sub> (see maximum in Figure 31 above) and CO<sub>2</sub> is present in the gas mixture. As the total formation and loss rates are more or less equal to each other, the net formation rate of CH<sub>2</sub>O is very low, and increases from 10<sup>11</sup> to 10<sup>13</sup> cm<sup>-3</sup>s<sup>-1</sup> upon rising CO<sub>2</sub> fraction. This explains why the CH<sub>2</sub>O density rises slightly upon increasing CO<sub>2</sub> fraction in the mixture, as illustrated in Figure 33 above.



**Figure 38.** Relative contributions of the production and consumption processes of CH<sub>2</sub>O (left axis), as well as the time-averaged total production rate, total loss rate and net production rate (right axis), as a function of the initial CO<sub>2</sub> fraction in the CO<sub>2</sub>/H<sub>2</sub> gas mixture.

As is clear from Figure 39, the most important channel for the production of methanol, as predicted by our model, is the three-body reaction between CH<sub>3</sub> and OH radicals, like was also the case in the CO<sub>2</sub>/CH<sub>4</sub> mixture studied before (see Section 5.5.3.). However, different from the CO<sub>2</sub>/CH<sub>4</sub> mixture, the three-body reaction between CH<sub>2</sub>OH and H radicals is now also an important production channel. Most of the CH<sub>3</sub>OH produced, is also consumed again upon collision with either H atoms, OH radicals or O atoms, so the net formation rate of CH<sub>3</sub>OH varies from 10<sup>11</sup> to 10<sup>12</sup> cm<sup>-3</sup>s<sup>-1</sup>. An optimum production of CH<sub>3</sub>OH is again observed at 50/50 CO<sub>2</sub>/H<sub>2</sub>, because at these conditions an optimum ratio of CH<sub>3</sub> and OH (see Figure 31 above) is present in the gas mixture, and this explains why the CH<sub>3</sub>OH density reaches a maximum at this mixing ratio, as shown in Figure 33 above.



**Figure 39.** Relative contributions of the production and consumption processes of CH<sub>3</sub>OH (left axis), as well as the time-averaged total production rate, total loss rate and net production rate (right axis), as a function of the initial CO<sub>2</sub> fraction in the CO<sub>2</sub>/H<sub>2</sub> gas mixture.

### **(c) Overall reaction mechanism for the hydrogenation of CO<sub>2</sub> into valuable products**

Figure 40 summarizes the dominant reaction pathways for the conversion of CO<sub>2</sub> and H<sub>2</sub> in a 50/50 CO<sub>2</sub>/H<sub>2</sub> gas mixture. Note that the thickness of the arrow lines is proportional to the rates of the net reactions. The conversion starts with electron impact dissociation of CO<sub>2</sub>, yielding CO and O radicals. Simultaneously, and much more pronounced, is the electron impact dissociation of H<sub>2</sub>, resulting in the formation of H radicals (cf. the thickness of the arrow line). Radical recombination reactions of the O and H radicals lead to the formation of OH radicals, which recombine further into H<sub>2</sub>O, and this explains why H<sub>2</sub>O is also formed at relatively high density, as shown in Figure 33 above. However, this is of course of lesser interest than CO as valuable product.

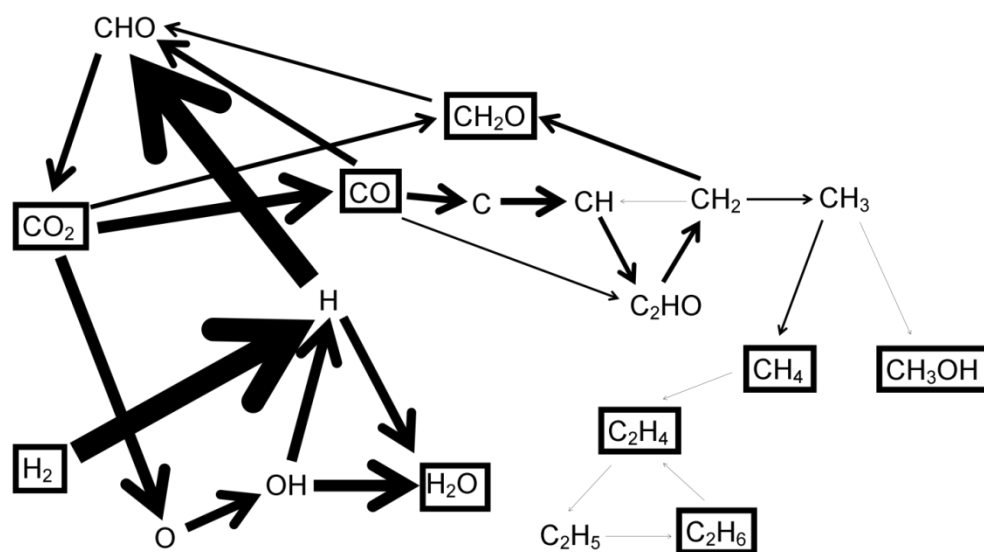
CO will partially react back into CO<sub>2</sub>, mainly through the formation of CHO radicals. Note that in this gas mixture, the major reaction from CO back into CO<sub>2</sub> indeed proceeds through CHO, as the rate of the reaction (CO + H + M → CHO + M) is in the order of 10<sup>17</sup> cm<sup>-3</sup> s<sup>-1</sup>, and the rate of the subsequent formation of CO<sub>2</sub> through the reaction (CHO + O → CO<sub>2</sub> + H) is about 7x10<sup>15</sup> cm<sup>-3</sup> s<sup>-1</sup>, while the rate of the direct reaction (CO + O + M → CO<sub>2</sub> + M) is only in the order of 10<sup>15</sup> cm<sup>-3</sup> s<sup>-1</sup>. The H atoms thus contribute significantly to the back reaction of CO into CO<sub>2</sub>. It is clear from the thick arrow line from H to CHO in Figure 40 that the formation of CHO out of CO and H indeed occurs at a very high rate. The reason why the arrow line from CO to CHO is much thinner is because CHO also reacts back into CO upon collision with H (CHO + H → CO + H<sub>2</sub>), so the net reaction from CO to CHO is smaller than the net reaction from H to CHO. Furthermore, electron impact dissociation of CO

results in the formation of C radicals, which react further into CH, CH<sub>2</sub>, C<sub>2</sub>HO and CH<sub>3</sub> radicals in several successive radical recombination reactions. The formed CH<sub>2</sub> radicals react with CO<sub>2</sub> into the formation of CH<sub>2</sub>O, as was also shown in Figure 38 above. The CH<sub>3</sub> radicals easily form CH<sub>4</sub>, which is much more favored (i.e., the rate is one order of magnitude larger) than the formation of CH<sub>3</sub>OH out of CH<sub>3</sub>. CH<sub>4</sub> partially reacts further into higher hydrocarbons (C<sub>x</sub>H<sub>y</sub>).

From the reaction scheme, it is clear that a lot of subsequent radical reactions are necessary for the formation of (higher) hydrocarbons and oxygenates, such as CH<sub>4</sub>, C<sub>2</sub>H<sub>6</sub>, CH<sub>2</sub>O and CH<sub>3</sub>OH, which explains the very low yields and selectivities of these end products (see Section 6.5.2. above). Indeed, the lack of direct formation of CH<sub>2</sub> and CH<sub>3</sub> in CO<sub>2</sub>/H<sub>2</sub>, which is important in CO<sub>2</sub>/CH<sub>4</sub> gas mixtures (see Section 5.5.), combined with the very low conversion of CO<sub>2</sub>, which is again due to the absence of CH<sub>2</sub> as important collision partner for the loss of CO<sub>2</sub>, makes a CO<sub>2</sub>/H<sub>2</sub> mixture under the present conditions less interesting for the formation of higher hydrocarbons and oxygenates than a CO<sub>2</sub>/CH<sub>4</sub> mixture. This is especially true because H<sub>2</sub> itself is a useful product, while CH<sub>4</sub>, besides being a fuel itself, also greatly contributes to global warming, and thus, the simultaneous conversion of CO<sub>2</sub> and CH<sub>4</sub> will reduce the concentration of two greenhouse gases. Moreover, CO<sub>2</sub>/CH<sub>4</sub> mixtures are available from biomass installations, and their simultaneous conversion can be seen as a direct valorization of biogas, instead of the energy intensive biogas upgrading to a CH<sub>4</sub>-rich gas by removing CO<sub>2</sub>. Another possibly interesting H-source to be added to a CO<sub>2</sub> plasma to produce value-added chemicals, could be water, and the combined CO<sub>2</sub>/H<sub>2</sub>O conversion could even mimic the natural photosynthesis process.

However, recent investigations have illustrated that this gas mixture is also not able to produce oxygenates above the ppm range in a DBD plasma.<sup>225</sup>

Nevertheless, we still believe a CO<sub>2</sub>/H<sub>2</sub> mixture can be of interest for producing CO, to obtain gas mixtures with a specific H<sub>2</sub>/CO ratio. In order to produce specific oxygenated compounds, however, we believe that a catalyst should be added to the plasma.<sup>226</sup> This was also demonstrated by Eliasson et al.<sup>219</sup>, who reported much higher methanol yields in the presence of a catalyst in the plasma, and by Zeng et al.<sup>222</sup>, who found that the combination of a plasma with a catalyst enhances the conversion of CO<sub>2</sub> by 7-36 %, as well as the yield and energy efficient production of CO.



**Figure 40.** Dominant reaction pathways for the conversion of CO<sub>2</sub> and H<sub>2</sub> into various products, in a 50/50 CO<sub>2</sub>/H<sub>2</sub> gas mixture. The thickness of the arrow lines is proportional to the rates of the net reactions. The stable molecules are indicated with black rectangles.

## 6.6. Conclusion

A 1D fluid modeling study for the hydrogenation of CO<sub>2</sub> in a DBD plasma was carried out for different CO<sub>2</sub>/H<sub>2</sub> gas mixing ratios. The densities of the various plasma species as a function of the residence time and the gas mixing ratio were discussed. The spatially averaged densities of the electrons, radicals and ions produced in the plasma exhibit periodic behavior as a function of time, following the period of the sinusoidal applied voltage. The most abundant radicals are H, O, OH, HO<sub>2</sub>, CHO, CH<sub>3</sub> and CH<sub>2</sub>. The densities of the molecules formed during the hydrogenation of CO<sub>2</sub>, i.e., CO, higher order hydrocarbons and oxygenates, exhibit a rising trend as a function of time, because their net production is higher than their net consumption. The most abundant reaction products are CO, H<sub>2</sub>O and CH<sub>4</sub>, and to a lower extent also CH<sub>2</sub>O, C<sub>2</sub>H<sub>6</sub>, O<sub>2</sub> and CH<sub>3</sub>OH. This is in good agreement with reported results from literature for similar CO<sub>2</sub>/H<sub>2</sub> discharges. Altering the inlet gas mixing ratio did not drastically affect the densities of the formed higher hydrocarbons and oxygenates, as the conversion of CO<sub>2</sub> was found to be very low in all gas mixing ratios. We have also presented the calculated conversions of the inlet gases and the maximum yields and corresponding selectivities of the main reaction products. It is clear that the conversion of CO<sub>2</sub> is rather low (i.e., in the order of 2-7 %) in all gas mixtures, and much lower than in a CO<sub>2</sub>/CH<sub>4</sub> mixture, where typical conversions in the order of 3-20 % are obtained at similar conditions. The reason is the abundance of CH<sub>2</sub> radicals in the latter mixture, which significantly contribute to the loss of CO<sub>2</sub>, but their density is very low in the CO<sub>2</sub>/H<sub>2</sub> mixture. The H<sub>2</sub> conversion was calculated to be about 30-60 %, depending on the gas mixing ratio. CO was found to be the only value-added end product with a high selectivity. Finally,

the underlying plasma chemistry governing the conversion of CO<sub>2</sub> and H<sub>2</sub> into the various products was analyzed in detail. The dominant reaction pathways for the consumption of CO<sub>2</sub> and H<sub>2</sub> and the production and loss of some interesting end products, i.e., CO, CH<sub>4</sub>, CH<sub>2</sub>O and CH<sub>3</sub>OH, were discussed. It is clear from our results that a higher conversion of CO<sub>2</sub>, as well as a higher density of CH<sub>3</sub> and CH<sub>2</sub> radicals, would be necessary in order to obtain higher yields of the desired end products. For the conditions under study, only CO is formed at an acceptable level. Thus, it is clear that a CO<sub>2</sub>/H<sub>2</sub> mixture is not very suitable for the production of other value-added chemicals besides CO, and that a CO<sub>2</sub>/CH<sub>4</sub> mixture is more appropriate, because of the presence of CH<sub>2</sub> and CH<sub>3</sub> radicals. The use of a catalyst can possibly increase the formation of some desired oxygenates, as is indeed also shown by Eliasson et al.<sup>219</sup> and Zeng et al.<sup>222</sup>.

# **Chapter 7**

## **General Conclusion and Outlook for the Future**

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## 7.1. General Conclusion

We have studied the plasma chemistry for gas conversion in a DBD plasma, in pure  $\text{CH}_4$ , as well as in  $\text{CH}_4/\text{O}_2$ ,  $\text{CH}_4/\text{CO}_2$  and  $\text{CO}_2/\text{H}_2$  mixtures, which are used for partial oxidation of  $\text{CH}_4$ , dry reforming of  $\text{CH}_4$  and  $\text{CO}_2$  hydrogenation, respectively. More specifically, we have calculated the densities of the various plasma species, created in these gas mixtures, as a function of residence time and gas mixing ratio.  $\text{C}_2\text{H}_6$  and  $\text{H}_2$  are found to be the main reaction products of the conversion of pure  $\text{CH}_4$  into higher hydrocarbons in a DBD reactor. Partial oxidation of  $\text{CH}_4$  favors the formation of  $\text{H}_2\text{O}_2$ ,  $\text{CH}_3\text{OH}$ ,  $\text{C}_2\text{H}_5\text{OH}$ ,  $\text{CH}_3\text{OOH}$  and  $\text{C}_2\text{H}_5\text{OOH}$ , while the densities of  $\text{H}_2$ ,  $\text{CH}_2\text{O}$ ,  $\text{CH}_3\text{CHO}$  and  $\text{CH}_2\text{CO}$  are higher for the dry reforming of  $\text{CH}_4$ .  $\text{CO}$  is formed at high density in both gas mixtures. Note that in the gas mixtures with  $\text{O}_2$  as co-reactant also a significant amount of undesired  $\text{CO}_2$  is formed. The most abundant reaction products for the hydrogenation of  $\text{CO}_2$  in a DBD plasma are  $\text{CO}$ ,  $\text{H}_2\text{O}$  and  $\text{CH}_4$ , and to a lower extent also  $\text{CH}_2\text{O}$ ,  $\text{C}_2\text{H}_6$ ,  $\text{O}_2$  and  $\text{CH}_3\text{OH}$ . It is illustrated that a careful selection of the residence time and gas mixing ratio can entail a higher production of some targeted molecules.

From the calculated densities, the conversions of the inlet gases and the yields and selectivities of the end products as a function of residence time and initial gas mixing ratio can be obtained. The conversion of  $\text{CH}_4$  after 20s is around 20% in all considered mixtures with  $\text{O}_2$ , while in pure  $\text{CH}_4$ , a conversion of 40% was calculated after 20s. A maximum conversion of 68% for  $\text{CH}_4$  and 55% for  $\text{CO}_2$  in  $\text{CH}_4/\text{CO}_2$  is predicted by our calculations. In contrast, the conversion of  $\text{CO}_2$  was found to be very low in  $\text{CO}_2/\text{H}_2$  for all gas mixing ratios (i.e., in the order of 2-7 %). Altering the inlet gas mixing ratio in  $\text{CO}_2/\text{H}_2$  did not drastically affect the densities of the formed higher

hydrocarbons and oxygenates. Therefore, it is clear that a  $\text{CO}_2/\text{H}_2$  mixture is not very suitable for the production of other value-added chemicals besides CO.

The dominant reaction pathways for the consumption of the inlet gases and the production and loss of the dominant end products are also discussed. These results explain in detail why the formation of some molecules is favored in one gas mixture, while other molecules are predominantly formed in another gas mixture. They also point out the reason for the rather low conversion in  $\text{CO}_2/\text{H}_2$  compared to the conversion in  $\text{CH}_4/\text{CO}_2$ , i.e., the lack of  $\text{CH}_2$  radicals in  $\text{CO}_2/\text{H}_2$ . Schematic overviews at the end of each chapter summarize the dominant reaction pathways for the conversion of the inlet gases into various compounds, in the different gas mixtures.

Reasonable agreement between our calculation results and the measurements for pure  $\text{CH}_4$  is established. Furthermore, our results on the partial oxidation and dry reforming of  $\text{CH}_4$  and on the hydrogenation of  $\text{CO}_2$  are in good agreement with reported results from literature for similar  $\text{CH}_4/\text{O}_2$ ,  $\text{CH}_4/\text{CO}_2$  and  $\text{CO}_2/\text{H}_2$  discharges. Moreover, the model can help to obtain more insight into the most suitable feed gas ratio, residence time, co-reactant and other plasma parameters, to obtain the highest yield and/or selectivity of a desired oxygenate.

## 7.2. Outlook for the Future

In this PhD dissertation, we only focused on the conversion, yields and selectivities, but another crucial parameter to determine whether a sustainable competitive industrial process for gas conversion in a DBD can be established, is the energy efficiency of the conversion process. The latter was not studied in the present PhD dissertation, but it is known that a DBD plasma has a rather low energy efficiency for gas conversion, as studied in other PhD dissertations within our group PLASMANT.<sup>109, 181, 197, 227-229</sup> To improve the energy efficiency, a (dielectric) packing can be included in the DBD reactor, enhancing the electric field, and thus the electron temperature, thereby increasing the electron impact reaction rates, yielding a higher conversion for the same input power, and thus a higher energy efficiency. The effect of introducing a dielectric packing in a DBD reactor is currently being investigated by fluid modeling in another PhD dissertation within our group PLASMANT,<sup>212, 230</sup> as well as experimentally,<sup>212</sup> in collaboration with the group LADCA.

Furthermore, a packed bed DBD reactor is also very suitable to introduce a catalyst in the plasma. Our calculation results indicate that the latter will indeed be crucial to improve the selectivities of the desired end products, by acting on one or more of the underlying gas-phase reactions, which will be needed to make this DBD plasma conversion competitive for industrial applications. Plasma catalysis is also being studied within the group PLASMANT, both by computer modeling and experiments, the latter in collaboration with LADCA.

Finally, our specific modeling results on the plasma chemistry can be further improved by including vibrational excitation levels, so that the model can also be applied to other types of plasma reactors, like a microwave or gliding arc discharge (which are known to have a higher energy efficiency, and which are also being studied within our group PLASMANT), or by including other value-added compounds in the model, such as dimethyl ether and formic acid. However, it will be crucial to find reliable data to describe the formation or loss of these species. On the other hand, a reduction of the chemistry set based on a sensitivity analysis is also worth to perform, to be able to simulate the plasma conversion by 2D fluid models, and account for the specific features of a plasma reactor, such as the occurrence of filaments in a DBD.



## Summary

The world primary energy demand is set to grow by one-third to 2040. Globally, fossil fuel resources are still plentiful and will last for decades, but it becomes more difficult to recover them and there can be no guarantee that they will be exploited fast enough to meet the level of demand. The availability of energy resources is, however, of paramount importance to the society. Access to reliable, affordable commercial energy provides the basis for heat, light, mobility, communications and agricultural and industrial capacity in modern society and in this way energy stipulates the degree of civilization. Therefore, socially, environmentally and economically, a growing need is being imposed for a global sustainable energy strategy, based on an improvement of the energy efficiency of the current technologies and a more intensifying diversification of the energy resources, with a huge preference for lower carbon resources. Future energy policy intentions indicate a boost to lower-carbon fuels and technologies worldwide, resulting in an increasing share of non-fossil fuels and natural gas, which is the least-carbon intensive fossil fuel, within the global energy mix up to 2040, while the share of oil and coal is decreasing.

Besides this, climate change due to anthropogenic greenhouse gas emission is a growing concern for the global society. Anthropogenic greenhouse gas emissions have increased since the pre-industrial era and have led to atmospheric concentrations of carbon dioxide (CO<sub>2</sub>), methane (CH<sub>4</sub>) and nitrous oxide (N<sub>2</sub>O) that are unprecedented in at least the last 800,000 years. At the 21st Conference of the Parties to the United Nations Framework Convention on Climate Change (COP21/CMP11; November-December, 2015) a new international agreement, which is strongly endorsed by the chemical

industry, on climate change was made, in order to keep global warming below 2°C.

The conversion of methane, the principal component of natural gas, and carbon dioxide to value-added chemicals and fuels has still a significant growth potential. Currently, both resources are greatly underutilized for the production of chemicals and liquid fuels, mainly because they are very stable molecules. More in particular, the development of a process for the direct synthesis of higher hydrocarbons, syngas and oxygenates, such as methanol and formaldehyde, from methane and/or carbon dioxide in an energy-efficient way would offer significant benefits.

Atmospheric pressure non-thermal plasmas, such as dielectric barrier discharges (DBDs), can offer here a distinct advantage because a DBD has the unique characteristic that it combines an ambient bulk gas temperature and the presence of highly energetic electrons with an electron temperature between 5000 and 20000 K at an electron density of about  $10^{14} \text{ cm}^{-3}$ , and so it enables gas phase reactions at ambient conditions.

A DBD is an electrical discharge that is generated between two electrodes of which at least one is covered with a dielectric material made of glass, quartz, alumina, etc. The gap between the two electrodes is typically a few millimeters. An ac voltage with an amplitude from 1 kV to 100 kV and a frequency of a few Hz to MHz is usually applied to this kind of discharges. Different plasma activation mechanisms will act, causing vibrational and electronic excitation, as well as ionization and dissociation of species, and in this way gas conversion processes are induced.

These processes always involve a huge underlying plasma chemistry and in order to optimize such a process, it is indispensable to get notion of the play of the different species in the immensity of chemical reactions. Fluid modeling can provide here the necessary information to obtain insight in the gas phase chemistry taking place in the discharge gap.

The aim of this dissertation was to describe in detail the plasma chemistry in an atmospheric pressure cylindrical DBD, used as a chemical reactor for gas conversion in different gas mixtures with  $\text{CH}_4$  and/or  $\text{CO}_2$ , by means of a 1D fluid model. The model applied in this study is called Plasimo's MD2D. It is based on the continuity and flux equations for each type of species treated, the electron energy equation and the Poisson equation. This set of coupled partial differential equations is solved by the so-called modified strongly implicit method.

More specifically, the goal was to develop a reliable chemistry set for the description of the gas phase chemistry in pure  $\text{CH}_4$ ,  $\text{CH}_4/\text{O}_2$ ,  $\text{CH}_4/\text{CO}_2$  and  $\text{CO}_2/\text{H}_2$  gas discharges. In order to achieve our goal, we started by developing a 1D fluid model for an atmospheric pressure DBD in pure methane, and extended this model in a later stage to describe the plasma chemistry in the other gas mixtures. A large number of different plasma species (i.e., electrons, molecules, radicals, ions) are included in our model, as well as a comprehensive set of chemical reactions, into which these species participate. For the electron-induced reactions, cross sections as a function of the electron energy were defined as input for the Boltzmann solver BOLSIG+, which provides the energy dependent electron transport coefficients and rate coefficients of the electron reactions, whereas the ion-neutral and neutral-



neutral reactions were characterized by a constant reaction rate coefficient for the working pressure and temperature of 1 atm and 300 K, respectively.

In this way, calculation results could be obtained for the densities of the different plasma species, the conversions of the inlet gases, the yields and selectivities of the end products and the dominant reaction pathways for each of the gas mixtures studied. This allows us to determine whether or not a specific gas mixture is suitable for the production of a specific end-product of interest. Our calculation results were validated with reported results in literature, and for pure  $\text{CH}_4$  also with some experiments for the reactor set-up under study.

In all gas mixtures, the spatially averaged densities of the electrons, ions and radicals exhibit a periodic behavior as a function of time, following the sinusoidal applied voltage, while the spatially averaged molecule densities do not show a periodic behavior. It is illustrated that a careful selection of the residence time and gas mixing ratio can entail a higher production of some targeted molecules.

Higher hydrocarbons ( $\text{C}_2\text{H}_y$  and  $\text{C}_3\text{H}_y$ ) and hydrogen gas are typically found as end products for the conversion of pure  $\text{CH}_4$ . A reasonable agreement between our calculation results and the measurements is established. It is found that electron impact dissociation of  $\text{CH}_4$ , resulting in the formation of the methyl radical ( $\text{CH}_3$ ), initiates the conversion process. Recombination of  $\text{CH}_3$  with either another  $\text{CH}_3$  radical or with a  $\text{C}_2\text{H}_5$  radical will lead to the formation of  $\text{C}_2\text{H}_6$  and  $\text{C}_3\text{H}_8$ . Dissociation of these higher hydrocarbons leads directly to the formation of other hydrocarbons, but also indirectly by the formation of new radicals, which can subsequently also recombine towards these higher order hydrocarbons. In other words, the conversion of  $\text{CH}_4$  is a

play of dissociation and recombination reactions leading to a diverse mixture of higher hydrocarbons.

Dry reforming of  $\text{CH}_4$  in a DBD favors the formation of  $\text{H}_2$ ,  $\text{CH}_2\text{O}$ ,  $\text{CH}_3\text{CHO}$  and  $\text{CH}_2\text{CO}$ , while the densities of  $\text{H}_2\text{O}_2$ ,  $\text{CH}_3\text{OH}$ ,  $\text{C}_2\text{H}_5\text{OH}$ ,  $\text{CH}_3\text{OOH}$  and  $\text{C}_2\text{H}_5\text{OOH}$  are higher for the partial oxidation of  $\text{CH}_4$  in a DBD.  $\text{CO}$  is formed at high density in both gas mixtures, i.e.,  $\text{CH}_4/\text{O}_2$  and  $\text{CH}_4/\text{CO}_2$ . In the gas mixtures with  $\text{O}_2$  as co-reactant, also a significant amount of undesired  $\text{CO}_2$  is formed. Electron impact dissociation of the inlet gases initiates the conversion process. The recombination of  $\text{CH}_3$  radicals again plays a crucial role and it was shown that this recombination leads to the formation of higher hydrocarbons in the mixtures with  $\text{CO}_2$ , while  $\text{CH}_3\text{O}_2$  radicals are favored in the mixtures with  $\text{O}_2$ . In the  $\text{CH}_4/\text{CO}_2$  mixture, also  $\text{CH}_2$  radicals play a role, which can be converted into formaldehyde and  $\text{CO}$  molecules. In the  $\text{CH}_4/\text{O}_2$  mixture, the  $\text{CH}_3\text{O}_2$  radicals lead among others to the formation of methanol, which can react further into formaldehyde and the latter can form  $\text{CO}$ . Our results are in reasonable agreement with reported results from literature for similar  $\text{CH}_4/\text{O}_2$  and  $\text{CH}_4/\text{CO}_2$  discharges. Moreover, our model provides additional information, mainly on the comparison between the formed end products in  $\text{CH}_4/\text{O}_2$  and  $\text{CH}_4/\text{CO}_2$  gas mixtures and on the different pathways leading to these products.

The most abundant reaction products for the hydrogenation of  $\text{CO}_2$  in a DBD are  $\text{CO}$ ,  $\text{H}_2\text{O}$  and  $\text{CH}_4$ , and to a lower extent also  $\text{CH}_2\text{O}$ ,  $\text{C}_2\text{H}_6$ ,  $\text{O}_2$  and  $\text{CH}_3\text{OH}$ . This is in good agreement with reported results from literature for similar  $\text{CO}_2/\text{H}_2$  discharges. Altering the inlet gas mixing ratio did not drastically affect the densities of the formed higher hydrocarbons and oxygenates, as the conversion of  $\text{CO}_2$  was found to be very low (i.e., in the order of 2-7 %) in all

gas mixtures, and much lower than in a  $\text{CO}_2/\text{CH}_4$  mixture, where typical conversions in the order of 3-20 % are obtained at similar conditions. The reason is the abundance of  $\text{CH}_2$  radicals in the latter mixture, which significantly contribute to the loss of  $\text{CO}_2$ , but their density is very low in the  $\text{CO}_2/\text{H}_2$  mixture. It is clear that a  $\text{CO}_2/\text{H}_2$  mixture is not very suitable for the production of other value-added chemicals besides CO, at least in a pure DBD, and that the combination with a catalyst will be needed for the selective production of some value-added compounds, not only in the  $\text{CO}_2/\text{H}_2$  mixture, but in a DBD plasma in general.

## Samenvatting

De wereldwijde vraag naar primaire energie zal naar verwachting met een derde groeien tegen 2040. Hoewel fossiele brandstoffen wereldwijd nog overvloedig aanwezig zijn, wordt het steeds moeilijker om ze te ontginnen en is er geen garantie dat ze snel genoeg gewonnen zullen worden om aan de vraag naar energie tegemoet te komen. De beschikbaarheid van energiebronnen is echter van het grootste belang voor onze maatschappij. De toegang tot betrouwbare, betaalbare commerciële energie vormt de basis voor warmte, licht, mobiliteit, communicatie en agrarische en industriële capaciteit in een moderne maatschappij, en op deze manier bepaalt energie de ontwikkelingsgraad van een maatschappij. Daarom is er vanuit sociaal, ecologisch en economisch oogpunt een groeiende behoefte aan een wereldwijde strategie voor duurzame energie, door middel van een verbetering van de energie-efficiëntie van de huidige technologieën en een toenemende verscheidenheid aan energiebronnen, met een grote voorkeur voor energiebronnen met een lager koolstofgehalte. Beleidsintenties inzake energie wijzen op een algemene verschuiving naar brandstoffen en technologieën met een lager koolstofgehalte. Dit leidt ertoe dat het aandeel aan niet-fossiele brandstoffen en aardgas, de minst koolstofintensieve fossiele brandstof, binnen de wereldwijde energiemix zal blijven groeien in de komende decennia, terwijl olie en steenkool minder belangrijk worden.

Daarnaast is er de toenemende bezorgdheid over de gevolgen van de klimaatverandering voor de samenleving. De antropogene uitstoot van broeikasgassen, welke aan de basis ligt van de klimaatverandering, is gestegen sinds het pre-industriële tijdperk. Daardoor is de atmosferische concentratie van koolstofdioxide (CO<sub>2</sub>), methaan (CH<sub>4</sub>) en lachgas (N<sub>2</sub>O) toegenomen tot

waarden die ongezien zijn in de laatste 800.000 jaar. Tijdens de 21<sup>ste</sup> Conferentie van Partijen over het Klimaatverdrag (COP21/CMP11, november-december 2015) werd een nieuwe internationale overeenkomst gemaakt over klimaatverandering, welke wordt onderschreven door de chemische industrie. Er werd hierbij afgesproken om de opwarming van de aarde onder de 2 °C te houden.

De omzetting van methaan, het hoofdbestanddeel van aardgas, en koolstofdioxide in chemicaliën en brandstoffen met toegevoegde waarde heeft nog steeds een aanzienlijk groeipotentieel. Momenteel worden beide grondstoffen sterk onderbenut voor de productie van chemicaliën en vloeibare brandstoffen, vooral omdat het beiden zeer stabiele moleculen zijn. Vooral de ontwikkeling van een energie-efficiënt en duurzaam proces voor de directe vorming van hogere koolwaterstoffen, syngas en zuurstofhoudende verbindingen, zoals methanol en formaldehyde uit methaan en/of koolstofdioxide zou perspectieven bieden.

Atmosferische niet-thermische plasma's, zoals diëlektrische barrière ontladingen (DBDs), kunnen hier een duidelijk voordeel bieden, daar in een DBD de temperatuur van het bulkgas relatief laag blijft (tussen kamertemperatuur en 200 °C) terwijl elektronen gevormd worden, die zeer energetisch zijn en een temperatuur hebben variërend tussen 5000 en 20.000 K, bij een elektronendichtheid van circa  $10^{14} \text{ cm}^{-3}$ . Dit maakt reacties mogelijk die thermodynamisch niet zouden kunnen optreden bij deze lage gastemperaturen. Als dusdanig kunnen plasmaprocessen de nadelen van de hoge temperatuur, die vereist is bij conventionele katalytische processen, vermijden.

Een DBD is een elektrische ontleding die wordt gegenereerd tussen twee elektroden waarvan er ten minste één is bedekt met een diëlektricum, gemaakt van bv. glas, kwarts, aluminiumoxide, enz. De afstand tussen de twee elektroden is typisch enkele millimeters. Doorgaans wordt een wisselspanning met een amplitude van 1 kV tot 100 kV en een frequentie van enkele Hz tot MHz over de elektroden aangelegd, waarna in de ontladingsruimte een plasma gecreëerd zal worden. Verschillende plasma-activatiemechanismen treden op en dit leidt tot vibrationele en elektronische excitatie, ionisatie en dissociatie van de gasdeeltjes en dusdanig tot gasconversie.

Een waaier aan deeltjes en reacties is betrokken in deze gasconversie processen. Het is dan ook cruciaal om een inzicht te krijgen in deze onderliggende plasmachemie, indien men dergelijk proces wenst te optimaliseren. Fluid modellering kan hier de nodige informatie aanreiken om een inzicht te krijgen in de gasfase chemie in zulk een DBD.

Het opzet van dit doctoraat was om in detail de plasmachemie in een cilindrische DBD bij atmosferedruk, gebruikt als een chemische reactor voor gasconversie, te beschrijven aan de hand van een 1D fluid model, voor verschillende gasmengsels met CH<sub>4</sub> en/of CO<sub>2</sub>. Het model dat gebruikt werd in dit onderzoek is Plasimo's MD2D. Een fluid model is gebaseerd op de snelheidsmomenten van de Boltzmann transportvergelijking. De nulde, eerste en tweede momenten van deze vergelijking geven namelijk de behoudsvergelijkingen van respectievelijk deeltjesdichtheid, hoeveelheid van beweging en energiedichtheid. De behoudsvergelijking voor hoeveelheid van beweging wordt hier echter benaderd door de eenvoudigere drift-diffusie vergelijking. De behoudsvergelijking van deeltjesdichtheid en de drift-diffusie vergelijking worden opgesteld voor elke deeltjessoort, terwijl de

energiebalansvergelijking enkel opgesteld wordt voor de elektronen. Deze vergelijkingen worden ten slotte gekoppeld aan de Poisson vergelijking om de elektrische potentiaalverdeling zelfconsistent te kunnen berekenen uit de dichtheden van elektronen en ionen. Aangezien deze set van vergelijkingen sterk gekoppeld is, moeten deze vergelijkingen ook simultaan worden opgelost.

Meer bepaald was het het doel om een betrouwbare chemieset op te stellen voor de beschrijving van de gasfase chemie in zuiver  $\text{CH}_4$ ,  $\text{CH}_4/\text{O}_2$ ,  $\text{CH}_4/\text{CO}_2$  en  $\text{CO}_2/\text{H}_2$  gasontladingen. Om ons doel te bereiken, zijn we begonnen met het ontwikkelen van een 1D fluid model voor een DBD bij atmosferedruk in zuiver methaan. In een volgende stap hebben we dit model dan uitgebreid om de plasmachemie in de andere gasmengsels te kunnen beschrijven.

Zulk een reactieset bestaat uit een groot aantal verschillende soorten plasmadeeltjes (elektronen, moleculen, radicalen, ionen) en hun bijhorende reacties. Voor de deeltjes dienen diffusiecoëfficiënten, mobiliteitscoëfficiënten, stickingcoëfficiënten en secundaire elektronen emissiecoëfficiënten gedefinieerd te worden in het model. Voor de reacties met elektronen werden cross secties als functie van de elektronenenergie gedefinieerd als input voor de Boltzmann solver BOLSIG+, die energieafhankelijke elektron transport- en snelheidscoëfficiënten van de elektronreacties bepaalt. De reacties tussen neutrale deeltjes en tussen neutrale deeltjes en ionen werden gedefinieerd met een constante reactiesnelheidscoëfficiënt voor 1 atmosfeer en 300 K.

Op deze manier konden de dichtheden van de verschillende plasmadeeltjes, de omzettingen van de inlaatgassen, de rendementen en de selectiviteiten

van de eindproducten en de belangrijkste reactiepaden berekend worden voor elk van de in dit onderzoek beschouwde gasmengsels. Daardoor konden we bepalen of een bepaald gasmengsel geschikt is voor de productie van een specifiek beoogd eindproduct. Onze resultaten werden gevalideerd aan de hand van gerapporteerde waarden in de literatuur voor gelijkaardige ontladingen, alsook aan de hand van experimenten uitgevoerd in de plasmareactor beschouwd in dit onderzoek, in het geval van zuiver  $\text{CH}_4$ .

De ruimtelijk gemiddelde dichtheden van de elektronen, ionen en radicalen vertonen in elk van de gasmengsels periodisch gedrag in functie van de tijd. Dit is in tegenstelling tot de ruimtelijk gemiddelde dichtheden van de moleculen, welke een dalende of stijgende trend vertonen. Een zorgvuldige keuze van de verblijftijd en de gassamenstelling kan leiden tot een hogere productie van bepaalde gewenste eindproducten.

Hogere koolwaterstoffen ( $\text{C}_2\text{H}_y$  en  $\text{C}_3\text{H}_y$ ) en waterstofgas zijn de belangrijkste eindproducten voor de conversie van zuiver  $\text{CH}_4$ . Een redelijke overeenkomst tussen onze berekeningen en de metingen werd verkregen. Het blijkt verder dat botsingen van elektronen met  $\text{CH}_4$  leiden tot de dissociatie van  $\text{CH}_4$  in methylradicalen ( $\text{CH}_3$ ) welke het gasconversie proces zullen initiëren. Recombinatie van  $\text{CH}_3$  met een ander  $\text{CH}_3$  radicaal of een  $\text{C}_2\text{H}_5$  radicaal leidt tot de vorming van  $\text{C}_2\text{H}_6$  en  $\text{C}_3\text{H}_8$ . Dissociatie van deze hogere koolwaterstoffen leidt direct en indirect (via nieuwe recombiniatiereacties) tot de vorming van andere koolwaterstoffen. De omzetting van  $\text{CH}_4$  is met andere woorden een spel van dissociatie- en recombiniatiereacties, die leiden tot een divers mengsel van hogere koolwaterstoffen.

‘Dry reforming’ van  $\text{CH}_4$  in een DBD leidt tot de vorming van  $\text{H}_2$ ,  $\text{CH}_2\text{O}$ ,  $\text{CH}_3\text{CHO}$  en  $\text{CH}_2\text{CO}$ , terwijl partiële oxidatie van  $\text{CH}_4$  resulteert in de vorming



van  $\text{H}_2\text{O}_2$ ,  $\text{CH}_3\text{OH}$ ,  $\text{C}_2\text{H}_5\text{OH}$ ,  $\text{CH}_3\text{OOH}$  en  $\text{C}_2\text{H}_5\text{OOH}$ . De dichtheid van CO is hoog in zowel  $\text{CH}_4/\text{O}_2$  als  $\text{CH}_4/\text{CO}_2$ . In de gasmengsels met  $\text{O}_2$  als co-reactant wordt ook een aanzienlijke hoeveelheid ongewenst  $\text{CO}_2$  gevormd. Elektron impact dissociatie van de gasmoleculen initieert het conversieproces. De recombinatie van  $\text{CH}_3$  radicalen speelt wederom een cruciale rol. Er werd aangetoond dat deze recombinatie leidt tot de vorming van hogere koolwaterstoffen in het mengsel met  $\text{CO}_2$ , terwijl  $\text{CH}_3\text{O}_2$  radicalen bij voorkeur gevormd worden in de mengsels met  $\text{O}_2$ . In de  $\text{CH}_4/\text{CO}_2$  gasmengsels spelen ook de  $\text{CH}_2$  radicalen een belangrijke rol, waarbij er via botsingen met  $\text{CO}_2$  formaldehyde en CO gevormd worden. De  $\text{CH}_3\text{O}_2$  radicalen in de  $\text{CH}_4/\text{O}_2$  gasmengsels leiden onder andere tot de vorming van methanol, dat verder kan reageren tot formaldehyde en dit kan dan weer verder reageren tot CO. Er is een redelijke overeenstemming tussen onze resultaten en gerapporteerde resultaten uit de literatuur voor soortgelijke  $\text{CH}_4/\text{O}_2$  en  $\text{CH}_4/\text{CO}_2$  ontladingen. Bovendien levert ons model extra informatie, voornamelijk wat betreft de vergelijking van de gevormde eindproducten tussen  $\text{CH}_4/\text{O}_2$  en  $\text{CH}_4/\text{CO}_2$  gas gasmengsels en de verschillende reactiepaden verantwoordelijk voor de vorming van deze producten.

De belangrijkste reactieproducten voor de hydrogenatie van  $\text{CO}_2$  in een DBD zijn CO,  $\text{H}_2\text{O}$  en  $\text{CH}_4$ , en in mindere mate ook  $\text{CH}_2\text{O}$ ,  $\text{C}_2\text{H}_6$ ,  $\text{O}_2$  en  $\text{CH}_3\text{OH}$ . Dit komt goed overeen met de gerapporteerde resultaten uit de literatuur voor soortgelijke  $\text{CO}_2/\text{H}_2$  ontladingen. Het veranderen van de initiële gasverhouding heeft geen grote invloed op de dichtheid van de gevormde hogere koolwaterstoffen en zuurstofhoudende verbindingen, daar de omzetting van  $\text{CO}_2$  zeer laag bleek (in de orde van 2-7%) in alle gasmengsels, en dus veel lager is dan deze in een  $\text{CO}_2/\text{CH}_4$  mengsel, waarbij omzettingen in

de orde van 3-20% worden verkregen bij soortgelijke omstandigheden. De reden is de grotere aanwezigheid van  $\text{CH}_2$  radicalen in het  $\text{CO}_2/\text{CH}_4$  gasmengsel, die aanzienlijk bijdragen tot de afbraak van  $\text{CO}_2$ . Het is duidelijk dat een  $\text{CO}_2/\text{H}_2$  mengsel niet erg geschikt is voor de productie van andere chemicaliën met toegevoegde waarde behalve dan  $\text{CO}$ , tenminste voor een DBD plasma, en dat de combinatie met een katalysator nodig zal zijn voor de selectieve productie van specifieke waardevolle componenten, niet enkel in het  $\text{CO}_2/\text{H}_2$  mengsel, maar ook meer algemeen in een DBD plasma.



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## Appendices - Overview of the Reactions in the Model

Note: This set is applicable for the CH<sub>4</sub>/CO<sub>2</sub>, CH<sub>4</sub>/O<sub>2</sub> and CO<sub>2</sub>/H<sub>2</sub> mixtures, as well as for pure CH<sub>4</sub>, where of course only the reactions with CH<sub>4</sub> and CH<sub>x</sub> species are included. The reactions included in the model for pure CH<sub>4</sub> are indicated with a gray shadow.

**Table A.1.** Electron impact reactions with the various molecules and radicals, included in the model. These reactions are treated by energy-dependent cross sections (or rate coefficients), and the references where these cross sections (or rate coefficients) were adopted from, are also included. For the vibrational and electronic excitations, several individual excitations are included, as indicated by the number between brackets.

CH <sub>4</sub>					
Momentum Transfer	e <sup>-</sup> + CH <sub>4</sub>	→	e <sup>-</sup> + CH <sub>4</sub>		231
Vibrational Excitation	e <sup>-</sup> + CH <sub>4</sub>	→	e <sup>-</sup> + CH <sub>4</sub> <sup>*</sup>	(2)	231
Ionization	e <sup>-</sup> + CH <sub>4</sub>	→	2e <sup>-</sup> + CH <sub>4</sub> <sup>+</sup>		232
Dissociative Ionization	e <sup>-</sup> + CH <sub>4</sub>	→	2e <sup>-</sup> + CH <sub>3</sub> <sup>+</sup> + H		232
	e <sup>-</sup> + CH <sub>4</sub>	→	2e <sup>-</sup> + CH <sub>2</sub> <sup>+</sup> + H <sub>2</sub>		232
Dissociation	e <sup>-</sup> + CH <sub>4</sub>	→	e <sup>-</sup> + CH <sub>3</sub> + H		233-234
	e <sup>-</sup> + CH <sub>4</sub>	→	e <sup>-</sup> + CH <sub>2</sub> + H <sub>2</sub>		233-234
	e <sup>-</sup> + CH <sub>4</sub>	→	e <sup>-</sup> + CH + H <sub>2</sub> + H		233-234
	e <sup>-</sup> + CH <sub>4</sub>	→	e <sup>-</sup> + C + 2H <sub>2</sub>		233-234
CH <sub>3</sub>					
Ionization	e <sup>-</sup> + CH <sub>3</sub>	→	2e <sup>-</sup> + CH <sub>3</sub> <sup>+</sup>		232



Appendices Table A.1.

Dissociative Ionization	$e^- + CH_3$	$\rightarrow 2e^- + CH_2^+ + H$	232
	$e^- + CH_3$	$\rightarrow 2e^- + CH^+ + H_2$	232
Dissociation	$e^- + CH_3$	$\rightarrow e^- + CH_2 + H$	233-234
	$e^- + CH_3$	$\rightarrow e^- + CH + H_2$	233-234
CH <sub>2</sub>			
Ionization	$e^- + CH_2$	$\rightarrow 2e^- + CH_2^+$	232
Dissociative Ionization	$e^- + CH_2$	$\rightarrow 2e^- + CH^+ + H$	232
	$e^- + CH_2$	$\rightarrow 2e^- + C^+ + H_2$	232
Dissociation	$e^- + CH_2$	$\rightarrow e^- + CH + H$	233-234
CH			
Ionization	$e^- + CH$	$\rightarrow 2e^- + CH^+$	232
Dissociative Ionization	$e^- + CH$	$\rightarrow 2e^- + C^+ + H$	232
Dissociation	$e^- + CH$	$\rightarrow e^- + C + H$	233-234
C			
Ionization	$e^- + C$	$\rightarrow 2e^- + C^+$	233-234
C <sub>2</sub> H <sub>6</sub>			
Momentum Transfer	$e^- + C_2H_6$	$\rightarrow e^- + C_2H_6$	231
Vibrational Excitation	$e^- + C_2H_6$	$\rightarrow e^- + C_2H_6^*$	(3) 231
Ionization	$e^- + C_2H_6$	$\rightarrow 2e^- + C_2H_6^+$	232
Dissociative Ionization	$e^- + C_2H_6$	$\rightarrow 2e^- + C_2H_5^+ + H$	232
	$e^- + C_2H_6$	$\rightarrow 2e^- + C_2H_4^+ + H_2$	232
	$e^- + C_2H_6$	$\rightarrow 2e^- + C_2H_3^+ + H_2 + H$	232
	$e^- + C_2H_6$	$\rightarrow 2e^- + C_2H_2^+ + 2H_2$	232

	$e^- + C_2H_6$	$\rightarrow 2e^- + CH_3^+ + CH_3$	232
Dissociation	$e^- + C_2H_6$	$\rightarrow e^- + C_2H_5 + H$	235-236
	$e^- + C_2H_6$	$\rightarrow e^- + C_2H_4 + H_2$	235-236
$C_2H_5$			
Ionization	$e^- + C_2H_5$	$\rightarrow 2e^- + C_2H_5^+$	232
Dissociative Ionization	$e^- + C_2H_5$	$\rightarrow 2e^- + C_2H_4^+ + H$	232
	$e^- + C_2H_5$	$\rightarrow 2e^- + C_2H_3^+ + H_2$	232
	$e^- + C_2H_5$	$\rightarrow 2e^- + C_2H_2^+ + H_2 + H$	232
Dissociation	$e^- + C_2H_5$	$\rightarrow e^- + C_2H_4 + H$	235-236
	$e^- + C_2H_5$	$\rightarrow e^- + C_2H_3 + H_2$	235-236
$C_2H_4$			
Momentum Transfer	$e^- + C_2H_4$	$\rightarrow e^- + C_2H_4$	231
Vibrational Excitation	$e^- + C_2H_4$	$\rightarrow e^- + C_2H_4^*$	(2) 231
Ionization	$e^- + C_2H_4$	$\rightarrow 2e^- + C_2H_4^+$	232
Dissociative Ionization	$e^- + C_2H_4$	$\rightarrow 2e^- + C_2H_3^+ + H$	232
	$e^- + C_2H_4$	$\rightarrow 2e^- + C_2H_2^+ + H_2$	232
Dissociation	$e^- + C_2H_4$	$\rightarrow e^- + C_2H_3 + H$	235-236
	$e^- + C_2H_4$	$\rightarrow e^- + C_2H_2 + H_2$	235-236
$C_2H_3$			
Ionization	$e^- + C_2H_3$	$\rightarrow 2e^- + C_2H_3^+$	232
Dissociative Ionization	$e^- + C_2H_3$	$\rightarrow 2e^- + C_2H_2^+ + H$	232
	$e^- + C_2H_3$	$\rightarrow 2e^- + C_2H^+ + H_2$	232
Dissociation	$e^- + C_2H_3$	$\rightarrow e^- + C_2H_2 + H$	235-236

Appendices Table A.1.

	$e^- + C_2H_3$	$\rightarrow e^- + C_2H + H_2$	235-236
$C_2H_2$			
Momentum Transfer	$e^- + C_2H_2$	$\rightarrow e^- + C_2H_2$	231
Vibrational Excitation	$e^- + C_2H_2$	$\rightarrow e^- + C_2H_2^*$	(3) 231
Ionization	$e^- + C_2H_2$	$\rightarrow 2e^- + C_2H_2^+$	232
Dissociation	$e^- + C_2H_2$	$\rightarrow e^- + C_2H + H$	235-236
	$e^- + C_2H_2$	$\rightarrow e^- + C_2 + H_2$	235-236
$C_2H$			
Ionization	$e^- + C_2H$	$\rightarrow 2e^- + C_2H^+$	232
Dissociation	$e^- + C_2H$	$\rightarrow e^- + C_2 + H$	235-236
	$e^- + C_2H$	$\rightarrow e^- + C + CH$	235-236
$C_2$			
Ionization	$e^- + C_2$	$\rightarrow 2e^- + C_2^+$	235-236
Dissociation	$e^- + C_2$	$\rightarrow e^- + C + C$	235-236
$C_3H_8$			
Momentum Transfer	$e^- + C_3H_8$	$\rightarrow e^- + C_3H_8$	231
Vibrational Excitation	$e^- + C_3H_8$	$\rightarrow e^- + C_3H_8^*$	(2) 231
Dissociative Ionization	$e^- + C_3H_8$	$\rightarrow 2e^- + C_2H_5^+ + CH_3$	232
	$e^- + C_3H_8$	$\rightarrow 2e^- + C_2H_4^+ + CH_4$	232
Dissociation	$e^- + C_3H_8$	$\rightarrow e^- + C_3H_7 + H$	235-236
	$e^- + C_3H_8$	$\rightarrow e^- + C_3H_6 + H_2$	235-236
	$e^- + C_3H_8$	$\rightarrow e^- + C_2H_4 + CH_4$	235-236

C <sub>3</sub> H <sub>7</sub>						
Dissociative Ionization	e <sup>-</sup>	+	C <sub>3</sub> H <sub>7</sub>	→	2e <sup>-</sup> + C <sub>2</sub> H <sub>5</sub> <sup>+</sup> + CH <sub>2</sub>	235-236
	e <sup>-</sup>	+	C <sub>3</sub> H <sub>7</sub>	→	2e <sup>-</sup> + C <sub>2</sub> H <sub>4</sub> <sup>+</sup> + CH <sub>3</sub>	235-236
	e <sup>-</sup>	+	C <sub>3</sub> H <sub>7</sub>	→	2e <sup>-</sup> + C <sub>2</sub> H <sub>3</sub> <sup>+</sup> + CH <sub>4</sub>	235-236
	e <sup>-</sup>	+	C <sub>3</sub> H <sub>7</sub>	→	2e <sup>-</sup> + CH <sub>3</sub> <sup>+</sup> + C <sub>2</sub> H <sub>4</sub>	235-236
Dissociation	e <sup>-</sup>	+	C <sub>3</sub> H <sub>7</sub>	→	e <sup>-</sup> + C <sub>3</sub> H <sub>6</sub> + H	235-236
	e <sup>-</sup>	+	C <sub>3</sub> H <sub>7</sub>	→	e <sup>-</sup> + C <sub>3</sub> H <sub>5</sub> + H <sub>2</sub>	235-236
	e <sup>-</sup>	+	C <sub>3</sub> H <sub>7</sub>	→	e <sup>-</sup> + C <sub>2</sub> H <sub>4</sub> + CH <sub>3</sub>	235-236
	e <sup>-</sup>	+	C <sub>3</sub> H <sub>7</sub>	→	e <sup>-</sup> + C <sub>2</sub> H <sub>3</sub> + CH <sub>4</sub>	235-236
C <sub>3</sub> H <sub>6</sub>						
Dissociative Ionization	e <sup>-</sup>	+	C <sub>3</sub> H <sub>6</sub>	→	2e <sup>-</sup> + C <sub>2</sub> H <sub>5</sub> <sup>+</sup> + CH	235-236
	e <sup>-</sup>	+	C <sub>3</sub> H <sub>6</sub>	→	2e <sup>-</sup> + C <sub>2</sub> H <sub>4</sub> <sup>+</sup> + CH <sub>2</sub>	235-236
	e <sup>-</sup>	+	C <sub>3</sub> H <sub>6</sub>	→	2e <sup>-</sup> + C <sub>2</sub> H <sub>3</sub> <sup>+</sup> + CH <sub>3</sub>	235-236
	e <sup>-</sup>	+	C <sub>3</sub> H <sub>6</sub>	→	2e <sup>-</sup> + C <sub>2</sub> H <sub>2</sub> <sup>+</sup> + CH <sub>4</sub>	235-236
	e <sup>-</sup>	+	C <sub>3</sub> H <sub>6</sub>	→	2e <sup>-</sup> + CH <sub>3</sub> <sup>+</sup> + C <sub>2</sub> H <sub>3</sub>	235-236
Dissociation	e <sup>-</sup>	+	C <sub>3</sub> H <sub>6</sub>	→	e <sup>-</sup> + C <sub>3</sub> H <sub>5</sub> + H	235-236
	e <sup>-</sup>	+	C <sub>3</sub> H <sub>6</sub>	→	e <sup>-</sup> + C <sub>2</sub> H <sub>2</sub> + CH <sub>4</sub>	235-236
C <sub>3</sub> H <sub>5</sub>						
Dissociative Ionization	e <sup>-</sup>	+	C <sub>3</sub> H <sub>5</sub>	→	2e <sup>-</sup> + C <sub>2</sub> H <sub>3</sub> <sup>+</sup> + CH <sub>2</sub>	235-236
	e <sup>-</sup>	+	C <sub>3</sub> H <sub>5</sub>	→	2e <sup>-</sup> + C <sub>2</sub> H <sub>2</sub> <sup>+</sup> + CH <sub>3</sub>	235-236
	e <sup>-</sup>	+	C <sub>3</sub> H <sub>5</sub>	→	2e <sup>-</sup> + CH <sub>3</sub> <sup>+</sup> + C <sub>2</sub> H <sub>2</sub>	235-236
Dissociation	e <sup>-</sup>	+	C <sub>3</sub> H <sub>5</sub>	→	e <sup>-</sup> + C <sub>2</sub> H <sub>2</sub> + CH <sub>3</sub>	235-236
H <sub>2</sub>						
Momentum Transfer	e <sup>-</sup>	+	H <sub>2</sub>	→	e <sup>-</sup> + H <sub>2</sub>	237

Appendices Table A.1.

Vibrational Excitation	$e^- + H_2$	$\rightarrow e^- + H_2^*$	(3)	238
Ionization	$e^- + H_2$	$\rightarrow 2e^- + H_2^+$		239
Dissociation	$e^- + H_2$	$\rightarrow e^- + 2H$		240
H				
Ionization	$e^- + H$	$\rightarrow 2e^- + H^+$		239
O <sub>2</sub>				
Momentum Transfer	$e^- + O_2$	$\rightarrow e^- + O_2$		195
Vibrational Excitation	$e^- + O_2$	$\rightarrow e^- + O_2^*$	(4)	195
Electronic Excitation	$e^- + O_2$	$\rightarrow e^- + O_2^*$	(4)	194-195
Ionization	$e^- + O_2$	$\rightarrow 2e^- + O_2^+$		194
Dissociative Ionization	$e^- + O_2$	$\rightarrow 2e^- + O^+ + O$		195
Attachment	$e^- + O_2 + O_2$	$\rightarrow O_2^- + O_2$	Energy dependent rate coefficient	241
Dissociative Attachment	$e^- + O_2$	$\rightarrow O^- + O$		195
Ion-pair formation	$e^- + O_2$	$\rightarrow e^- + O^+ + O^-$	Energy dependent rate coefficient	242
Dissociation	$e^- + O_2$	$\rightarrow e^- + 2O$	(2)	195
O				
Momentum Transfer	$e^- + O$	$\rightarrow e^- + O$		243
Electronic Excitation	$e^- + O$	$\rightarrow e^- + O^*$	(2)	244

Appendices Table A.1.

Ionization	$e^- + O \rightarrow 2e^- + O^+$		244
Attachment	$e^- + O + O_2 \rightarrow O^- + O_2$	$1.00 \times 10^{-31} \text{ cm}^6 \text{ s}^{-1}$	195
<hr/> O <sub>3</sub> <hr/>			
Dissociative Ionization	$e^- + O_3 \rightarrow 2e^- + O_2^+ + O$		195
Attachment	$e^- + O_3 + O_2 \rightarrow O_3^- + O_2$	Energy dependent rate coefficient	241
Dissociative Attachment	$e^- + O_3 \rightarrow O^- + O_2$		245
	$e^- + O_3 \rightarrow O_2^- + O$		245
Ion-pair formation	$e^- + O_3 \rightarrow e^- + O^- + O^+ + O$		195
Dissociation	$e^- + O_3 \rightarrow e^- + O_2 + O$	Energy dependent rate coefficient	195
<hr/> CO <sub>2</sub> <hr/>			
Momentum Transfer	$e^- + CO_2 \rightarrow e^- + CO_2$		196
Vibrational Excitation	$e^- + CO_2 \rightarrow e^- + CO_2^*$	(3)	196
Electronic Excitation	$e^- + CO_2 \rightarrow e^- + CO_2^*$	(2)	246-247
Ionization	$e^- + CO_2 \rightarrow 2e^- + CO_2^+$		196
Dissociative Attachment	$e^- + CO_2 \rightarrow O^- + CO$		196
Dissociation	$e^- + CO_2 \rightarrow e^- + CO + O$		196

Appendices Table A.1.

CO						
Momentum Transfer	$e^-$	+	CO	$\rightarrow$	$e^-$	+ CO 238
Vibrational Excitation	$e^-$	+	CO	$\rightarrow$	$e^-$	+ CO* (1) 238
Electronic Excitation	$e^-$	+	CO	$\rightarrow$	$e^-$	+ CO* (5) 246-247
Ionization	$e^-$	+	CO	$\rightarrow$	$2e^-$	+ CO* 248
Dissociative Attachment	$e^-$	+	CO	$\rightarrow$	O $^-$	+ C 249
Dissociation	$e^-$	+	CO	$\rightarrow$	$e^-$	+ C + O 248
H <sub>2</sub> O						
Momentum Transfer	$e^-$	+	H <sub>2</sub> O	$\rightarrow$	$e^-$	+ H <sub>2</sub> O 250
Vibrational Excitation	$e^-$	+	H <sub>2</sub> O	$\rightarrow$	$e^-$	+ H <sub>2</sub> O* (2) 250
Ionization	$e^-$	+	H <sub>2</sub> O	$\rightarrow$	$2e^-$	+ H <sub>2</sub> O $^+$ 250
Dissociative Attachment	$e^-$	+	H <sub>2</sub> O	$\rightarrow$	H $^-$	+ OH 250
	$e^-$	+	H <sub>2</sub> O	$\rightarrow$	O $^-$	+ H <sub>2</sub> 250
	$e^-$	+	H <sub>2</sub> O	$\rightarrow$	OH $^-$	+ H 250
Dissociation	$e^-$	+	H <sub>2</sub> O	$\rightarrow$	$e^-$	+ OH + H 250
	$e^-$	+	H <sub>2</sub> O	$\rightarrow$	$e^-$	+ O + H <sub>2</sub> 250
OH						
Ionization	$e^-$	+	OH	$\rightarrow$	$2e^-$	+ OH $^+$ Energy dependent rate coefficient 251
Dissociation	$e^-$	+	OH	$\rightarrow$	$e^-$	+ O + H Energy dependent rate coefficient 251

**Table A.2.** Electron-ion recombination reactions included in the model. These reactions are treated by energy-dependent rate coefficients, and the references where these rate coefficients were adopted from, are also included.

$e^-$	+	$CH_5^+$	$\rightarrow$	$CH_3$	+	$2H$	233, 252
$e^-$	+	$CH_5^+$	$\rightarrow$	$CH_2$	+	$H_2 + H$	233, 252
$e^-$	+	$CH_4^+$	$\rightarrow$	$CH_3$	+	$H$	233, 252
$e^-$	+	$CH_4^+$	$\rightarrow$	$CH_2$	+	$2H$	233, 252
$e^-$	+	$CH_4^+$	$\rightarrow$	$CH$	+	$H_2 + H$	233, 252
$e^-$	+	$CH_3^+$	$\rightarrow$	$CH_2$	+	$H$	233, 252
$e^-$	+	$CH_3^+$	$\rightarrow$	$CH$	+	$H_2$	233, 252
$e^-$	+	$CH_3^+$	$\rightarrow$	$CH$	+	$2H$	233, 252
$e^-$	+	$CH_3^+$	$\rightarrow$	$C$	+	$H_2 + H$	233, 252
$e^-$	+	$CH_2^+$	$\rightarrow$	$CH$	+	$H$	233, 252
$e^-$	+	$CH_2^+$	$\rightarrow$	$C$	+	$H_2$	233, 252
$e^-$	+	$CH_2^+$	$\rightarrow$	$C$	+	$2H$	233, 252
$e^-$	+	$CH^+$	$\rightarrow$	$C$	+	$H$	233, 252
$e^-$	+	$C_2H_6^+$	$\rightarrow$	$C_2H_5$	+	$H$	236
$e^-$	+	$C_2H_6^+$	$\rightarrow$	$C_2H_4$	+	$2H$	236
$e^-$	+	$C_2H_5^+$	$\rightarrow$	$C_2H_4$	+	$H$	236
$e^-$	+	$C_2H_5^+$	$\rightarrow$	$C_2H_3$	+	$2H$	236
$e^-$	+	$C_2H_5^+$	$\rightarrow$	$C_2H_2$	+	$H_2 + H$	236
$e^-$	+	$C_2H_5^+$	$\rightarrow$	$C_2H_2$	+	$3H$	236
$e^-$	+	$C_2H_5^+$	$\rightarrow$	$CH_3$	+	$CH_2$	236
$e^-$	+	$C_2H_4^+$	$\rightarrow$	$C_2H_3$	+	$H$	236
$e^-$	+	$C_2H_4^+$	$\rightarrow$	$C_2H_2$	+	$2H$	236



Appendices Table A.2.

$e^-$	+	$C_2H_4^+$	$\rightarrow$	$C_2H$	+	$H_2$	+	$H$	236
$e^-$	+	$C_2H_3^+$	$\rightarrow$	$C_2H_2$	+	$H$			236
$e^-$	+	$C_2H_3^+$	$\rightarrow$	$C_2H$	+	$2H$			236
$e^-$	+	$C_2H_2^+$	$\rightarrow$	$C_2H$	+	$H$			236
$e^-$	+	$C_2H_2^+$	$\rightarrow$	$C_2$	+	$2H$			236
$e^-$	+	$C_2H_2^+$	$\rightarrow$	$2CH$					236
$e^-$	+	$C_2H^+$	$\rightarrow$	$C_2$	+	$H$			236
$e^-$	+	$C_2H^+$	$\rightarrow$	$CH$	+	$C$			236
$e^-$	+	$C_2H^+$	$\rightarrow$	$2C$	+	$H$			236
$e^-$	+	$C_2^+$	$\rightarrow$	$2C$					236
$e^-$	+	$H_3^+$	$\rightarrow$	$3H$					252
$e^-$	+	$H_3^+$	$\rightarrow$	$H_2$	+	$H$			252
$e^-$	+	$H_2^+$	$\rightarrow$	$2H$					252
$e^-$	+	$O^+$	+	$O_2$	$\rightarrow$	$O$	+	$O_2$	241
$e^-$	+	$O_2^+$			$\rightarrow$	$O$	+	$O$	241
$e^-$	+	$O_2^+$	+	$O_2$	$\rightarrow$	$O_2$	+	$O_2$	241
$e^-$	+	$O_4^+$			$\rightarrow$	$O_2$	+	$O_2$	241
$e^-$	+	$CO_2^+$			$\rightarrow$	$CO$	+	$O$	252
$e^-$	+	$CO^+$			$\rightarrow$	$C$	+	$O$	252
$e^-$	+	$OH^+$			$\rightarrow$	$O$	+	$H$	252
$e^-$	+	$H_2O^+$			$\rightarrow$	$OH$	+	$H$	252
$e^-$	+	$H_2O^+$			$\rightarrow$	$O$	+	$H_2$	252
$e^-$	+	$H_2O^+$			$\rightarrow$	$O$	+	$2H$	252
$e^-$	+	$H_3O^+$			$\rightarrow$	$H_2O$	+	$H$	252
$e^-$	+	$H_3O^+$			$\rightarrow$	$OH$	+	$H_2$	252
$e^-$	+	$H_3O^+$			$\rightarrow$	$OH$	+	$2H$	252

**Table A.3.** Neutral-neutral reactions included in the model, as well as the corresponding rate coefficients at 300 K and the references where these data were adopted from. Note a means “estimated value”; b = “adjusted in the model for a three-body collision by dividing by  $2.446 \times 10^{19} \text{ cm}^{-3}$ , i.e., the density of the inlet gas”. M = CH<sub>4</sub> in pure CH<sub>4</sub>, M = CH<sub>4</sub>, CO<sub>2</sub>, O<sub>2</sub> or H<sub>2</sub>O in the CH<sub>4</sub>/O<sub>2</sub> and CH<sub>4</sub>/CO<sub>2</sub> gas mixtures and M = CO<sub>2</sub> or H<sub>2</sub> in the CO<sub>2</sub>/H<sub>2</sub> gas mixtures. The rate coefficients are expressed in  $\text{cm}^3 \text{ s}^{-1}$  and  $\text{cm}^6 \text{ s}^{-1}$  for two-body and three-body reactions, respectively. Note that the values in Table A.3. and Table A.4. are defined with two decimal digits, as found in literature, however, this precision is not decisive for the output of the model considering the likely uncertainty of these values.

CH <sub>4</sub>	+	CH <sub>2</sub>	→	CH <sub>3</sub>	+	CH <sub>3</sub>	3.01x10 <sup>-19</sup>	253		
CH <sub>4</sub>	+	CH	→	C <sub>2</sub> H <sub>4</sub>	+	H	9.74x10 <sup>-11</sup>	254		
CH <sub>4</sub>	+	C <sub>2</sub> H <sub>5</sub>	→	C <sub>2</sub> H <sub>6</sub>	+	CH <sub>3</sub>	1.83x10 <sup>-24</sup>	253		
CH <sub>4</sub>	+	C <sub>2</sub> H <sub>3</sub>	→	C <sub>2</sub> H <sub>4</sub>	+	CH <sub>3</sub>	2.28x10 <sup>-18</sup>	253		
CH <sub>4</sub>	+	C <sub>2</sub> H	→	C <sub>2</sub> H <sub>2</sub>	+	CH <sub>3</sub>	1.31x10 <sup>-12</sup>	253		
CH <sub>4</sub>	+	C <sub>3</sub> H <sub>7</sub>	→	C <sub>3</sub> H <sub>8</sub>	+	CH <sub>3</sub>	4.38x10 <sup>-24</sup>	255		
CH <sub>4</sub>	+	C <sub>3</sub> H <sub>5</sub>	→	C <sub>3</sub> H <sub>6</sub>	+	CH <sub>3</sub>	2.02x10 <sup>-31</sup>	256		
CH <sub>4</sub>	+	H	→	CH <sub>3</sub>	+	H <sub>2</sub>	8.43x10 <sup>-19</sup>	254		
CH <sub>3</sub>	+	CH <sub>3</sub>	→	C <sub>2</sub> H <sub>5</sub>	+	H	2.71x10 <sup>-19</sup>	257		
CH <sub>3</sub>	+	CH <sub>3</sub>	+	M	→	C <sub>2</sub> H <sub>6</sub>	+	M	1.56x10 <sup>-26</sup>	254
CH <sub>3</sub>	+	CH <sub>2</sub>	→	C <sub>2</sub> H <sub>4</sub>	+	H	7.01x10 <sup>-11</sup>	254		
CH <sub>3</sub>	+	C <sub>2</sub> H <sub>6</sub>	→	C <sub>2</sub> H <sub>5</sub>	+	CH <sub>4</sub>	7.21x10 <sup>-21</sup>	254		
CH <sub>3</sub>	+	C <sub>2</sub> H <sub>5</sub>	→	C <sub>2</sub> H <sub>4</sub>	+	CH <sub>4</sub>	1.91x10 <sup>-12</sup>	254		
CH <sub>3</sub>	+	C <sub>2</sub> H <sub>5</sub>	+	M	→	C <sub>3</sub> H <sub>8</sub>	+	M	1.00x10 <sup>-28</sup>	a
CH <sub>3</sub>	+	C <sub>2</sub> H <sub>4</sub>	→	C <sub>2</sub> H <sub>3</sub>	+	CH <sub>4</sub>	1.94x10 <sup>-21</sup>	253		

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CH <sub>3</sub>	+	C <sub>2</sub> H <sub>3</sub>		→	C <sub>2</sub> H <sub>2</sub>	+	CH <sub>4</sub>	6.51x10 <sup>-13</sup>	253	
								1.20x10 <sup>-10</sup>	258	
CH <sub>3</sub>	+	C <sub>2</sub> H <sub>3</sub>	+	M	→	C <sub>3</sub> H <sub>6</sub>	+	M	4.91x10 <sup>-30</sup> <b>b</b>	
CH <sub>3</sub>	+	C <sub>2</sub> H <sub>2</sub>		→	CH <sub>4</sub>	+	C <sub>2</sub> H	7.65x10 <sup>-26</sup>	253	
CH <sub>3</sub>	+	C <sub>3</sub> H <sub>8</sub>		→	C <sub>3</sub> H <sub>7</sub>	+	CH <sub>4</sub>	1.02x10 <sup>-20</sup>	255	
CH <sub>3</sub>	+	C <sub>3</sub> H <sub>7</sub>		→	C <sub>3</sub> H <sub>6</sub>	+	CH <sub>4</sub>	3.07x10 <sup>-12</sup>	255	
CH <sub>3</sub>	+	C <sub>3</sub> H <sub>6</sub>		→	C <sub>3</sub> H <sub>5</sub>	+	CH <sub>4</sub>	1.24x10 <sup>-19</sup>	256	
CH <sub>3</sub>	+	H <sub>2</sub>		→	CH <sub>4</sub>	+	H	9.60x10 <sup>-21</sup>	254	
CH <sub>3</sub>	+	H		→	CH <sub>2</sub>	+	H <sub>2</sub>	9.96x10 <sup>-22</sup>	254	
CH <sub>3</sub>	+	H	+	M	→	CH <sub>4</sub>	+	M	2.97x10 <sup>-28</sup>	254
CH <sub>2</sub>	+	CH <sub>2</sub>		→	C <sub>2</sub> H <sub>2</sub>	+	2H	5.27x10 <sup>-11</sup>	254	
CH <sub>2</sub>	+	C <sub>2</sub> H <sub>5</sub>		→	C <sub>2</sub> H <sub>4</sub>	+	CH <sub>3</sub>	3.01x10 <sup>-11</sup>	253	
CH <sub>2</sub>	+	C <sub>2</sub> H <sub>3</sub>		→	C <sub>2</sub> H <sub>2</sub>	+	CH <sub>3</sub>	3.01x10 <sup>-11</sup>	253	
CH <sub>2</sub>	+	C <sub>2</sub> H		→	C <sub>2</sub> H <sub>2</sub>	+	CH	3.01x10 <sup>-11</sup>	253	
CH <sub>2</sub>	+	C <sub>3</sub> H <sub>8</sub>		→	C <sub>3</sub> H <sub>7</sub>	+	CH <sub>3</sub>	1.02x10 <sup>-20</sup>	255	
CH <sub>2</sub>	+	C <sub>3</sub> H <sub>7</sub>		→	C <sub>2</sub> H <sub>4</sub>	+	C <sub>2</sub> H <sub>5</sub>	3.01x10 <sup>-11</sup>	255	
CH <sub>2</sub>	+	C <sub>3</sub> H <sub>7</sub>		→	C <sub>3</sub> H <sub>6</sub>	+	CH <sub>3</sub>	3.01x10 <sup>-12</sup>	255	
CH <sub>2</sub>	+	C <sub>3</sub> H <sub>6</sub>		→	C <sub>3</sub> H <sub>5</sub>	+	CH <sub>3</sub>	3.65x10 <sup>-17</sup>	256	
CH <sub>2</sub>	+	H <sub>2</sub>		→	CH <sub>3</sub>	+	H	5.00x10 <sup>-15</sup>	253	
CH <sub>2</sub>	+	H		→	CH	+	H <sub>2</sub>	2.01x10 <sup>-10</sup>	254	
								2.78x10 <sup>-10</sup>	254	
CH	+	C <sub>2</sub> H <sub>6</sub>	+	M	→	C <sub>3</sub> H <sub>7</sub>	+	M	1.14x10 <sup>-29</sup> <b>b</b>	
CH	+	H <sub>2</sub>		→	CH <sub>2</sub>	+	H	6.80x10 <sup>-13</sup>	254	
CH	+	H		→	C	+	H <sub>2</sub>	1.00x10 <sup>-10</sup>	259	
C	+	H <sub>2</sub>		→	CH	+	H	1.50x10 <sup>-10</sup>	260	
C <sub>2</sub> H <sub>6</sub>	+	C <sub>2</sub> H <sub>3</sub>		→	C <sub>2</sub> H <sub>5</sub>	+	C <sub>2</sub> H <sub>4</sub>	3.39x10 <sup>-21</sup>	253	

$C_2H_6$	+	$C_2H$	$\rightarrow$	$C_2H_2$	+	$C_2H_5$	$5.99 \times 10^{-12}$	253
$C_2H_6$	+	$C_3H_7$	$\rightarrow$	$C_3H_8$	+	$C_2H_5$	$3.16 \times 10^{-22}$	255
$C_2H_6$	+	$C_3H_5$	$\rightarrow$	$C_3H_6$	+	$C_2H_5$	$2.02 \times 10^{-28}$	256
$C_2H_6$	+	H	$\rightarrow$	$C_2H_5$	+	$H_2$	$4.96 \times 10^{-17}$	254
$C_2H_5$	+	$C_2H_5$	$\rightarrow$	$C_2H_6$	+	$C_2H_4$	$2.41 \times 10^{-12}$	254
$C_2H_5$	+	$C_2H_4$	$\rightarrow$	$C_2H_6$	+	$C_2H_3$	$4.56 \times 10^{-27}$	253
$C_2H_5$	+	$C_2H_2$	$\rightarrow$	$C_2H_6$	+	$C_2H$	$3.72 \times 10^{-30}$	253
$C_2H_5$	+	$C_2H$	$\rightarrow$	$C_2H_4$	+	$C_2H_2$	$3.01 \times 10^{-12}$	253
$C_2H_5$	+	$C_3H_8$	$\rightarrow$	$C_2H_6$	+	$C_3H_7$	$3.62 \times 10^{-22}$	255
$C_2H_5$	+	$C_3H_7$	$\rightarrow$	$C_3H_8$	+	$C_2H_4$	$1.91 \times 10^{-12}$	255
$C_2H_5$	+	$C_3H_7$	$\rightarrow$	$C_3H_6$	+	$C_2H_6$	$2.41 \times 10^{-12}$	255
$C_2H_5$	+	$C_3H_6$	$\rightarrow$	$C_3H_5$	+	$C_2H_6$	$2.53 \times 10^{-20}$	256
$C_2H_5$	+	$C_3H_5$	$\rightarrow$	$C_3H_6$	+	$C_2H_4$	$5.36 \times 10^{-12}$	256
$C_2H_5$	+	$H_2$	$\rightarrow$	$C_2H_6$	+	H	$2.97 \times 10^{-21}$	253
$C_2H_5$	+	H	$\rightarrow$	$CH_3$	+	$CH_3$	$5.99 \times 10^{-11}$	254
$C_2H_5$	+	H	$\rightarrow$	$C_2H_4$	+	$H_2$	$3.01 \times 10^{-12}$	253
$C_2H_5$	+	H					$2.25 \times 10^{-10}$	261
$C_2H_5$	+	H	+	M	$\rightarrow$	$C_2H_6$	+	M
							$9.20 \times 10^{-30}$	b
$C_2H_4$	+	$C_2H$	$\rightarrow$	$C_2H_2$	+	$C_2H_3$	$1.40 \times 10^{-10}$	258
$C_2H_4$	+	H	$\rightarrow$	$C_2H_3$	+	$H_2$	$4.92 \times 10^{-21}$	253
$C_2H_4$	+	H	+	M	$\rightarrow$	$C_2H_5$	+	M
							$3.66 \times 10^{-30}$	254
$C_2H_3$	+	$C_2H_3$	$\rightarrow$	$C_2H_4$	+	$C_2H_2$	$1.60 \times 10^{-12}$	253
$C_2H_3$	+	$C_2H$	$\rightarrow$	$C_2H_2$	+	$C_2H_2$	$1.60 \times 10^{-12}$	253
$C_2H_3$	+	$C_3H_8$	$\rightarrow$	$C_2H_4$	+	$C_3H_7$	$3.40 \times 10^{-21}$	255
$C_2H_3$	+	$C_3H_7$	$\rightarrow$	$C_3H_8$	+	$C_2H_2$	$2.01 \times 10^{-12}$	255
$C_2H_3$	+	$C_3H_7$	$\rightarrow$	$C_3H_6$	+	$C_2H_4$	$2.01 \times 10^{-12}$	255

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C <sub>2</sub> H <sub>3</sub>	+	C <sub>3</sub> H <sub>6</sub>		→	C <sub>3</sub> H <sub>5</sub>	+	C <sub>2</sub> H <sub>4</sub>	6.58x10 <sup>-19</sup>	256	
C <sub>2</sub> H <sub>3</sub>	+	C <sub>3</sub> H <sub>5</sub>		→	C <sub>3</sub> H <sub>6</sub>	+	C <sub>2</sub> H <sub>2</sub>	8.00x10 <sup>-12</sup>	256	
C <sub>2</sub> H <sub>3</sub>	+	H <sub>2</sub>		→	C <sub>2</sub> H <sub>4</sub>	+	H	9.78x10 <sup>-20</sup>	253	
C <sub>2</sub> H <sub>3</sub>	+	H		→	C <sub>2</sub> H <sub>2</sub>	+	H <sub>2</sub>	2.01x10 <sup>-11</sup>	254	
C <sub>2</sub> H <sub>3</sub>	+	H	+	M	→	C <sub>2</sub> H <sub>4</sub>	+	M	2.02x10 <sup>-10</sup>	261
									8.26x10 <sup>-30</sup>	b
C <sub>2</sub> H <sub>2</sub>	+	C <sub>2</sub> H		→	C <sub>4</sub> H <sub>2</sub>	+	H	1.50x10 <sup>-10</sup>	114	
C <sub>2</sub> H <sub>2</sub>	+	H		→	C <sub>2</sub> H	+	H <sub>2</sub>	6.12x10 <sup>-27</sup>	253	
C <sub>2</sub> H <sub>2</sub>	+	H	+	M	→	C <sub>2</sub> H <sub>3</sub>	+	M	2.81x10 <sup>-31</sup>	254
C <sub>2</sub> H	+	C <sub>2</sub> H		→	C <sub>2</sub> H <sub>2</sub>	+	C <sub>2</sub>	3.01x10 <sup>-12</sup>	253	
C <sub>2</sub> H	+	C <sub>3</sub> H <sub>8</sub>		→	C <sub>2</sub> H <sub>2</sub>	+	C <sub>3</sub> H <sub>7</sub>	5.99x10 <sup>-12</sup>	255	
C <sub>2</sub> H	+	C <sub>3</sub> H <sub>7</sub>		→	C <sub>3</sub> H <sub>6</sub>	+	C <sub>2</sub> H <sub>2</sub>	1.00x10 <sup>-11</sup>	255	
C <sub>2</sub> H	+	C <sub>3</sub> H <sub>6</sub>		→	C <sub>3</sub> H <sub>5</sub>	+	C <sub>2</sub> H <sub>2</sub>	5.99x10 <sup>-12</sup>	256	
C <sub>2</sub> H	+	H <sub>2</sub>		→	C <sub>2</sub> H <sub>2</sub>	+	H	1.52x10 <sup>-13</sup>	253	
C <sub>2</sub> H	+	H		→	C <sub>2</sub>	+	H <sub>2</sub>	1.66x10 <sup>-31</sup>	253	
C <sub>2</sub> H	+	H	+	M	→	C <sub>2</sub> H <sub>2</sub>	+	M	2.31x10 <sup>-10</sup>	261
									9.44x10 <sup>-30</sup>	b
C <sub>3</sub> H <sub>8</sub>	+	C <sub>3</sub> H <sub>5</sub>		→	C <sub>3</sub> H <sub>6</sub>	+	C <sub>3</sub> H <sub>7</sub>	2.02x10 <sup>-28</sup>	256	
C <sub>3</sub> H <sub>8</sub>	+	H		→	C <sub>3</sub> H <sub>7</sub>	+	H <sub>2</sub>	5.15x10 <sup>-17</sup>	255	
C <sub>3</sub> H <sub>7</sub>	+	C <sub>3</sub> H <sub>7</sub>		→	C <sub>3</sub> H <sub>6</sub>	+	C <sub>3</sub> H <sub>8</sub>	2.81x10 <sup>-12</sup>	255	
C <sub>3</sub> H <sub>7</sub>	+	C <sub>3</sub> H <sub>6</sub>		→	C <sub>3</sub> H <sub>5</sub>	+	C <sub>3</sub> H <sub>8</sub>	2.53x10 <sup>-20</sup>	256	
C <sub>3</sub> H <sub>7</sub>	+	C <sub>3</sub> H <sub>5</sub>		→	C <sub>3</sub> H <sub>6</sub>	+	C <sub>3</sub> H <sub>6</sub>	3.00x10 <sup>-12</sup>	256	
C <sub>3</sub> H <sub>7</sub>	+	H <sub>2</sub>		→	C <sub>3</sub> H <sub>8</sub>	+	H	7.12x10 <sup>-21</sup>	255	
C <sub>3</sub> H <sub>7</sub>	+	H		→	C <sub>3</sub> H <sub>6</sub>	+	H <sub>2</sub>	3.01x10 <sup>-12</sup>	255	
C <sub>3</sub> H <sub>7</sub>	+	H	+	M	→	C <sub>3</sub> H <sub>8</sub>	+	M	9.68x10 <sup>-11</sup>	261
									3.96x10 <sup>-30</sup>	b

C <sub>3</sub> H <sub>6</sub>	+	H		→	C <sub>3</sub> H <sub>5</sub>	+	H <sub>2</sub>		6.94x10 <sup>-15</sup>	256	
C <sub>3</sub> H <sub>6</sub>	+	H	+	M	→	C <sub>3</sub> H <sub>7</sub>	+	M	9.26x10 <sup>-14</sup>	256	
									3.79x10 <sup>-33</sup>	b	
C <sub>3</sub> H <sub>5</sub>	+	H <sub>2</sub>			→	C <sub>3</sub> H <sub>6</sub>	+	H	2.05x10 <sup>-27</sup>	256	
C <sub>3</sub> H <sub>5</sub>	+	H	+	M	→	C <sub>3</sub> H <sub>6</sub>	+	M	3.26x10 <sup>-10</sup>	262	
									1.33x10 <sup>-29</sup>	b	
H	+	H	+	M	→	H <sub>2</sub>	+	M	6.00x10 <sup>-33</sup>	254	
O <sub>3</sub>	+	O			→	O <sub>2</sub>	+	O <sub>2</sub>	8.43x10 <sup>-15</sup>	263	
O <sub>3</sub>	+	O <sub>2</sub>			→	O	+	O <sub>2</sub>	+ O <sub>2</sub>	2.29x10 <sup>-26</sup>	263
O	+	O <sub>2</sub>	+	M	→	O <sub>3</sub>	+	M		6.90x10 <sup>-34</sup>	263
O <sub>3</sub>	+	O <sub>3</sub>			→	O	+	O <sub>2</sub>	+ O <sub>3</sub>	5.18x10 <sup>-26</sup>	263
O	+	O	+	O	→	O <sub>2</sub>	+	O		5.09x10 <sup>-33</sup>	263
O	+	O	+	M	→	O <sub>2</sub>	+	M		7.19x10 <sup>-33</sup>	263
O	+	O <sub>2</sub>	+	O	→	O <sub>3</sub>	+	O		6.32x10 <sup>-34</sup>	263
O	+	O <sub>2</sub>	+	O <sub>3</sub>	→	O <sub>3</sub>	+	O <sub>3</sub>		1.52x10 <sup>-33</sup>	263
O <sub>3</sub>	+	O			→	O	+	O <sub>2</sub>	+ O	3.14x10 <sup>-27</sup>	263
CH <sub>4</sub>	+	O			→	CH <sub>3</sub>	+	OH		5.54x10 <sup>-18</sup>	254
CH <sub>3</sub>	+	O			→	CH <sub>2</sub> O	+	H		1.12x10 <sup>-10</sup>	264
CH <sub>3</sub>	+	O			→	CO	+	H <sub>2</sub>	+ H	2.80x10 <sup>-11</sup>	264
CH <sub>3</sub>	+	O <sub>2</sub>	+	M	→	CH <sub>3</sub> O <sub>2</sub>	+	M		9.79x10 <sup>-31</sup>	265
CH <sub>3</sub>	+	O <sub>3</sub>			→	CH <sub>3</sub> O	+	O <sub>2</sub>		2.33x10 <sup>-12</sup>	265
CH <sub>2</sub>	+	O			→	CO	+	H <sub>2</sub>		5.53x10 <sup>-11</sup>	264
CH <sub>2</sub>	+	O			→	CO	+	2H		8.29x10 <sup>-11</sup>	264
CH <sub>2</sub>	+	O <sub>2</sub>			→	CO <sub>2</sub>	+	H <sub>2</sub>		1.42x10 <sup>-12</sup>	254, 266
CH <sub>2</sub>	+	O <sub>2</sub>			→	CO	+	H <sub>2</sub> O		1.42x10 <sup>-12</sup>	254, 266

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CH <sub>2</sub>	+	O <sub>2</sub>	→	CH <sub>2</sub> O	+	O	5.39x10 <sup>-13</sup>	254, 266	
CH	+	O	→	CO	+	H	6.60x10 <sup>-11</sup>	254	
CH	+	O <sub>2</sub>	→	CO <sub>2</sub>	+	H	1.20x10 <sup>-11</sup>	264	
CH	+	O <sub>2</sub>	→	CO	+	OH	8.00x10 <sup>-12</sup>	264	
CH	+	O <sub>2</sub>	→	CHO	+	O	8.00x10 <sup>-12</sup>	264	
CH	+	O <sub>2</sub>	→	CO	+	H	+ O	1.20x10 <sup>-11</sup>	264
C	+	O <sub>2</sub>	→	CO	+	O	2.45x10 <sup>-13</sup>	267	
C <sub>2</sub> H <sub>6</sub>	+	O	→	C <sub>2</sub> H <sub>5</sub>	+	OH	5.11x10 <sup>-16</sup>	254	
C <sub>2</sub> H <sub>5</sub>	+	O	→	CH <sub>3</sub> CHO	+	H	8.80x10 <sup>-11</sup>	264	
C <sub>2</sub> H <sub>5</sub>	+	O	→	CH <sub>2</sub> O	+	CH <sub>3</sub>	6.60x10 <sup>-11</sup>	264	
C <sub>2</sub> H <sub>5</sub>	+	O	→	C <sub>2</sub> H <sub>4</sub>	+	OH	4.40x10 <sup>-11</sup>	264	
C <sub>2</sub> H <sub>5</sub>	+	O <sub>2</sub>	→	C <sub>2</sub> H <sub>4</sub>	+	HO <sub>2</sub>	3.80x10 <sup>-15</sup>	265	
C <sub>2</sub> H <sub>5</sub>	+	O <sub>2</sub>	+ M	→	C <sub>2</sub> H <sub>5</sub> O <sub>2</sub>	+	M	5.75x10 <sup>-29</sup>	265
C <sub>2</sub> H <sub>4</sub>	+	O	→	CH <sub>2</sub> CHO	+	H	2.63x10 <sup>-13</sup>	264	
C <sub>2</sub> H <sub>4</sub>	+	O	→	CHO	+	CH <sub>3</sub>	4.51x10 <sup>-13</sup>	264	
C <sub>2</sub> H <sub>4</sub>	+	O <sub>3</sub>	→	CH <sub>2</sub> O	+	CO <sub>2</sub>	+ H <sub>2</sub>	7.06x10 <sup>-19</sup>	265- 266
C <sub>2</sub> H <sub>4</sub>	+	O <sub>3</sub>	→	CH <sub>2</sub> O	+	CO	+ H <sub>2</sub> O	7.06x10 <sup>-19</sup>	265- 266
C <sub>2</sub> H <sub>4</sub>	+	O <sub>3</sub>	→	2CH <sub>2</sub> O	+	O	2.69x10 <sup>-19</sup>	265- 266	
C <sub>2</sub> H <sub>3</sub>	+	O	→	C <sub>2</sub> H <sub>2</sub>	+	OH	1.25x10 <sup>-11</sup>	264	
C <sub>2</sub> H <sub>3</sub>	+	O	→	CO	+	CH <sub>3</sub>	1.25x10 <sup>-11</sup>	264	
C <sub>2</sub> H <sub>3</sub>	+	O	→	CHO	+	CH <sub>2</sub>	1.25x10 <sup>-11</sup>	264	
C <sub>2</sub> H <sub>3</sub>	+	O	→	CH <sub>2</sub> CO	+	H	1.25x10 <sup>-11</sup>	264	
C <sub>2</sub> H <sub>3</sub>	+	O <sub>2</sub>	→	CH <sub>2</sub> O	+	CHO	9.00x10 <sup>-12</sup>	254	
C <sub>2</sub> H <sub>2</sub>	+	O	→	CH <sub>2</sub>	+	CO	6.75x10 <sup>-14</sup>	254	

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C <sub>2</sub> H <sub>2</sub>	+	O		→	C <sub>2</sub> HO	+	H	6.75x10 <sup>-14</sup>	254	
C <sub>2</sub> H	+	O		→	CH	+	CO	1.70x10 <sup>-11</sup>	254	
C <sub>2</sub> H	+	O <sub>2</sub>		→	CHO	+	CO	3.00x10 <sup>-11</sup>	254	
C <sub>2</sub> H	+	O <sub>2</sub>		→	C <sub>2</sub> HO	+	O	1.00x10 <sup>-12</sup>	253	
C <sub>3</sub> H <sub>8</sub>	+	O		→	C <sub>3</sub> H <sub>7</sub>	+	OH	2.73x10 <sup>-15</sup>	255	
H <sub>2</sub>	+	O		→	OH	+	H	9.32x10 <sup>-18</sup>	254	
H	+	O	+	M	→	OH	+	M	4.33x10 <sup>-32</sup>	253
H	+	O <sub>2</sub>		→	OH	+	O	1.87x10 <sup>-22</sup>	254	
H	+	O <sub>2</sub>	+	M	→	HO <sub>2</sub>	+	M	5.40x10 <sup>-32</sup>	268
H	+	O <sub>3</sub>		→	OH	+	O <sub>2</sub>	2.83x10 <sup>-11</sup>	269	
CH <sub>4</sub>	+	OH		→	CH <sub>3</sub>	+	H <sub>2</sub> O	6.62x10 <sup>-15</sup>	265	
CH <sub>4</sub>	+	HO <sub>2</sub>		→	CH <sub>3</sub>	+	H <sub>2</sub> O <sub>2</sub>	8.76x10 <sup>-27</sup>	253	
CH <sub>4</sub>	+	CHO		→	CH <sub>3</sub>	+	CH <sub>2</sub> O	6.07x10 <sup>-30</sup>	253	
CH <sub>4</sub>	+	CH <sub>3</sub> O		→	CH <sub>3</sub> OH	+	CH <sub>3</sub>	9.42x10 <sup>-20</sup>	253	
CH <sub>4</sub>	+	CH <sub>3</sub> O <sub>2</sub>		→	CH <sub>3</sub>	+	CH <sub>3</sub> OOH	1.03x10 <sup>-26</sup>	253	
CH <sub>3</sub>	+	CO	+	M	→	CH <sub>3</sub> CO	+	M	4.19x10 <sup>-36</sup>	114
CH <sub>3</sub>	+	H <sub>2</sub> O		→	CH <sub>4</sub>	+	OH	1.82x10 <sup>-25</sup>	253	
CH <sub>3</sub>	+	OH		→	CH <sub>2</sub>	+	H <sub>2</sub> O	1.13x10 <sup>-12</sup>	114	
CH <sub>3</sub>	+	OH		→	CH <sub>2</sub> OH	+	H	1.31x10 <sup>-11</sup>	270	
CH <sub>3</sub>	+	OH		→	CH <sub>3</sub> O	+	H	1.60x10 <sup>-10</sup>	270	
CH <sub>3</sub>	+	OH	+	M	→	CH <sub>3</sub> OH	+	M	2.30x10 <sup>-27</sup>	114
CH <sub>3</sub>	+	HO <sub>2</sub>		→	CH <sub>3</sub> O	+	OH	3.00x10 <sup>-11</sup>	254	
CH <sub>3</sub>	+	HO <sub>2</sub>		→	CH <sub>4</sub>	+	O <sub>2</sub>	5.99x10 <sup>-12</sup>	253	
CH <sub>3</sub>	+	CH <sub>2</sub> O		→	CH <sub>4</sub>	+	CHO	6.14x10 <sup>-18</sup>	114	
CH <sub>3</sub>	+	CHO		→	CH <sub>4</sub>	+	CO	2.00x10 <sup>-10</sup>	253	
CH <sub>3</sub>	+	CH <sub>3</sub> O		→	CH <sub>4</sub>	+	CH <sub>2</sub> O	4.00x10 <sup>-11</sup>	253	



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CH <sub>3</sub>	+	CH <sub>3</sub> CHO	→	CH <sub>4</sub>	+	CH <sub>3</sub> CO	4.95x10 <sup>-18</sup>	254
CH <sub>3</sub>	+	CH <sub>3</sub> O <sub>2</sub>	→	CH <sub>3</sub> O	+	CH <sub>3</sub> O	4.00x10 <sup>-11</sup>	253
CH <sub>2</sub>	+	CO <sub>2</sub>	→	CH <sub>2</sub> O	+	CO	3.90x10 <sup>-14</sup>	253
CH <sub>2</sub>	+	H <sub>2</sub> O	→	CH <sub>3</sub>	+	OH	1.60x10 <sup>-16</sup>	253
CH <sub>2</sub>	+	OH	→	CH <sub>2</sub> O	+	H	3.00x10 <sup>-11</sup>	253
CH <sub>2</sub>	+	HO <sub>2</sub>	→	CH <sub>2</sub> O	+	OH	3.00x10 <sup>-11</sup>	253
CH <sub>2</sub>	+	CH <sub>2</sub> O	→	CH <sub>3</sub>	+	CHO	1.00x10 <sup>-14</sup>	253
CH <sub>2</sub>	+	CHO	→	CH <sub>3</sub>	+	CO	3.00x10 <sup>-11</sup>	253
CH <sub>2</sub>	+	CH <sub>3</sub> O	→	CH <sub>3</sub>	+	CH <sub>2</sub> O	3.00x10 <sup>-11</sup>	253
CH <sub>2</sub>	+	CH <sub>3</sub> O <sub>2</sub>	→	CH <sub>2</sub> O	+	CH <sub>3</sub> O	3.00x10 <sup>-11</sup>	253
CH	+	CO <sub>2</sub>	→	CHO	+	CO	9.68x10 <sup>-13</sup>	264
CH	+	CO <sub>2</sub>	→	2CO	+	H	9.68x10 <sup>-13</sup>	264
CH	+	CO	+	M	→	C <sub>2</sub> H <sub>2</sub> O	4.04x10 <sup>-30</sup>	264
C <sub>2</sub> H <sub>6</sub>	+	OH	→	C <sub>2</sub> H <sub>5</sub>	+	H <sub>2</sub> O	2.46x10 <sup>-13</sup>	265
C <sub>2</sub> H <sub>6</sub>	+	HO <sub>2</sub>	→	C <sub>2</sub> H <sub>5</sub>	+	H <sub>2</sub> O <sub>2</sub>	6.36x10 <sup>-24</sup>	253
C <sub>2</sub> H <sub>6</sub>	+	CHO	→	C <sub>2</sub> H <sub>5</sub>	+	CH <sub>2</sub> O	2.19x10 <sup>-26</sup>	253
C <sub>2</sub> H <sub>6</sub>	+	CH <sub>3</sub> O	→	C <sub>2</sub> H <sub>5</sub>	+	CH <sub>3</sub> OH	2.72x10 <sup>-18</sup>	253
C <sub>2</sub> H <sub>6</sub>	+	CH <sub>3</sub> O <sub>2</sub>	→	C <sub>2</sub> H <sub>5</sub>	+	CH <sub>3</sub> OOH	6.36x10 <sup>-24</sup>	253
C <sub>2</sub> H <sub>6</sub>	+	C <sub>2</sub> H <sub>5</sub> O <sub>2</sub>	→	C <sub>2</sub> H <sub>5</sub>	+	C <sub>2</sub> H <sub>5</sub> OOH	8.69x10 <sup>-27</sup>	271
C <sub>2</sub> H <sub>5</sub>	+	H <sub>2</sub> O	→	C <sub>2</sub> H <sub>6</sub>	+	OH	3.56x10 <sup>-29</sup>	253
C <sub>2</sub> H <sub>5</sub>	+	OH	→	C <sub>2</sub> H <sub>4</sub>	+	H <sub>2</sub> O	4.00x10 <sup>-11</sup>	253
C <sub>2</sub> H <sub>5</sub>	+	HO <sub>2</sub>	→	C <sub>2</sub> H <sub>6</sub>	+	O <sub>2</sub>	5.00x10 <sup>-13</sup>	253
C <sub>2</sub> H <sub>5</sub>	+	HO <sub>2</sub>	→	C <sub>2</sub> H <sub>4</sub>	+	H <sub>2</sub> O <sub>2</sub>	5.00x10 <sup>-13</sup>	253
C <sub>2</sub> H <sub>5</sub>	+	CH <sub>2</sub> O	→	C <sub>2</sub> H <sub>6</sub>	+	CHO	4.47x10 <sup>-18</sup>	253
C <sub>2</sub> H <sub>5</sub>	+	CHO	→	C <sub>2</sub> H <sub>6</sub>	+	CO	2.00x10 <sup>-10</sup>	253
C <sub>2</sub> H <sub>5</sub>	+	CH <sub>3</sub> O	→	C <sub>2</sub> H <sub>6</sub>	+	CH <sub>2</sub> O	4.00x10 <sup>-11</sup>	253

C <sub>2</sub> H <sub>5</sub>	+	CH <sub>3</sub> O <sub>2</sub>	→	CH <sub>3</sub> O	+	C <sub>2</sub> H <sub>5</sub> O	4.00x10 <sup>-11</sup>	253
C <sub>2</sub> H <sub>4</sub>	+	OH	→	C <sub>2</sub> H <sub>3</sub>	+	H <sub>2</sub> O	1.54x10 <sup>-16</sup>	253
C <sub>2</sub> H <sub>4</sub>	+	HO <sub>2</sub>	→	CH <sub>3</sub> CHO	+	OH	1.62x10 <sup>-20</sup>	253
C <sub>2</sub> H <sub>3</sub>	+	H <sub>2</sub> O	→	C <sub>2</sub> H <sub>4</sub>	+	OH	1.82x10 <sup>-25</sup>	253
C <sub>2</sub> H <sub>3</sub>	+	OH	→	C <sub>2</sub> H <sub>2</sub>	+	H <sub>2</sub> O	5.00x10 <sup>-11</sup>	253
C <sub>2</sub> H <sub>3</sub>	+	CH <sub>2</sub> O	→	C <sub>2</sub> H <sub>4</sub>	+	CHO	4.41x10 <sup>-18</sup>	253
C <sub>2</sub> H <sub>3</sub>	+	CHO	→	C <sub>2</sub> H <sub>4</sub>	+	CO	1.50x10 <sup>-10</sup>	253
C <sub>2</sub> H <sub>3</sub>	+	CH <sub>3</sub> O	→	C <sub>2</sub> H <sub>4</sub>	+	CH <sub>2</sub> O	4.00x10 <sup>-11</sup>	253
C <sub>2</sub> H <sub>2</sub>	+	OH	→	C <sub>2</sub> H	+	H <sub>2</sub> O	1.77x10 <sup>-22</sup>	253
C <sub>2</sub> H <sub>2</sub>	+	HO <sub>2</sub>	→	CH <sub>2</sub> CO	+	OH	1.62x10 <sup>-20</sup>	253
C <sub>2</sub> H	+	OH	→	CH <sub>2</sub>	+	CO	3.00x10 <sup>-11</sup>	253
C <sub>2</sub> H	+	OH	→	C <sub>2</sub> H <sub>2</sub>	+	O	3.00x10 <sup>-11</sup>	253
C <sub>2</sub> H	+	HO <sub>2</sub>	→	C <sub>2</sub> H <sub>2</sub>	+	O <sub>2</sub>	3.00x10 <sup>-11</sup>	253
C <sub>2</sub> H	+	HO <sub>2</sub>	→	C <sub>2</sub> HO	+	OH	3.00x10 <sup>-11</sup>	253
C <sub>2</sub> H	+	CHO	→	C <sub>2</sub> H <sub>2</sub>	+	CO	1.00x10 <sup>-10</sup>	253
C <sub>2</sub> H	+	CH <sub>3</sub> O	→	C <sub>2</sub> H <sub>2</sub>	+	CH <sub>2</sub> O	4.00x10 <sup>-11</sup>	253
C <sub>2</sub> H	+	CH <sub>3</sub> O <sub>2</sub>	→	CH <sub>3</sub> O	+	C <sub>2</sub> HO	4.00x10 <sup>-11</sup>	253
C <sub>3</sub> H <sub>8</sub>	+	OH	→	C <sub>3</sub> H <sub>7</sub>	+	H <sub>2</sub> O	3.76x10 <sup>-15</sup>	255
C <sub>3</sub> H <sub>8</sub>	+	HO <sub>2</sub>	→	C <sub>3</sub> H <sub>7</sub>	+	H <sub>2</sub> O <sub>2</sub>	1.58x10 <sup>-25</sup>	255
C <sub>3</sub> H <sub>8</sub>	+	CHO	→	C <sub>3</sub> H <sub>7</sub>	+	CH <sub>2</sub> O	1.95x10 <sup>-26</sup>	255
C <sub>3</sub> H <sub>8</sub>	+	CH <sub>3</sub> O	→	C <sub>3</sub> H <sub>7</sub>	+	CH <sub>3</sub> OH	1.42x10 <sup>-17</sup>	255
C <sub>3</sub> H <sub>8</sub>	+	CH <sub>3</sub> O <sub>2</sub>	→	C <sub>3</sub> H <sub>7</sub>	+	CH <sub>3</sub> OOH	7.69x10 <sup>-26</sup>	255
C <sub>3</sub> H <sub>7</sub>	+	CH <sub>2</sub> O	→	C <sub>3</sub> H <sub>8</sub>	+	CHO	4.10x10 <sup>-18</sup>	255
C <sub>3</sub> H <sub>7</sub>	+	CHO	→	C <sub>3</sub> H <sub>8</sub>	+	CO	1.00x10 <sup>-10</sup>	255
C <sub>3</sub> H <sub>7</sub>	+	CH <sub>3</sub> O	→	C <sub>3</sub> H <sub>8</sub>	+	CH <sub>2</sub> O	4.00x10 <sup>-11</sup>	255
C <sub>3</sub> H <sub>7</sub>	+	CH <sub>3</sub> O <sub>2</sub>	→	C <sub>2</sub> H <sub>5</sub>	+	CH <sub>2</sub> O + CH <sub>3</sub> O	5.99x10 <sup>-11</sup>	255

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H <sub>2</sub>	+	OH	→	H	+	H <sub>2</sub> O	7.02x10 <sup>-15</sup>	268	
H <sub>2</sub>	+	HO <sub>2</sub>	→	H	+	H <sub>2</sub> O <sub>2</sub>	5.43x10 <sup>-30</sup>	253	
H <sub>2</sub>	+	CHO	→	H	+	CH <sub>2</sub> O	2.78x10 <sup>-26</sup>	253	
H <sub>2</sub>	+	CH <sub>3</sub> O <sub>2</sub>	→	H	+	CH <sub>3</sub> OOH	5.43x10 <sup>-30</sup>	253	
H	+	CO <sub>2</sub>	→	CO	+	OH	1.40x10 <sup>-29</sup>	253	
H	+	CO	+ M	→	CHO	+	M	1.54x10 <sup>-34</sup>	114
H	+	H <sub>2</sub> O	→	H <sub>2</sub>	+	OH	5.86x10 <sup>-26</sup>	254	
H	+	OH	→	H <sub>2</sub>	+	O	1.05x10 <sup>-16</sup>	253	
H	+	OH	+ M	→	H <sub>2</sub> O	+	M	4.33x10 <sup>-30</sup>	254
H	+	HO <sub>2</sub>	→	H <sub>2</sub>	+	O <sub>2</sub>	5.60x10 <sup>-12</sup>	268	
H	+	HO <sub>2</sub>	→	H <sub>2</sub> O	+	O	2.40x10 <sup>-12</sup>	268	
H	+	HO <sub>2</sub>	→	OH	+	OH	7.20x10 <sup>-11</sup>	268	
H	+	CH <sub>2</sub> O	→	H <sub>2</sub>	+	CHO	5.72x10 <sup>-14</sup>	114	
H	+	CHO	→	H <sub>2</sub>	+	CO	1.50x10 <sup>-10</sup>	254	
H	+	CH <sub>3</sub> O	→	H <sub>2</sub>	+	CH <sub>2</sub> O	2.32x10 <sup>-11</sup>	264	
H	+	CH <sub>3</sub> O	→	CH <sub>3</sub>	+	OH	9.93x10 <sup>-12</sup>	264	
H	+	CH <sub>3</sub> CHO	→	H <sub>2</sub>	+	CH <sub>3</sub> CO	8.98x10 <sup>-14</sup>	254	
H	+	CH <sub>2</sub> CO	→	CH <sub>3</sub>	+	CO	1.04x10 <sup>-13</sup>	254	
H	+	C <sub>2</sub> HO	→	CH <sub>2</sub>	+	CO	2.50x10 <sup>-10</sup>	254	
H	+	CH <sub>3</sub> O <sub>2</sub>	→	OH	+	CH <sub>3</sub> O	1.60x10 <sup>-10</sup>	253	
O	+	CO	+ M	→	CO <sub>2</sub>	+	M	1.11x10 <sup>-35</sup>	253
O	+	H <sub>2</sub> O	→	OH	+	OH	4.48x10 <sup>-24</sup>	253	
O	+	OH	→	H	+	O <sub>2</sub>	3.46x10 <sup>-11</sup>	268	
O	+	HO <sub>2</sub>	→	O <sub>2</sub>	+	OH	5.70x10 <sup>-11</sup>	268	
O	+	CH <sub>2</sub> O	→	OH	+	CHO	1.73x10 <sup>-13</sup>	254	
O	+	CHO	→	CO	+	OH	5.00x10 <sup>-11</sup>	254	

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O	+	CHO	→	H	+	CO <sub>2</sub>	5.00x10 <sup>-11</sup>	254		
O	+	CH <sub>3</sub> O	→	CH <sub>3</sub>	+	O <sub>2</sub>	2.20x10 <sup>-11</sup>	254		
O	+	CH <sub>3</sub> O	→	OH	+	CH <sub>2</sub> O	3.00x10 <sup>-12</sup>	254		
O	+	CH <sub>3</sub> CHO	→	OH	+	CH <sub>3</sub> CO	4.68x10 <sup>-13</sup>	254		
O	+	CH <sub>2</sub> CO	→	CH <sub>2</sub>	+	CO <sub>2</sub>	2.29x10 <sup>-13</sup>	254, 272		
O	+	CH <sub>2</sub> CO	→	CH <sub>2</sub> O	+	CO	7.88x10 <sup>-14</sup>	254, 272		
O	+	CH <sub>2</sub> CO	→	CHO	+	CO	+	H	4.33x10 <sup>-14</sup>	254, 272
O	+	CH <sub>2</sub> CO	→	CHO	+	CHO	4.33x10 <sup>-14</sup>	254, 272		
O	+	C <sub>2</sub> HO	→	CO	+	CO	+	H	1.60x10 <sup>-10</sup>	254
O	+	CH <sub>3</sub> O <sub>2</sub>	→	CH <sub>3</sub> O	+	O <sub>2</sub>	5.99x10 <sup>-11</sup>	253		
O	+	CH <sub>3</sub> OOH	→	CH <sub>3</sub> O <sub>2</sub>	+	OH	5.63x10 <sup>-15</sup>	264		
O <sub>2</sub>	+	CHO	→	CO	+	HO <sub>2</sub>	5.10x10 <sup>-12</sup>	265		
O <sub>2</sub>	+	CH <sub>3</sub> O	→	CH <sub>2</sub> O	+	HO <sub>2</sub>	1.97x10 <sup>-15</sup>	265		
O <sub>2</sub>	+	CH <sub>2</sub> CHO	→	CH <sub>2</sub> O	+	CO	+	OH	3.00x10 <sup>-14</sup>	254, 273- 274
O <sub>2</sub>	+	C <sub>2</sub> HO	→	CO	+	CO	+	OH	6.46x10 <sup>-13</sup>	254
O <sub>3</sub>	+	OH	→	O <sub>2</sub>	+	HO <sub>2</sub>	7.41x10 <sup>-14</sup>	268		
O <sub>3</sub>	+	HO <sub>2</sub>	→	O <sub>2</sub>	+	O <sub>2</sub>	+	OH	2.05x10 <sup>-15</sup>	268
O <sub>3</sub>	+	CH <sub>3</sub> O <sub>2</sub>	→	CH <sub>3</sub> O	+	O <sub>2</sub>	+	O <sub>2</sub>	1.00x10 <sup>-17</sup>	275
CO	+	OH	→	CO <sub>2</sub>	+	H	1.25x10 <sup>-13</sup>	254		
CO	+	HO <sub>2</sub>	→	CO <sub>2</sub>	+	OH	1.49x10 <sup>-27</sup>	254		
CO	+	CH <sub>3</sub> O	→	CO <sub>2</sub>	+	CH <sub>3</sub>	6.56x10 <sup>-20</sup>	253		
H <sub>2</sub> O	+	CHO	→	CH <sub>2</sub> O	+	OH	9.35x10 <sup>-32</sup>	253		
H <sub>2</sub> O	+	CH <sub>3</sub> O	→	CH <sub>3</sub> OH	+	OH	1.67x10 <sup>-14</sup>	276		

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OH	+	OH		→	H <sub>2</sub> O	+	O		1.47x10 <sup>-12</sup>	268
OH	+	OH	+	M	→	H <sub>2</sub> O <sub>2</sub>	+	M	6.86x10 <sup>-31</sup>	268
OH	+	HO <sub>2</sub>		→	O <sub>2</sub>	+	H <sub>2</sub> O		1.10x10 <sup>-10</sup>	268
OH	+	CH <sub>2</sub> O		→	H <sub>2</sub> O	+	CHO		8.47x10 <sup>-12</sup>	265
OH	+	CHO		→	CO	+	H <sub>2</sub> O		1.70x10 <sup>-10</sup>	254
OH	+	CH <sub>3</sub> O		→	CH <sub>2</sub> O	+	H <sub>2</sub> O		3.00x10 <sup>-11</sup>	253
OH	+	CH <sub>3</sub> CHO		→	CH <sub>3</sub> CO	+	H <sub>2</sub> O		1.49x10 <sup>-11</sup>	265
OH	+	CH <sub>2</sub> CO		→	CO	+	CH <sub>2</sub> OH		1.14x10 <sup>-11</sup>	254, 277
OH	+	CH <sub>3</sub> O <sub>2</sub>		→	CH <sub>3</sub> OH	+	O <sub>2</sub>		1.00x10 <sup>-10</sup>	253
HO <sub>2</sub>	+	HO <sub>2</sub>		→	H <sub>2</sub> O <sub>2</sub>	+	O <sub>2</sub>		1.63x10 <sup>-12</sup>	268
HO <sub>2</sub>	+	CH <sub>2</sub> O		→	CHO	+	H <sub>2</sub> O <sub>2</sub>		1.05x10 <sup>-20</sup>	253
HO <sub>2</sub>	+	CHO		→	OH	+	H	+	CO <sub>2</sub>	5.00x10 <sup>-11</sup> 253
HO <sub>2</sub>	+	CH <sub>3</sub> O		→	CH <sub>2</sub> O	+	H <sub>2</sub> O <sub>2</sub>		5.00x10 <sup>-13</sup>	253
HO <sub>2</sub>	+	CH <sub>3</sub> O <sub>2</sub>		→	CH <sub>3</sub> OOH	+	O <sub>2</sub>		5.12x10 <sup>-12</sup>	265
HO <sub>2</sub>	+	C <sub>2</sub> H <sub>5</sub> O <sub>2</sub>		→	C <sub>2</sub> H <sub>5</sub> OOH	+	O <sub>2</sub>		7.63x10 <sup>-12</sup>	265
CH <sub>2</sub> O	+	CH <sub>3</sub> O		→	CH <sub>3</sub> OH	+	CHO		1.14x10 <sup>-15</sup>	253
CH <sub>2</sub> O	+	CH <sub>3</sub> O <sub>2</sub>		→	CHO	+	CH <sub>3</sub> OOH		1.05x10 <sup>-20</sup>	253
CHO	+	CHO		→	CH <sub>2</sub> O	+	CO		5.00x10 <sup>-11</sup>	254
CHO	+	CH <sub>3</sub> O		→	CH <sub>3</sub> OH	+	CO		1.50x10 <sup>-10</sup>	253
CHO	+	CH <sub>3</sub> O <sub>2</sub>		→	CH <sub>3</sub> O	+	H	+	CO <sub>2</sub>	5.00x10 <sup>-11</sup> 253
CH <sub>3</sub> O	+	CH <sub>3</sub> O		→	CH <sub>2</sub> O	+	CH <sub>3</sub> OH		1.00x10 <sup>-10</sup>	253
CH <sub>3</sub> O	+	CH <sub>3</sub> O <sub>2</sub>		→	CH <sub>2</sub> O	+	CH <sub>3</sub> OOH		5.00x10 <sup>-13</sup>	253
CH <sub>3</sub> O <sub>2</sub>	+	CH <sub>3</sub> O <sub>2</sub>		→	CH <sub>3</sub> OH	+	CH <sub>2</sub> O	+	O <sub>2</sub>	2.19x10 <sup>-13</sup> 265
CH <sub>3</sub> O <sub>2</sub>	+	CH <sub>3</sub> O <sub>2</sub>		→	CH <sub>3</sub> O	+	CH <sub>3</sub> O	+	O <sub>2</sub>	1.29x10 <sup>-13</sup> 265
C <sub>2</sub> H <sub>5</sub> O <sub>2</sub>	+	C <sub>2</sub> H <sub>5</sub> O <sub>2</sub>		→	C <sub>2</sub> H <sub>5</sub> OH	+	CH <sub>3</sub> CHO	+	O <sub>2</sub>	2.43x10 <sup>-14</sup> 265
C <sub>2</sub> H <sub>5</sub> O <sub>2</sub>	+	C <sub>2</sub> H <sub>5</sub> O <sub>2</sub>		→	C <sub>2</sub> H <sub>5</sub> O	+	C <sub>2</sub> H <sub>5</sub> O	+	O <sub>2</sub>	3.97x10 <sup>-14</sup> 265

CH <sub>4</sub>	+	CH <sub>3</sub> CO	→	CH <sub>3</sub> CHO	+	CH <sub>3</sub>	1.14x10 <sup>-29</sup>	253
CH <sub>4</sub>	+	CH <sub>2</sub> OH	→	CH <sub>3</sub> OH	+	CH <sub>3</sub>	2.55x10 <sup>-27</sup>	278
CH <sub>3</sub>	+	H <sub>2</sub> O <sub>2</sub>	→	CH <sub>4</sub>	+	HO <sub>2</sub>	5.46x10 <sup>-14</sup>	253
CH <sub>3</sub>	+	CH <sub>3</sub> OH	→	CH <sub>4</sub>	+	CH <sub>3</sub> O	1.01x10 <sup>-20</sup>	278
CH <sub>3</sub>	+	CH <sub>3</sub> OH	→	CH <sub>4</sub>	+	CH <sub>2</sub> OH	2.66x10 <sup>-20</sup>	278
CH <sub>3</sub>	+	CH <sub>2</sub> OH	→	CH <sub>4</sub>	+	CH <sub>2</sub> O	4.00x10 <sup>-12</sup>	278
CH <sub>3</sub>	+	C <sub>2</sub> H <sub>5</sub> OH	→	CH <sub>4</sub>	+	C <sub>2</sub> H <sub>5</sub> O	3.11x10 <sup>-19</sup>	279
CH <sub>2</sub>	+	H <sub>2</sub> O <sub>2</sub>	→	CH <sub>3</sub>	+	HO <sub>2</sub>	1.00x10 <sup>-14</sup>	253
CH <sub>2</sub>	+	CH <sub>3</sub> CO	→	CH <sub>2</sub> CO	+	CH <sub>3</sub>	3.00x10 <sup>-11</sup>	253
CH <sub>2</sub>	+	CH <sub>3</sub> OH	→	CH <sub>3</sub> O	+	CH <sub>3</sub>	1.01x10 <sup>-20</sup>	278
CH <sub>2</sub>	+	CH <sub>3</sub> OH	→	CH <sub>2</sub> OH	+	CH <sub>3</sub>	2.66x10 <sup>-20</sup>	278
CH <sub>2</sub>	+	CH <sub>2</sub> OH	→	CH <sub>2</sub> O	+	CH <sub>3</sub>	2.00x10 <sup>-12</sup>	278
CH <sub>2</sub>	+	CH <sub>2</sub> OH	→	C <sub>2</sub> H <sub>4</sub>	+	OH	4.00x10 <sup>-11</sup>	278
C <sub>2</sub> H <sub>6</sub>	+	CH <sub>3</sub> CO	→	CH <sub>3</sub> CHO	+	C <sub>2</sub> H <sub>5</sub>	3.32x10 <sup>-26</sup>	253
C <sub>2</sub> H <sub>6</sub>	+	CH <sub>2</sub> OH	→	CH <sub>3</sub> OH	+	C <sub>2</sub> H <sub>5</sub>	5.93x10 <sup>-25</sup>	278
C <sub>2</sub> H <sub>5</sub>	+	H <sub>2</sub> O <sub>2</sub>	→	C <sub>2</sub> H <sub>6</sub>	+	HO <sub>2</sub>	2.83x10 <sup>-15</sup>	253
C <sub>2</sub> H <sub>5</sub>	+	CH <sub>3</sub> OH	→	C <sub>2</sub> H <sub>6</sub>	+	CH <sub>3</sub> O	3.50x10 <sup>-22</sup>	278
C <sub>2</sub> H <sub>5</sub>	+	CH <sub>3</sub> OH	→	C <sub>2</sub> H <sub>6</sub>	+	CH <sub>2</sub> OH	9.49x10 <sup>-22</sup>	278
C <sub>2</sub> H <sub>5</sub>	+	CH <sub>2</sub> OH	→	C <sub>2</sub> H <sub>6</sub>	+	CH <sub>2</sub> O	4.00x10 <sup>-12</sup>	278
C <sub>2</sub> H <sub>5</sub>	+	CH <sub>2</sub> OH	→	CH <sub>3</sub> OH	+	C <sub>2</sub> H <sub>4</sub>	4.00x10 <sup>-12</sup>	278
C <sub>2</sub> H <sub>3</sub>	+	H <sub>2</sub> O <sub>2</sub>	→	C <sub>2</sub> H <sub>4</sub>	+	HO <sub>2</sub>	5.46x10 <sup>-14</sup>	253
C <sub>2</sub> H <sub>3</sub>	+	CH <sub>3</sub> OH	→	C <sub>2</sub> H <sub>4</sub>	+	CH <sub>3</sub> O	1.01x10 <sup>-20</sup>	278
C <sub>2</sub> H <sub>3</sub>	+	CH <sub>3</sub> OH	→	C <sub>2</sub> H <sub>4</sub>	+	CH <sub>2</sub> OH	2.66x10 <sup>-20</sup>	278
C <sub>2</sub> H <sub>3</sub>	+	CH <sub>2</sub> OH	→	C <sub>2</sub> H <sub>4</sub>	+	CH <sub>2</sub> O	5.00x10 <sup>-11</sup>	278
C <sub>2</sub> H <sub>3</sub>	+	CH <sub>2</sub> OH	→	C <sub>3</sub> H <sub>5</sub>	+	OH	2.00x10 <sup>-11</sup>	278
C <sub>2</sub> H <sub>2</sub>	+	CH <sub>2</sub> OH	→	C <sub>2</sub> H <sub>3</sub>	+	CH <sub>2</sub> O	3.32x10 <sup>-19</sup>	278

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$C_2H$	+	$CH_3OH$	$\rightarrow$	$C_2H_2$	+	$CH_3O$	$2.00 \times 10^{-12}$	278
$C_2H$	+	$CH_3OH$	$\rightarrow$	$C_2H_2$	+	$CH_2OH$	$1.00 \times 10^{-11}$	278
$C_2H$	+	$CH_2OH$	$\rightarrow$	$C_2H_2$	+	$CH_2O$	$5.99 \times 10^{-11}$	278
$C_3H_8$	+	$CH_3CO$	$\rightarrow$	$CH_3CHO$	+	$C_3H_7$	$2.60 \times 10^{-26}$	255
$C_3H_8$	+	$CH_2OH$	$\rightarrow$	$CH_3OH$	+	$C_3H_7$	$4.45 \times 10^{-25}$	255
$C_3H_7$	+	$OH$	$\rightarrow$	$C_3H_6$	+	$H_2O$	$4.00 \times 10^{-11}$	255
$C_3H_7$	+	$H_2O_2$	$\rightarrow$	$C_3H_8$	+	$HO_2$	$7.08 \times 10^{-17}$	255
$C_3H_7$	+	$CH_3OH$	$\rightarrow$	$C_3H_8$	+	$CH_3O$	$3.51 \times 10^{-22}$	255
$C_3H_7$	+	$CH_3OH$	$\rightarrow$	$C_3H_8$	+	$CH_2OH$	$8.45 \times 10^{-22}$	255
$C_3H_7$	+	$CH_2OH$	$\rightarrow$	$C_3H_8$	+	$CH_2O$	$1.60 \times 10^{-12}$	255
$C_3H_7$	+	$CH_2OH$	$\rightarrow$	$C_3H_6$	+	$CH_3OH$	$8.00 \times 10^{-13}$	255
$C_3H_6$	+	$O$	$\rightarrow$	$C_3H_5$	+	$OH$	$8.15 \times 10^{-16}$	256
$C_3H_6$	+	$OH$	$\rightarrow$	$C_3H_5$	+	$H_2O$	$7.69 \times 10^{-13}$	256
$C_3H_6$	+	$HO_2$	$\rightarrow$	$C_3H_5$	+	$H_2O_2$	$3.24 \times 10^{-24}$	256
$C_3H_6$	+	$CHO$	$\rightarrow$	$C_3H_5$	+	$CH_2O$	$3.72 \times 10^{-25}$	256
$C_3H_6$	+	$CH_3O$	$\rightarrow$	$C_3H_5$	+	$CH_3OH$	$5.65 \times 10^{-24}$	256
$C_3H_6$	+	$CH_3O_2$	$\rightarrow$	$C_3H_5$	+	$CH_3OOH$	$1.25 \times 10^{-24}$	256
$C_3H_6$	+	$CH_3CO$	$\rightarrow$	$C_3H_5$	+	$CH_3CHO$	$1.18 \times 10^{-24}$	256
$C_3H_6$	+	$CH_2OH$	$\rightarrow$	$C_3H_5$	+	$CH_3OH$	$3.79 \times 10^{-24}$	256
$C_3H_5$	+	$HO_2$	$\rightarrow$	$C_3H_6$	+	$O_2$	$4.40 \times 10^{-12}$	264
$C_3H_5$	+	$H_2O_2$	$\rightarrow$	$C_3H_6$	+	$HO_2$	$1.00 \times 10^{-23}$	256
$C_3H_5$	+	$CH_2O$	$\rightarrow$	$C_3H_6$	+	$CHO$	$6.06 \times 10^{-25}$	256
$C_3H_5$	+	$CHO$	$\rightarrow$	$C_3H_6$	+	$CO$	$1.00 \times 10^{-10}$	256
$C_3H_5$	+	$CH_3O$	$\rightarrow$	$C_3H_6$	+	$CH_2O$	$5.00 \times 10^{-11}$	256
$C_3H_5$	+	$CH_3OH$	$\rightarrow$	$C_3H_6$	+	$CH_2OH$	$5.43 \times 10^{-29}$	256
$C_3H_5$	+	$CH_2OH$	$\rightarrow$	$C_3H_6$	+	$CH_2O$	$3.00 \times 10^{-11}$	256

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H <sub>2</sub>	+	CH <sub>3</sub> CO	→	CH <sub>3</sub> CHO	+	H	3.29x10 <sup>-26</sup>	253		
H <sub>2</sub>	+	CH <sub>2</sub> OH	→	CH <sub>3</sub> OH	+	H	1.89x10 <sup>-23</sup>	278		
H	+	H <sub>2</sub> O <sub>2</sub>	→	H <sub>2</sub> O	+	OH	4.20x10 <sup>-14</sup>	254		
H	+	H <sub>2</sub> O <sub>2</sub>	→	H <sub>2</sub>	+	HO <sub>2</sub>	5.15x10 <sup>-15</sup>	254		
H	+	CH <sub>3</sub> OH	→	CH <sub>2</sub> OH	+	H <sub>2</sub>	1.27x10 <sup>-15</sup>	278		
H	+	CH <sub>3</sub> OH	→	CH <sub>3</sub> O	+	H <sub>2</sub>	3.18x10 <sup>-16</sup>	278		
H	+	CH <sub>2</sub> OH	→	CH <sub>2</sub> O	+	H <sub>2</sub>	1.00x10 <sup>-11</sup>	278		
H	+	CH <sub>2</sub> OH	→	CH <sub>3</sub>	+	OH	1.60x10 <sup>-10</sup>	278		
H	+	CH <sub>2</sub> OH	+	M	→	CH <sub>3</sub> OH	+	M	2.89x10 <sup>-10</sup>	280
									1.18x10 <sup>-29</sup>	b
H	+	C <sub>2</sub> H <sub>5</sub> OH	→	H <sub>2</sub>	+	C <sub>2</sub> H <sub>5</sub> O	2.52x10 <sup>-17</sup>	281		
H	+	CH <sub>3</sub> OOH	→	H <sub>2</sub> O	+	CH <sub>3</sub> O	5.88x10 <sup>-15</sup>	282		
H	+	CH <sub>3</sub> OOH	→	H <sub>2</sub>	+	CH <sub>3</sub> O <sub>2</sub>	7.11x10 <sup>-15</sup>	282		
O	+	H <sub>2</sub> O <sub>2</sub>	→	HO <sub>2</sub>	+	OH	8.91x10 <sup>-16</sup>	264		
O	+	H <sub>2</sub> O <sub>2</sub>	→	O <sub>2</sub>	+	H <sub>2</sub> O	8.91x10 <sup>-16</sup>	264		
O	+	CH <sub>3</sub> CO	→	OH	+	CH <sub>2</sub> CO	8.75x10 <sup>-11</sup>	264		
O	+	CH <sub>3</sub> CO	→	CO <sub>2</sub>	+	CH <sub>3</sub>	2.63x10 <sup>-10</sup>	264		
O	+	CH <sub>3</sub> OH	→	OH	+	CH <sub>2</sub> OH	1.12x10 <sup>-14</sup>	283		
O	+	CH <sub>3</sub> OH	→	OH	+	CH <sub>3</sub> O	1.68x10 <sup>-15</sup>	283		
O	+	CH <sub>2</sub> OH	→	CH <sub>2</sub> O	+	OH	7.00x10 <sup>-11</sup>	278		
O	+	C <sub>2</sub> H <sub>5</sub> OOH	→	C <sub>2</sub> H <sub>5</sub> O <sub>2</sub>	+	OH	5.19x10 <sup>-14</sup>	264		
O <sub>2</sub>	+	CH <sub>2</sub> OH	→	CH <sub>2</sub> O	+	HO <sub>2</sub>	9.70x10 <sup>-12</sup>	265		
O <sub>2</sub>	+	C <sub>2</sub> H <sub>5</sub> O	→	CH <sub>3</sub> CHO	+	HO <sub>2</sub>	8.12x10 <sup>-15</sup>	265		
OH	+	H <sub>2</sub> O <sub>2</sub>	→	HO <sub>2</sub>	+	H <sub>2</sub> O	1.70x10 <sup>-12</sup>	268		
OH	+	CH <sub>3</sub> CO	→	CH <sub>2</sub> CO	+	H <sub>2</sub> O	2.00x10 <sup>-11</sup>	253		
OH	+	CH <sub>3</sub> CO	→	CH <sub>3</sub>	+	CO	+	OH	5.00x10 <sup>-11</sup>	253



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OH	+	CH <sub>3</sub> OH	→	H <sub>2</sub> O	+	CH <sub>2</sub> OH	7.67x10 <sup>-13</sup>	265
OH	+	CH <sub>3</sub> OH	→	H <sub>2</sub> O	+	CH <sub>3</sub> O	1.35x10 <sup>-13</sup>	265
OH	+	CH <sub>2</sub> OH	→	CH <sub>2</sub> O	+	H <sub>2</sub> O	4.00x10 <sup>-11</sup>	278
OH	+	C <sub>2</sub> H <sub>5</sub> OH	→	H <sub>2</sub> O	+	C <sub>2</sub> H <sub>5</sub> O	1.60x10 <sup>-13</sup>	265
OH	+	CH <sub>3</sub> OOH	→	H <sub>2</sub> O	+	CH <sub>3</sub> O <sub>2</sub>	3.55x10 <sup>-12</sup>	265
OH	+	C <sub>2</sub> H <sub>5</sub> OOH	→	H <sub>2</sub> O	+	C <sub>2</sub> H <sub>5</sub> O <sub>2</sub>	2.83x10 <sup>-12</sup>	254
HO <sub>2</sub>	+	CH <sub>3</sub> CO	→	CH <sub>3</sub>	+	CO <sub>2</sub> + OH	5.00x10 <sup>-11</sup>	253
HO <sub>2</sub>	+	CH <sub>3</sub> OH	→	CH <sub>2</sub> OH	+	H <sub>2</sub> O <sub>2</sub>	1.10x10 <sup>-22</sup>	278
HO <sub>2</sub>	+	CH <sub>2</sub> OH	→	CH <sub>2</sub> O	+	H <sub>2</sub> O <sub>2</sub>	2.00x10 <sup>-11</sup>	278
CH <sub>2</sub> O	+	CH <sub>3</sub> CO	→	CH <sub>3</sub> CHO	+	CHO	1.17x10 <sup>-22</sup>	253
CH <sub>2</sub> O	+	CH <sub>2</sub> OH	→	CH <sub>3</sub> OH	+	CHO	4.22x10 <sup>-18</sup>	278
CHO	+	H <sub>2</sub> O <sub>2</sub>	→	CH <sub>2</sub> O	+	HO <sub>2</sub>	1.50x10 <sup>-18</sup>	253
CHO	+	CH <sub>3</sub> CO	→	CH <sub>3</sub> CHO	+	CO	1.50x10 <sup>-11</sup>	253
CHO	+	CH <sub>3</sub> OH	→	CH <sub>2</sub> O	+	CH <sub>2</sub> OH	6.85x10 <sup>-23</sup>	278
CHO	+	CH <sub>2</sub> OH	→	CH <sub>2</sub> O	+	CH <sub>2</sub> O	3.00x10 <sup>-10</sup>	278
CHO	+	CH <sub>2</sub> OH	→	CH <sub>3</sub> OH	+	CO	2.00x10 <sup>-10</sup>	278
CH <sub>3</sub> O	+	CH <sub>3</sub> CO	→	CH <sub>3</sub> OH	+	CH <sub>2</sub> CO	1.00x10 <sup>-11</sup>	253
CH <sub>3</sub> O	+	CH <sub>3</sub> OH	→	CH <sub>3</sub> OH	+	CH <sub>2</sub> OH	5.38x10 <sup>-16</sup>	278
CH <sub>3</sub> O	+	CH <sub>2</sub> OH	→	CH <sub>2</sub> O	+	CH <sub>3</sub> OH	4.00x10 <sup>-11</sup>	278
CH <sub>3</sub> O <sub>2</sub>	+	H <sub>2</sub> O <sub>2</sub>	→	CH <sub>3</sub> OOH	+	HO <sub>2</sub>	2.31x10 <sup>-19</sup>	253
CH <sub>3</sub> O <sub>2</sub>	+	CH <sub>3</sub> CO	→	CH <sub>3</sub>	+	CO <sub>2</sub> + CH <sub>3</sub> O	4.00x10 <sup>-11</sup>	253
CH <sub>3</sub> O <sub>2</sub>	+	CH <sub>3</sub> OH	→	CH <sub>2</sub> OH	+	CH <sub>3</sub> OOH	3.08x10 <sup>-22</sup>	278
CH <sub>3</sub> O <sub>2</sub>	+	CH <sub>2</sub> OH	→	CH <sub>3</sub> O	+	OH + CH <sub>2</sub> O	2.00x10 <sup>-11</sup>	278
H <sub>2</sub> O <sub>2</sub>	+	CH <sub>3</sub> CO	→	CH <sub>3</sub> CHO	+	HO <sub>2</sub>	3.05x10 <sup>-19</sup>	253
H <sub>2</sub> O <sub>2</sub>	+	CH <sub>2</sub> OH	→	CH <sub>3</sub> OH	+	HO <sub>2</sub>	6.56x10 <sup>-17</sup>	278
CH <sub>3</sub> CO	+	CH <sub>3</sub> OH	→	CH <sub>3</sub> CHO	+	CH <sub>2</sub> OH	2.22x10 <sup>-22</sup>	278

Appendices Table A.3.

$\text{CH}_3\text{OH}$	+	$\text{CH}_2\text{OH}$	$\rightarrow$	$\text{CH}_3\text{OH}$	+	$\text{CH}_3\text{O}$	$2.12 \times 10^{-23}$	<sup>278</sup>
$\text{CH}_2\text{OH}$	+	$\text{CH}_2\text{OH}$	$\rightarrow$	$\text{CH}_2\text{O}$	+	$\text{CH}_3\text{OH}$	$8.00 \times 10^{-12}$	<sup>278</sup>



**Table A.4.** Ion-neutral and ion-ion reactions included in the model, as well as the corresponding rate coefficients and the references where these data were adopted from. The rate coefficients are expressed in  $\text{cm}^3 \text{s}^{-1}$  and  $\text{cm}^6 \text{s}^{-1}$  for two-body and three-body reactions, respectively.

$\text{CH}_5^+$	+	$\text{CH}_2$	$\rightarrow$	$\text{CH}_3^+$	+	$\text{CH}_4$	$9.60 \times 10^{-10}$	284
$\text{CH}_5^+$	+	$\text{CH}$	$\rightarrow$	$\text{CH}_2^+$	+	$\text{CH}_4$	$6.90 \times 10^{-10}$	284
$\text{CH}_5^+$	+	$\text{C}$	$\rightarrow$	$\text{CH}^+$	+	$\text{CH}_4$	$1.20 \times 10^{-09}$	284
$\text{CH}_5^+$	+	$\text{C}_2\text{H}_6$	$\rightarrow$	$\text{C}_2\text{H}_5^+$	+	$\text{H}_2 + \text{CH}_4$	$2.25 \times 10^{-10}$	285
$\text{CH}_5^+$	+	$\text{C}_2\text{H}_4$	$\rightarrow$	$\text{C}_2\text{H}_5^+$	+	$\text{CH}_4$	$1.50 \times 10^{-09}$	284
$\text{CH}_5^+$	+	$\text{C}_2\text{H}_2$	$\rightarrow$	$\text{C}_2\text{H}_3^+$	+	$\text{CH}_4$	$1.60 \times 10^{-09}$	284
$\text{CH}_5^+$	+	$\text{C}_2\text{H}$	$\rightarrow$	$\text{C}_2\text{H}_2^+$	+	$\text{CH}_4$	$9.00 \times 10^{-10}$	284
$\text{CH}_5^+$	+	$\text{C}_2$	$\rightarrow$	$\text{C}_2\text{H}^+$	+	$\text{CH}_4$	$9.50 \times 10^{-10}$	284
$\text{CH}_5^+$	+	$\text{H}$	$\rightarrow$	$\text{CH}_4^+$	+	$\text{H}_2$	$1.50 \times 10^{-10}$	284
$\text{CH}_5^+$	+	$\text{O}$	$\rightarrow$	$\text{H}_3\text{O}^+$	+	$\text{CH}_2$	$2.20 \times 10^{-10}$	284
$\text{CH}_5^+$	+	$\text{H}_2\text{O}$	$\rightarrow$	$\text{H}_3\text{O}^+$	+	$\text{CH}_4$	$3.70 \times 10^{-09}$	284
$\text{CH}_5^+$	+	$\text{OH}$	$\rightarrow$	$\text{H}_2\text{O}^+$	+	$\text{CH}_4$	$7.00 \times 10^{-10}$	284
$\text{CH}_4^+$	+	$\text{CH}_4$	$\rightarrow$	$\text{CH}_5^+$	+	$\text{CH}_3$	$1.50 \times 10^{-09}$	284
$\text{CH}_4^+$	+	$\text{C}_2\text{H}_6$	$\rightarrow$	$\text{C}_2\text{H}_4^+$	+	$\text{CH}_4 + \text{H}_2$	$1.91 \times 10^{-09}$	285
$\text{CH}_4^+$	+	$\text{C}_2\text{H}_4$	$\rightarrow$	$\text{C}_2\text{H}_5^+$	+	$\text{CH}_3$	$4.23 \times 10^{-10}$	284
$\text{CH}_4^+$	+	$\text{C}_2\text{H}_4$	$\rightarrow$	$\text{C}_2\text{H}_4^+$	+	$\text{CH}_4$	$1.38 \times 10^{-09}$	284
$\text{CH}_4^+$	+	$\text{C}_2\text{H}_2$	$\rightarrow$	$\text{C}_2\text{H}_3^+$	+	$\text{CH}_3$	$1.23 \times 10^{-09}$	284
$\text{CH}_4^+$	+	$\text{C}_2\text{H}_2$	$\rightarrow$	$\text{C}_2\text{H}_2^+$	+	$\text{CH}_4$	$1.13 \times 10^{-09}$	284
$\text{CH}_4^+$	+	$\text{H}_2$	$\rightarrow$	$\text{CH}_5^+$	+	$\text{H}$	$3.30 \times 10^{-11}$	284
$\text{CH}_4^+$	+	$\text{H}$	$\rightarrow$	$\text{CH}_3^+$	+	$\text{H}_2$	$1.00 \times 10^{-11}$	284
$\text{CH}_4^+$	+	$\text{O}$	$\rightarrow$	$\text{CH}_3^+$	+	$\text{OH}$	$1.00 \times 10^{-09}$	284
$\text{CH}_4^+$	+	$\text{O}_2$	$\rightarrow$	$\text{O}_2^+$	+	$\text{CH}_4$	$3.90 \times 10^{-10}$	284

Appendices Table A.4.

$\text{CH}_4^+$	+	$\text{H}_2\text{O}$	$\rightarrow$	$\text{H}_3\text{O}^+$	+	$\text{CH}_3$	$2.60 \times 10^{-09}$	284
$\text{CH}_3^+$	+	$\text{CH}_4$	$\rightarrow$	$\text{CH}_4^+$	+	$\text{CH}_3$	$1.36 \times 10^{-10}$	286
$\text{CH}_3^+$	+	$\text{CH}_4$	$\rightarrow$	$\text{C}_2\text{H}_5^+$	+	$\text{H}_2$	$1.20 \times 10^{-09}$	284
$\text{CH}_3^+$	+	$\text{CH}_2$	$\rightarrow$	$\text{C}_2\text{H}_3^+$	+	$\text{H}_2$	$9.90 \times 10^{-10}$	284
$\text{CH}_3^+$	+	$\text{CH}$	$\rightarrow$	$\text{C}_2\text{H}_2^+$	+	$\text{H}_2$	$7.10 \times 10^{-10}$	284
$\text{CH}_3^+$	+	$\text{C}$	$\rightarrow$	$\text{C}_2\text{H}^+$	+	$\text{H}_2$	$1.20 \times 10^{-09}$	284
$\text{CH}_3^+$	+	$\text{C}_2\text{H}_6$	$\rightarrow$	$\text{C}_2\text{H}_5^+$	+	$\text{CH}_4$	$1.48 \times 10^{-09}$	284
$\text{CH}_3^+$	+	$\text{C}_2\text{H}_4$	$\rightarrow$	$\text{C}_2\text{H}_3^+$	+	$\text{CH}_4$	$3.50 \times 10^{-10}$	284
$\text{CH}_3^+$	+	$\text{C}_2\text{H}_3$	$\rightarrow$	$\text{C}_2\text{H}_3^+$	+	$\text{CH}_3$	$3.00 \times 10^{-10}$	284
$\text{CH}_2^+$	+	$\text{CH}_4$	$\rightarrow$	$\text{CH}_3^+$	+	$\text{CH}_3$	$1.38 \times 10^{-10}$	81
$\text{CH}_2^+$	+	$\text{CH}_4$	$\rightarrow$	$\text{C}_2\text{H}_5^+$	+	$\text{H}$	$3.60 \times 10^{-10}$	284
$\text{CH}_2^+$	+	$\text{CH}_4$	$\rightarrow$	$\text{C}_2\text{H}_4^+$	+	$\text{H}_2$	$8.40 \times 10^{-10}$	284
$\text{CH}_2^+$	+	$\text{CH}_4$	$\rightarrow$	$\text{C}_2\text{H}_3^+$	+	$\text{H}_2 + \text{H}$	$2.31 \times 10^{-10}$	81
$\text{CH}_2^+$	+	$\text{CH}_4$	$\rightarrow$	$\text{C}_2\text{H}_2^+$	+	$2\text{H}_2$	$3.97 \times 10^{-10}$	81
$\text{CH}_2^+$	+	$\text{C}$	$\rightarrow$	$\text{C}_2\text{H}^+$	+	$\text{H}$	$1.20 \times 10^{-09}$	284
$\text{CH}_2^+$	+	$\text{H}_2$	$\rightarrow$	$\text{CH}_3^+$	+	$\text{H}$	$1.60 \times 10^{-09}$	284
$\text{CH}^+$	+	$\text{CH}_4$	$\rightarrow$	$\text{C}_2\text{H}_4^+$	+	$\text{H}$	$6.50 \times 10^{-11}$	284
$\text{CH}^+$	+	$\text{CH}_4$	$\rightarrow$	$\text{C}_2\text{H}_3^+$	+	$\text{H}_2$	$1.09 \times 10^{-09}$	284
$\text{CH}^+$	+	$\text{CH}_4$	$\rightarrow$	$\text{C}_2\text{H}_2^+$	+	$\text{H}_2 + \text{H}$	$1.43 \times 10^{-10}$	284
$\text{CH}^+$	+	$\text{CH}_2$	$\rightarrow$	$\text{C}_2\text{H}^+$	+	$\text{H}_2$	$1.00 \times 10^{-09}$	284
$\text{CH}^+$	+	$\text{CH}$	$\rightarrow$	$\text{C}_2^+$	+	$\text{H}_2$	$7.40 \times 10^{-10}$	284
$\text{CH}^+$	+	$\text{C}$	$\rightarrow$	$\text{C}_2^+$	+	$\text{H}$	$1.20 \times 10^{-09}$	284
$\text{CH}^+$	+	$\text{H}_2$	$\rightarrow$	$\text{CH}_2^+$	+	$\text{H}$	$1.20 \times 10^{-09}$	284
$\text{CH}^+$	+	$\text{H}$	$\rightarrow$	$\text{C}^+$	+	$\text{H}_2$	$7.50 \times 10^{-10}$	284
$\text{CH}^+$	+	$\text{O}$	$\rightarrow$	$\text{CO}^+$	+	$\text{H}$	$3.50 \times 10^{-10}$	284
$\text{CH}^+$	+	$\text{O}_2$	$\rightarrow$	$\text{CO}^+$	+	$\text{OH}$	$1.00 \times 10^{-11}$	284

$\text{CH}^+$	+	$\text{O}_2$	$\rightarrow$	$\text{O}^+$	+	$\text{CHO}$	$1.00 \times 10^{-11}$	284
$\text{CH}^+$	+	$\text{H}_2\text{O}$	$\rightarrow$	$\text{H}_3\text{O}^+$	+	$\text{C}$	$5.80 \times 10^{-10}$	284
$\text{CH}^+$	+	$\text{OH}$	$\rightarrow$	$\text{CO}^+$	+	$\text{H}_2$	$7.50 \times 10^{-10}$	284
$\text{C}^+$	+	$\text{CH}_4$	$\rightarrow$	$\text{C}_2\text{H}_3^+$	+	$\text{H}$	$1.10 \times 10^{-09}$	284
$\text{C}^+$	+	$\text{CH}_4$	$\rightarrow$	$\text{C}_2\text{H}_2^+$	+	$\text{H}_2$	$4.00 \times 10^{-10}$	284
$\text{C}^+$	+	$\text{CH}_3$	$\rightarrow$	$\text{C}_2\text{H}_2^+$	+	$\text{H}$	$1.30 \times 10^{-09}$	284
$\text{C}^+$	+	$\text{CH}_3$	$\rightarrow$	$\text{C}_2\text{H}^+$	+	$\text{H}_2$	$1.00 \times 10^{-09}$	284
$\text{C}^+$	+	$\text{CH}_2$	$\rightarrow$	$\text{CH}_2^+$	+	$\text{C}$	$5.20 \times 10^{-10}$	284
$\text{C}^+$	+	$\text{CH}_2$	$\rightarrow$	$\text{C}_2\text{H}^+$	+	$\text{H}$	$5.20 \times 10^{-10}$	284
$\text{C}^+$	+	$\text{CH}$	$\rightarrow$	$\text{CH}^+$	+	$\text{C}$	$3.80 \times 10^{-10}$	284
$\text{C}^+$	+	$\text{CH}$	$\rightarrow$	$\text{C}_2^+$	+	$\text{H}$	$3.80 \times 10^{-10}$	284
$\text{C}^+$	+	$\text{C}_2\text{H}_6$	$\rightarrow$	$\text{C}_2\text{H}_5^+$	+	$\text{CH}$	$2.31 \times 10^{-10}$	284
$\text{C}^+$	+	$\text{C}_2\text{H}_6$	$\rightarrow$	$\text{C}_2\text{H}_4^+$	+	$\text{CH}_2$	$1.16 \times 10^{-10}$	284
$\text{C}^+$	+	$\text{C}_2\text{H}_6$	$\rightarrow$	$\text{C}_2\text{H}_3^+$	+	$\text{CH}_3$	$4.95 \times 10^{-10}$	284
$\text{C}^+$	+	$\text{C}_2\text{H}_6$	$\rightarrow$	$\text{C}_2\text{H}_2^+$	+	$\text{CH}_4$	$8.25 \times 10^{-11}$	284
$\text{C}^+$	+	$\text{C}_2\text{H}_5$	$\rightarrow$	$\text{C}_2\text{H}_5^+$	+	$\text{C}$	$5.00 \times 10^{-10}$	284
$\text{C}^+$	+	$\text{C}_2\text{H}_4$	$\rightarrow$	$\text{C}_2\text{H}_4^+$	+	$\text{C}$	$1.70 \times 10^{-11}$	284
$\text{C}^+$	+	$\text{C}_2\text{H}_4$	$\rightarrow$	$\text{C}_2\text{H}_3^+$	+	$\text{CH}$	$8.50 \times 10^{-11}$	284
$\text{C}^+$	+	$\text{O}_2$	$\rightarrow$	$\text{O}^+$	+	$\text{CO}$	$6.20 \times 10^{-10}$	284
$\text{C}^+$	+	$\text{O}_2$	$\rightarrow$	$\text{CO}^+$	+	$\text{O}$	$3.80 \times 10^{-10}$	284
$\text{C}^+$	+	$\text{OH}$	$\rightarrow$	$\text{CO}^+$	+	$\text{H}$	$7.70 \times 10^{-10}$	284
$\text{C}^+$	+	$\text{CO}_2$	$\rightarrow$	$\text{CO}^+$	+	$\text{CO}$	$1.10 \times 10^{-09}$	284
$\text{C}^+$	+	$\text{H}^-$	$\rightarrow$	$\text{C}$	+	$\text{H}$	$2.30 \times 10^{-07}$	284
$\text{C}_2\text{H}_6^+$	+	$\text{C}_2\text{H}_4$	$\rightarrow$	$\text{C}_2\text{H}_4^+$	+	$\text{C}_2\text{H}_6$	$1.15 \times 10^{-09}$	284
$\text{C}_2\text{H}_6^+$	+	$\text{C}_2\text{H}_2$	$\rightarrow$	$\text{C}_2\text{H}_5^+$	+	$\text{C}_2\text{H}_3$	$2.47 \times 10^{-10}$	284
$\text{C}_2\text{H}_6^+$	+	$\text{H}$	$\rightarrow$	$\text{C}_2\text{H}_5^+$	+	$\text{H}_2$	$1.00 \times 10^{-10}$	284

Appendices Table A.4.

$C_2H_6^+$	+	$H_2O$	$\rightarrow$	$H_3O^+$	+	$C_2H_5$	$2.95 \times 10^{-09}$	284
$C_2H_5^+$	+	$H$	$\rightarrow$	$C_2H_4^+$	+	$H_2$	$1.00 \times 10^{-11}$	284
$C_2H_5^+$	+	$H_2O$	$\rightarrow$	$H_3O^+$	+	$C_2H_4$	$1.40 \times 10^{-09}$	284
$C_2H_4^+$	+	$C_2H_3$	$\rightarrow$	$C_2H_5^+$	+	$C_2H_2$	$5.00 \times 10^{-10}$	284
$C_2H_4^+$	+	$C_2H_3$	$\rightarrow$	$C_2H_3^+$	+	$C_2H_4$	$5.00 \times 10^{-10}$	284
$C_2H_4^+$	+	$H$	$\rightarrow$	$C_2H_3^+$	+	$H_2$	$3.00 \times 10^{-10}$	284
$C_2H_4^+$	+	$O$	$\rightarrow$	$CH_3^+$	+	$CHO$	$1.08 \times 10^{-10}$	284
$C_2H_3^+$	+	$C_2H_6$	$\rightarrow$	$C_2H_5^+$	+	$C_2H_4$	$2.91 \times 10^{-10}$	284
$C_2H_3^+$	+	$C_2H_4$	$\rightarrow$	$C_2H_5^+$	+	$C_2H_2$	$8.90 \times 10^{-10}$	284
$C_2H_3^+$	+	$C_2H_3$	$\rightarrow$	$C_2H_5^+$	+	$C_2H$	$5.00 \times 10^{-10}$	284
$C_2H_3^+$	+	$C_2H$	$\rightarrow$	$C_2H_2^+$	+	$C_2H_2$	$3.30 \times 10^{-10}$	284
$C_2H_3^+$	+	$H$	$\rightarrow$	$C_2H_2^+$	+	$H_2$	$6.80 \times 10^{-11}$	284
$C_2H_3^+$	+	$H_2O$	$\rightarrow$	$H_3O^+$	+	$C_2H_2$	$1.11 \times 10^{-09}$	284
$C_2H_2^+$	+	$CH_4$	$\rightarrow$	$C_2H_3^+$	+	$CH_3$	$4.10 \times 10^{-09}$	81
$C_2H_2^+$	+	$C_2H_6$	$\rightarrow$	$C_2H_5^+$	+	$C_2H_3$	$1.31 \times 10^{-10}$	285
$C_2H_2^+$	+	$C_2H_6$	$\rightarrow$	$C_2H_4^+$	+	$C_2H_4$	$2.48 \times 10^{-10}$	284
$C_2H_2^+$	+	$C_2H_4$	$\rightarrow$	$C_2H_4^+$	+	$C_2H_2$	$4.14 \times 10^{-10}$	284
$C_2H_2^+$	+	$C_2H_3$	$\rightarrow$	$C_2H_3^+$	+	$C_2H_2$	$3.30 \times 10^{-10}$	284
$C_2H_2^+$	+	$H_2$	$\rightarrow$	$C_2H_3^+$	+	$H$	$1.00 \times 10^{-11}$	284
$C_2H_2^+$	+	$H_2O$	$\rightarrow$	$H_3O^+$	+	$C_2H$	$2.20 \times 10^{-10}$	284
$C_2H^+$	+	$CH_4$	$\rightarrow$	$C_2H_2^+$	+	$CH_3$	$3.74 \times 10^{-10}$	284
$C_2H^+$	+	$CH_2$	$\rightarrow$	$CH_3^+$	+	$C_2$	$4.40 \times 10^{-10}$	284
$C_2H^+$	+	$CH$	$\rightarrow$	$CH_2^+$	+	$C_2$	$3.20 \times 10^{-10}$	284
$C_2H^+$	+	$H_2$	$\rightarrow$	$C_2H_2^+$	+	$H$	$1.10 \times 10^{-09}$	284
$C_2^+$	+	$CH_4$	$\rightarrow$	$C_2H_2^+$	+	$CH_2$	$1.82 \times 10^{-10}$	284
$C_2^+$	+	$CH_4$	$\rightarrow$	$C_2H^+$	+	$CH_3$	$2.38 \times 10^{-10}$	284

$C_2^+$	+	$CH_2$	$\rightarrow$	$CH_2^+$	+	$C_2$	$4.50 \times 10^{-10}$	284
$C_2^+$	+	$CH$	$\rightarrow$	$CH^+$	+	$C_2$	$3.20 \times 10^{-10}$	284
$C_2^+$	+	$C$	$\rightarrow$	$C^+$	+	$C_2$	$1.10 \times 10^{-10}$	284
$C_2^+$	+	$H_2$	$\rightarrow$	$C_2H^+$	+	$H$	$1.10 \times 10^{-9}$	284
$C_2^+$	+	$O$	$\rightarrow$	$CO^+$	+	$C$	$3.10 \times 10^{-10}$	284
$C_2^+$	+	$O_2$	$\rightarrow$	$CO^+$	+	$CO$	$8.00 \times 10^{-10}$	284
$C_2^+$	+	$H_2O$	$\rightarrow$	$C_2H^+$	+	$OH$	$4.40 \times 10^{-10}$	284
$C_2^+$	+	$OH$	$\rightarrow$	$OH^+$	+	$C_2$	$6.50 \times 10^{-10}$	284
$H_3^+$	+	$CH_4$	$\rightarrow$	$CH_5^+$	+	$H_2$	$2.40 \times 10^{-9}$	284
$H_3^+$	+	$CH_3$	$\rightarrow$	$CH_4^+$	+	$H_2$	$2.10 \times 10^{-9}$	284
$H_3^+$	+	$CH_2$	$\rightarrow$	$CH_3^+$	+	$H_2$	$1.70 \times 10^{-9}$	284
$H_3^+$	+	$CH$	$\rightarrow$	$CH_2^+$	+	$H_2$	$1.20 \times 10^{-9}$	284
$H_3^+$	+	$C$	$\rightarrow$	$CH^+$	+	$H_2$	$2.00 \times 10^{-9}$	284
$H_3^+$	+	$C_2H_6$	$\rightarrow$	$C_2H_5^+$	+	$2H_2$	$2.40 \times 10^{-9}$	284
$H_3^+$	+	$C_2H_5$	$\rightarrow$	$C_2H_6^+$	+	$H_2$	$1.40 \times 10^{-9}$	284
$H_3^+$	+	$C_2H_4$	$\rightarrow$	$C_2H_5^+$	+	$H_2$	$1.15 \times 10^{-9}$	284
$H_3^+$	+	$C_2H_4$	$\rightarrow$	$C_2H_3^+$	+	$2H_2$	$1.15 \times 10^{-9}$	284
$H_3^+$	+	$C_2H_3$	$\rightarrow$	$C_2H_4^+$	+	$H_2$	$2.00 \times 10^{-9}$	284
$H_3^+$	+	$C_2H_2$	$\rightarrow$	$C_2H_3^+$	+	$H_2$	$3.50 \times 10^{-9}$	284
$H_3^+$	+	$C_2H$	$\rightarrow$	$C_2H_2^+$	+	$H_2$	$1.70 \times 10^{-9}$	284
$H_3^+$	+	$C_2$	$\rightarrow$	$C_2H^+$	+	$H_2$	$1.80 \times 10^{-9}$	284
$H_3^+$	+	$O$	$\rightarrow$	$OH^+$	+	$H_2$	$8.40 \times 10^{-10}$	284
$H_3^+$	+	$O$	$\rightarrow$	$H_2O^+$	+	$H$	$3.60 \times 10^{-10}$	284
$H_3^+$	+	$OH$	$\rightarrow$	$H_2O^+$	+	$H_2$	$1.30 \times 10^{-9}$	284
$H_3^+$	+	$H_2O$	$\rightarrow$	$H_3O^+$	+	$H_2$	$5.90 \times 10^{-9}$	284
$H_3^+$	+	$H^-$	$\rightarrow$	$H_2$	+	$H_2$	$2.30 \times 10^{-7}$	284



Appendices Table A.4.

$\text{H}_2^+$	+	$\text{CH}_4$	$\rightarrow$	$\text{CH}_5^+$	+	$\text{H}$	$1.14 \times 10^{-10}$	284
$\text{H}_2^+$	+	$\text{CH}_4$	$\rightarrow$	$\text{CH}_4^+$	+	$\text{H}_2$	$1.40 \times 10^{-09}$	284
$\text{H}_2^+$	+	$\text{CH}_4$	$\rightarrow$	$\text{CH}_3^+$	+	$\text{H}_2 + \text{H}$	$2.30 \times 10^{-09}$	284
$\text{H}_2^+$	+	$\text{CH}_2$	$\rightarrow$	$\text{CH}_3^+$	+	$\text{H}$	$1.00 \times 10^{-09}$	284
$\text{H}_2^+$	+	$\text{CH}_2$	$\rightarrow$	$\text{CH}_2^+$	+	$\text{H}_2$	$1.00 \times 10^{-09}$	284
$\text{H}_2^+$	+	$\text{CH}$	$\rightarrow$	$\text{CH}_2^+$	+	$\text{H}$	$7.10 \times 10^{-10}$	284
$\text{H}_2^+$	+	$\text{CH}$	$\rightarrow$	$\text{CH}^+$	+	$\text{H}_2$	$7.10 \times 10^{-10}$	284
$\text{H}_2^+$	+	$\text{C}$	$\rightarrow$	$\text{CH}^+$	+	$\text{H}$	$2.40 \times 10^{-09}$	284
$\text{H}_2^+$	+	$\text{C}_2\text{H}_6$	$\rightarrow$	$\text{C}_2\text{H}_6^+$	+	$\text{H}_2$	$2.94 \times 10^{-10}$	284
$\text{H}_2^+$	+	$\text{C}_2\text{H}_6$	$\rightarrow$	$\text{C}_2\text{H}_5^+$	+	$\text{H}_2 + \text{H}$	$1.37 \times 10^{-09}$	284
$\text{H}_2^+$	+	$\text{C}_2\text{H}_6$	$\rightarrow$	$\text{C}_2\text{H}_4^+$	+	$2\text{H}_2$	$2.35 \times 10^{-09}$	284
$\text{H}_2^+$	+	$\text{C}_2\text{H}_6$	$\rightarrow$	$\text{C}_2\text{H}_3^+$	+	$2\text{H}_2 + \text{H}$	$6.86 \times 10^{-10}$	285
$\text{H}_2^+$	+	$\text{C}_2\text{H}_6$	$\rightarrow$	$\text{C}_2\text{H}_2^+$	+	$3\text{H}_2$	$1.96 \times 10^{-10}$	285
$\text{H}_2^+$	+	$\text{C}_2\text{H}_4$	$\rightarrow$	$\text{C}_2\text{H}_4^+$	+	$\text{H}_2$	$2.21 \times 10^{-09}$	284
$\text{H}_2^+$	+	$\text{C}_2\text{H}_4$	$\rightarrow$	$\text{C}_2\text{H}_3^+$	+	$\text{H}_2 + \text{H}$	$1.81 \times 10^{-09}$	284
$\text{H}_2^+$	+	$\text{C}_2\text{H}_4$	$\rightarrow$	$\text{C}_2\text{H}_2^+$	+	$2\text{H}_2$	$8.82 \times 10^{-10}$	284
$\text{H}_2^+$	+	$\text{C}_2\text{H}_2$	$\rightarrow$	$\text{C}_2\text{H}_3^+$	+	$\text{H}$	$4.80 \times 10^{-10}$	284
$\text{H}_2^+$	+	$\text{C}_2\text{H}_2$	$\rightarrow$	$\text{C}_2\text{H}_2^+$	+	$\text{H}_2$	$4.82 \times 10^{-09}$	284
$\text{H}_2^+$	+	$\text{C}_2\text{H}$	$\rightarrow$	$\text{C}_2\text{H}_2^+$	+	$\text{H}$	$1.00 \times 10^{-09}$	284
$\text{H}_2^+$	+	$\text{C}_2\text{H}$	$\rightarrow$	$\text{C}_2\text{H}^+$	+	$\text{H}_2$	$1.00 \times 10^{-09}$	284
$\text{H}_2^+$	+	$\text{C}_2$	$\rightarrow$	$\text{C}_2\text{H}^+$	+	$\text{H}$	$1.10 \times 10^{-09}$	284
$\text{H}_2^+$	+	$\text{C}_2$	$\rightarrow$	$\text{C}_2^+$	+	$\text{H}_2$	$1.10 \times 10^{-09}$	284
$\text{H}_2^+$	+	$\text{H}_2$	$\rightarrow$	$\text{H}_3^+$	+	$\text{H}$	$2.08 \times 10^{-09}$	284
$\text{H}_2^+$	+	$\text{H}$	$\rightarrow$	$\text{H}^+$	+	$\text{H}_2$	$6.40 \times 10^{-10}$	284
$\text{H}_2^+$	+	$\text{O}$	$\rightarrow$	$\text{OH}^+$	+	$\text{H}$	$1.50 \times 10^{-09}$	284
$\text{H}_2^+$	+	$\text{O}_2$	$\rightarrow$	$\text{O}_2^+$	+	$\text{H}_2$	$8.00 \times 10^{-10}$	284

$\text{H}_2^+$	+	OH	$\rightarrow$	$\text{OH}^+$	+	$\text{H}_2$	$7.60 \times 10^{-10}$	284
$\text{H}_2^+$	+	OH	$\rightarrow$	$\text{H}_2\text{O}^+$	+	H	$7.60 \times 10^{-10}$	284
$\text{H}_2^+$	+	$\text{H}_2\text{O}$	$\rightarrow$	$\text{H}_2\text{O}^+$	+	$\text{H}_2$	$3.90 \times 10^{-09}$	284
$\text{H}_2^+$	+	$\text{H}_2\text{O}$	$\rightarrow$	$\text{H}_3\text{O}^+$	+	H	$3.40 \times 10^{-09}$	284
$\text{H}_2^+$	+	CO	$\rightarrow$	$\text{CO}^+$	+	$\text{H}_2$	$6.44 \times 10^{-10}$	284
$\text{H}_2^+$	+	$\text{H}^-$	$\rightarrow$	$\text{H}_2$	+	H	$2.30 \times 10^{-07}$	284
$\text{H}^+$	+	$\text{CH}_4$	$\rightarrow$	$\text{CH}_4^+$	+	H	$1.50 \times 10^{-09}$	284
$\text{H}^+$	+	$\text{CH}_4$	$\rightarrow$	$\text{CH}_3^+$	+	$\text{H}_2$	$2.30 \times 10^{-09}$	284
$\text{H}^+$	+	$\text{CH}_3$	$\rightarrow$	$\text{CH}_3^+$	+	H	$3.40 \times 10^{-09}$	284
$\text{H}^+$	+	$\text{CH}_2$	$\rightarrow$	$\text{CH}_2^+$	+	H	$1.40 \times 10^{-09}$	284
$\text{H}^+$	+	$\text{CH}_2$	$\rightarrow$	$\text{CH}^+$	+	$\text{H}_2$	$1.40 \times 10^{-09}$	284
$\text{H}^+$	+	CH	$\rightarrow$	$\text{CH}^+$	+	H	$1.90 \times 10^{-09}$	284
$\text{H}^+$	+	$\text{C}_2\text{H}_6$	$\rightarrow$	$\text{C}_2\text{H}_5^+$	+	$\text{H}_2$	$1.30 \times 10^{-09}$	285
$\text{H}^+$	+	$\text{C}_2\text{H}_6$	$\rightarrow$	$\text{C}_2\text{H}_4^+$	+	$\text{H}_2$ + H	$1.40 \times 10^{-09}$	284
$\text{H}^+$	+	$\text{C}_2\text{H}_6$	$\rightarrow$	$\text{C}_2\text{H}_3^+$	+	$2\text{H}_2$	$2.80 \times 10^{-09}$	284
$\text{H}^+$	+	$\text{C}_2\text{H}_5$	$\rightarrow$	$\text{C}_2\text{H}_4^+$	+	$\text{H}_2$	$1.65 \times 10^{-09}$	284
$\text{H}^+$	+	$\text{C}_2\text{H}_5$	$\rightarrow$	$\text{C}_2\text{H}_3^+$	+	$\text{H}_2$ + H	$3.06 \times 10^{-09}$	284
$\text{H}^+$	+	$\text{C}_2\text{H}_4$	$\rightarrow$	$\text{C}_2\text{H}_4^+$	+	H	$1.00 \times 10^{-09}$	284
$\text{H}^+$	+	$\text{C}_2\text{H}_4$	$\rightarrow$	$\text{C}_2\text{H}_3^+$	+	$\text{H}_2$	$3.00 \times 10^{-09}$	284
$\text{H}^+$	+	$\text{C}_2\text{H}_4$	$\rightarrow$	$\text{C}_2\text{H}_2^+$	+	$\text{H}_2$ + H	$1.00 \times 10^{-09}$	284
$\text{H}^+$	+	$\text{C}_2\text{H}_3$	$\rightarrow$	$\text{C}_2\text{H}_3^+$	+	H	$2.00 \times 10^{-09}$	284
$\text{H}^+$	+	$\text{C}_2\text{H}_3$	$\rightarrow$	$\text{C}_2\text{H}_2^+$	+	$\text{H}_2$	$2.00 \times 10^{-09}$	284
$\text{H}^+$	+	$\text{C}_2\text{H}_2$	$\rightarrow$	$\text{C}_2\text{H}_2^+$	+	H	$5.40 \times 10^{-10}$	284
$\text{H}^+$	+	$\text{C}_2\text{H}$	$\rightarrow$	$\text{C}_2\text{H}^+$	+	H	$1.50 \times 10^{-09}$	284
$\text{H}^+$	+	$\text{C}_2\text{H}$	$\rightarrow$	$\text{C}_2^+$	+	$\text{H}_2$	$1.50 \times 10^{-09}$	284
$\text{H}^+$	+	$\text{C}_2$	$\rightarrow$	$\text{C}_2^+$	+	H	$3.10 \times 10^{-09}$	284

Appendices Table A.4.

$H^+$	+	O	$\rightarrow$	$O^+$	+	H	$3.44 \times 10^{-10}$	284
$H^+$	+	$O_2$	$\rightarrow$	$O_2^+$	+	H	$2.00 \times 10^{-09}$	284
$H^+$	+	OH	$\rightarrow$	$OH^+$	+	H	$2.10 \times 10^{-09}$	284
$H^+$	+	$H_2O$	$\rightarrow$	$H_2O^+$	+	H	$6.90 \times 10^{-09}$	284
$H^+$	+	$H^-$	$\rightarrow$	H	+	H	$2.30 \times 10^{-07}$	284
$H^-$	+	$CH_3$	$\rightarrow$	$CH_4$	+	$e^-$	$1.00 \times 10^{-09}$	284
$H^-$	+	$CH_2$	$\rightarrow$	$CH_3$	+	$e^-$	$1.00 \times 10^{-09}$	284
$H^-$	+	CH	$\rightarrow$	$CH_2$	+	$e^-$	$1.00 \times 10^{-10}$	284
$H^-$	+	C	$\rightarrow$	CH	+	$e^-$	$1.00 \times 10^{-09}$	284
$H^-$	+	$C_2H$	$\rightarrow$	$C_2H_2$	+	$e^-$	$1.00 \times 10^{-09}$	284
$H^-$	+	$C_2$	$\rightarrow$	$C_2H$	+	$e^-$	$1.00 \times 10^{-09}$	284
$H^-$	+	H	$\rightarrow$	$H_2$	+	$e^-$	$1.30 \times 10^{-09}$	284
$H^-$	+	O	$\rightarrow$	OH	+	$e^-$	$1.00 \times 10^{-09}$	284
$H^-$	+	OH	$\rightarrow$	$H_2O$	+	$e^-$	$1.00 \times 10^{-10}$	284
$H^-$	+	$H_2O$	$\rightarrow$	$OH^-$	+	$H_2$	$3.80 \times 10^{-09}$	284
$H^-$	+	$O^+$	$\rightarrow$	H	+	O	$2.30 \times 10^{-07}$	284
$H^-$	+	$H_3O^+$	$\rightarrow$	$H_2$	+	OH + H	$2.30 \times 10^{-07}$	284
$H^-$	+	$H_3O^+$	$\rightarrow$	$H_2O$	+	$H_2$	$2.30 \times 10^{-07}$	284
$O^+$	+	$CH_4$	$\rightarrow$	$CH_4^+$	+	O	$8.90 \times 10^{-10}$	284
$O^+$	+	$CH_4$	$\rightarrow$	$CH_3^+$	+	OH	$1.10 \times 10^{-10}$	284
$O^+$	+	$CH_2$	$\rightarrow$	$CH_2^+$	+	O	$9.70 \times 10^{-10}$	284
$O^+$	+	CH	$\rightarrow$	$CH^+$	+	O	$3.50 \times 10^{-10}$	284
$O^+$	+	CH	$\rightarrow$	$CO^+$	+	H	$3.50 \times 10^{-10}$	284
$O^+$	+	$C_2H_4$	$\rightarrow$	$C_2H_4^+$	+	O	$7.00 \times 10^{-11}$	284
$O^+$	+	$C_2H_4$	$\rightarrow$	$C_2H_3^+$	+	OH	$2.10 \times 10^{-10}$	284
$O^+$	+	$C_2H_4$	$\rightarrow$	$C_2H_2^+$	+	$H_2O$	$1.12 \times 10^{-09}$	284

O <sup>+</sup>	+	C <sub>2</sub> H <sub>2</sub>	→	C <sub>2</sub> H <sub>2</sub> <sup>+</sup>	+	O	3.90x10 <sup>-11</sup>	284	
O <sup>+</sup>	+	C <sub>2</sub> H	→	C <sub>2</sub> H <sup>+</sup>	+	O	4.60x10 <sup>-10</sup>	284	
O <sup>+</sup>	+	C <sub>2</sub> H	→	CO <sup>+</sup>	+	CH	4.60x10 <sup>-10</sup>	284	
O <sup>+</sup>	+	C <sub>2</sub>	→	C <sub>2</sub> <sup>+</sup>	+	O	4.80x10 <sup>-10</sup>	284	
O <sup>+</sup>	+	C <sub>2</sub>	→	CO <sup>+</sup>	+	C	4.80x10 <sup>-10</sup>	284	
O <sup>+</sup>	+	H <sub>2</sub>	→	OH <sup>+</sup>	+	H	1.70x10 <sup>-09</sup>	284	
O <sup>+</sup>	+	H	→	H <sup>+</sup>	+	O	5.82x10 <sup>-10</sup>	284	
O <sup>+</sup>	+	O	+ O <sub>2</sub>	→	O <sub>2</sub> <sup>+</sup>	+	O <sub>2</sub>	1.00x10 <sup>-29</sup>	195
O <sup>+</sup>	+	O <sub>2</sub>	→	O <sub>2</sub> <sup>+</sup>	+	O	2.00x10 <sup>-11</sup>	195	
O <sup>+</sup>	+	O <sub>3</sub>	→	O <sub>2</sub> <sup>+</sup>	+	O <sub>2</sub>	1.00x10 <sup>-10</sup>	241	
O <sup>+</sup>	+	OH	→	OH <sup>+</sup>	+	O	3.60x10 <sup>-10</sup>	284	
O <sup>+</sup>	+	OH	→	O <sub>2</sub> <sup>+</sup>	+	H	3.60x10 <sup>-10</sup>	284	
O <sup>+</sup>	+	H <sub>2</sub> O	→	H <sub>2</sub> O <sup>+</sup>	+	O	3.20x10 <sup>-09</sup>	284	
O <sup>+</sup>	+	CO <sub>2</sub>	→	O <sub>2</sub> <sup>+</sup>	+	CO	9.40x10 <sup>-10</sup>	284	
O <sup>+</sup>	+	CO	→	CO <sup>+</sup>	+	O	1.15x10 <sup>-18</sup>	284	
O <sup>+</sup>	+	O <sup>-</sup>	→	O	+	O	4.00x10 <sup>-08</sup>	287	
O <sup>+</sup>	+	O <sup>-</sup>	+ O	→	O <sub>2</sub>	+	O	2.00x10 <sup>-25</sup>	195
O <sup>+</sup>	+	O <sup>-</sup>	+ O <sub>2</sub>	→	O <sub>2</sub>	+	O <sub>2</sub>	2.00x10 <sup>-25</sup>	195
O <sup>+</sup>	+	O <sub>2</sub> <sup>-</sup>	→	O	+	O <sub>2</sub>	2.70x10 <sup>-07</sup>	287	
O <sup>+</sup>	+	O <sub>2</sub> <sup>-</sup>	+ O <sub>2</sub>	→	O <sub>3</sub>	+	O <sub>2</sub>	2.00x10 <sup>-25</sup>	195
O <sup>+</sup>	+	O <sub>3</sub> <sup>-</sup>	→	O <sub>3</sub>	+	O	1.00x10 <sup>-07</sup>	195	
O <sub>2</sub> <sup>+</sup>	+	CH <sub>2</sub>	→	CH <sub>2</sub> <sup>+</sup>	+	O <sub>2</sub>	4.30x10 <sup>-10</sup>	284	
O <sub>2</sub> <sup>+</sup>	+	CH	→	CH <sup>+</sup>	+	O <sub>2</sub>	3.10x10 <sup>-10</sup>	284	
O <sub>2</sub> <sup>+</sup>	+	C	→	CO <sup>+</sup>	+	O	5.20x10 <sup>-11</sup>	284	
O <sub>2</sub> <sup>+</sup>	+	C	→	C <sup>+</sup>	+	O <sub>2</sub>	5.20x10 <sup>-11</sup>	284	
O <sub>2</sub> <sup>+</sup>	+	C <sub>2</sub> H <sub>4</sub>	→	C <sub>2</sub> H <sub>4</sub> <sup>+</sup>	+	O <sub>2</sub>	6.80x10 <sup>-10</sup>	284	

Appendices Table A.4.

O <sub>2</sub> <sup>+</sup>	+	C <sub>2</sub> H <sub>2</sub>	→	C <sub>2</sub> H <sub>2</sub> <sup>+</sup>	+	O <sub>2</sub>	1.11x10 <sup>-09</sup>	284				
O <sub>2</sub> <sup>+</sup>	+	C <sub>2</sub>	→	C <sub>2</sub> <sup>+</sup>	+	O <sub>2</sub>	4.10x10 <sup>-10</sup>	284				
O <sub>2</sub> <sup>+</sup>	+	C <sub>2</sub>	→	CO <sup>+</sup>	+	CO	4.10x10 <sup>-10</sup>	284				
O <sub>2</sub> <sup>+</sup>	+	O <sub>2</sub>	+	O <sub>2</sub>	→	O <sub>4</sub> <sup>+</sup>	+	O <sub>2</sub>	2.40x10 <sup>-30</sup>	241		
O <sub>2</sub> <sup>+</sup>	+	O <sup>-</sup>	→	O	+	O <sub>2</sub>	2.60x10 <sup>-08</sup>	287				
O <sub>2</sub> <sup>+</sup>	+	O <sup>-</sup>	→	O	+	O	+	O	2.60x10 <sup>-08</sup>	287		
O <sub>2</sub> <sup>+</sup>	+	O <sup>-</sup>	+	O <sub>2</sub>	→	O <sub>3</sub>	+	O <sub>2</sub>	2.00x10 <sup>-25</sup>	195		
O <sub>2</sub> <sup>+</sup>	+	O <sub>2</sub> <sup>-</sup>	→	O <sub>2</sub>	+	O <sub>2</sub>	2.00x10 <sup>-07</sup>	287				
O <sub>2</sub> <sup>+</sup>	+	O <sub>2</sub> <sup>-</sup>	→	O <sub>2</sub>	+	O	+	O	1.00x10 <sup>-07</sup>	195		
O <sub>2</sub> <sup>+</sup>	+	O <sub>2</sub> <sup>-</sup>	+	O <sub>2</sub>	→	O <sub>2</sub>	+	O <sub>2</sub>	+	O <sub>2</sub>	2.00x10 <sup>-25</sup>	195
O <sub>2</sub> <sup>+</sup>	+	O <sub>3</sub> <sup>-</sup>	→	O <sub>2</sub>	+	O <sub>3</sub>	2.00x10 <sup>-07</sup>	195				
O <sub>2</sub> <sup>+</sup>	+	O <sub>3</sub> <sup>-</sup>	→	O	+	O	+	O <sub>3</sub>	1.00x10 <sup>-07</sup>	195		
O <sub>4</sub> <sup>+</sup>	+	O	→	O <sub>2</sub> <sup>+</sup>	+	O <sub>3</sub>	3.00x10 <sup>-10</sup>	241				
O <sub>4</sub> <sup>+</sup>	+	O <sub>2</sub>	→	O <sub>2</sub> <sup>+</sup>	+	O <sub>2</sub>	+	O <sub>2</sub>	1.73x10 <sup>-13</sup>	241		
O <sup>-</sup>	+	CH <sub>4</sub>	→	OH <sup>-</sup>	+	CH <sub>3</sub>	1.00x10 <sup>-10</sup>	284				
O <sup>-</sup>	+	C	→	CO	+	e <sup>-</sup>	5.00x10 <sup>-10</sup>	284				
O <sup>-</sup>	+	H <sub>2</sub>	→	H <sub>2</sub> O	+	e <sup>-</sup>	7.00x10 <sup>-10</sup>	284				
O <sup>-</sup>	+	H <sub>2</sub>	→	OH <sup>-</sup>	+	H	3.00x10 <sup>-11</sup>	284				
O <sup>-</sup>	+	H	→	OH	+	e <sup>-</sup>	5.00x10 <sup>-10</sup>	284				
O <sup>-</sup>	+	O	→	O <sub>2</sub>	+	e <sup>-</sup>	2.30x10 <sup>-10</sup>	287				
O <sup>-</sup>	+	O <sub>2</sub>	→	O	+	O <sub>2</sub>	+	e <sup>-</sup>	k = f(E/N)	195		
O <sup>-</sup>	+	O <sub>2</sub>	→	O <sub>2</sub> <sup>-</sup>	+	O	k = f(E/N)	195				
O <sup>-</sup>	+	O <sub>2</sub>	→	O <sub>3</sub>	+	e <sup>-</sup>	5.00x10 <sup>-15</sup>	195				
O <sup>-</sup>	+	O <sub>2</sub>	+	O <sub>2</sub>	→	O <sub>3</sub> <sup>-</sup>	+	O <sub>2</sub>	1.10x10 <sup>-30</sup>	195		
O <sup>-</sup>	+	O <sub>3</sub>	→	O <sub>3</sub> <sup>-</sup>	+	O	5.30x10 <sup>-10</sup>	195				
O <sup>-</sup>	+	O <sub>3</sub>	→	O <sub>2</sub>	+	O <sub>2</sub>	+	e <sup>-</sup>	3.00x10 <sup>-10</sup>	288		

$O^-$	+	CO	→	CO <sub>2</sub>	+	e <sup>-</sup>	6.50x10 <sup>-10</sup>	284
O <sub>2</sub> <sup>-</sup>	+	O	→	O <sup>-</sup>	+	O <sub>2</sub>	3.30x10 <sup>-10</sup>	195
O <sub>2</sub> <sup>-</sup>	+	O	→	O <sub>3</sub>	+	e <sup>-</sup>	3.30x10 <sup>-10</sup>	287
O <sub>2</sub> <sup>-</sup>	+	O <sub>2</sub>	→	O <sub>2</sub>	+	O <sub>2</sub> + e <sup>-</sup>	2.18x10 <sup>-18</sup>	195
O <sub>2</sub> <sup>-</sup>	+	O <sub>2</sub> + O <sub>2</sub>	→	O <sub>4</sub> <sup>-</sup>	+	O <sub>2</sub>	3.50x10 <sup>-31</sup>	241
O <sub>2</sub> <sup>-</sup>	+	O <sub>3</sub>	→	O <sub>3</sub> <sup>-</sup>	+	O <sub>2</sub>	4.00x10 <sup>-10</sup>	195
O <sub>3</sub> <sup>-</sup>	+	O	→	O <sup>-</sup>	+	O <sub>3</sub>	1.00x10 <sup>-13</sup>	288
O <sub>3</sub> <sup>-</sup>	+	O	→	O <sub>2</sub>	+	O <sub>2</sub> + e <sup>-</sup>	3.00x10 <sup>-10</sup>	241
O <sub>3</sub> <sup>-</sup>	+	O	→	O <sub>2</sub> <sup>-</sup>	+	O <sub>2</sub>	3.20x10 <sup>-10</sup>	241
O <sub>3</sub> <sup>-</sup>	+	O <sub>2</sub>	→	O <sub>3</sub>	+	O <sub>2</sub> + e <sup>-</sup>	2.30x10 <sup>-11</sup>	195
O <sub>3</sub> <sup>-</sup>	+	O <sub>3</sub>	→	O <sub>2</sub>	+	O <sub>2</sub> + O <sub>2</sub> + e <sup>-</sup>	1.00x10 <sup>-12</sup>	288
O <sub>4</sub> <sup>-</sup>	+	O	→	O <sub>3</sub> <sup>-</sup>	+	O <sub>2</sub>	4.00x10 <sup>-10</sup>	241
O <sub>4</sub> <sup>-</sup>	+	O	→	O <sup>-</sup>	+	O <sub>2</sub> + O <sub>2</sub>	3.00x10 <sup>-10</sup>	241
O <sub>4</sub> <sup>-</sup>	+	O <sub>2</sub>	→	O <sub>2</sub> <sup>-</sup>	+	O <sub>2</sub> + O <sub>2</sub>	3.08x10 <sup>-12</sup>	241
CO <sub>2</sub> <sup>+</sup>	+	CH <sub>4</sub>	→	CH <sub>4</sub> <sup>+</sup>	+	CO <sub>2</sub>	5.50x10 <sup>-10</sup>	284
CO <sub>2</sub> <sup>+</sup>	+	C <sub>2</sub> H <sub>4</sub>	→	C <sub>2</sub> H <sub>4</sub> <sup>+</sup>	+	CO <sub>2</sub>	1.50x10 <sup>-10</sup>	284
CO <sub>2</sub> <sup>+</sup>	+	C <sub>2</sub> H <sub>2</sub>	→	C <sub>2</sub> H <sub>2</sub> <sup>+</sup>	+	CO <sub>2</sub>	7.30x10 <sup>-10</sup>	284
CO <sub>2</sub> <sup>+</sup>	+	O <sub>2</sub>	→	O <sub>2</sub> <sup>+</sup>	+	CO <sub>2</sub>	5.30x10 <sup>-11</sup>	284
CO <sub>2</sub> <sup>+</sup>	+	O	→	O <sub>2</sub> <sup>+</sup>	+	CO	1.64x10 <sup>-10</sup>	284
CO <sub>2</sub> <sup>+</sup>	+	O	→	O <sup>+</sup>	+	CO <sub>2</sub>	9.62x10 <sup>-11</sup>	284
CO <sub>2</sub> <sup>+</sup>	+	H <sub>2</sub> O	→	H <sub>2</sub> O <sup>+</sup>	+	CO <sub>2</sub>	2.04x10 <sup>-09</sup>	284
CO <sup>+</sup>	+	CH <sub>4</sub>	→	CH <sub>4</sub> <sup>+</sup>	+	CO	7.93x10 <sup>-10</sup>	284
CO <sup>+</sup>	+	CH <sub>2</sub>	→	CH <sub>2</sub> <sup>+</sup>	+	CO	4.30x10 <sup>-10</sup>	284
CO <sup>+</sup>	+	CH	→	CH <sup>+</sup>	+	CO	3.20x10 <sup>-10</sup>	284
CO <sup>+</sup>	+	C	→	C <sup>+</sup>	+	CO	1.10x10 <sup>-10</sup>	284
CO <sup>+</sup>	+	C <sub>2</sub> H	→	C <sub>2</sub> H <sup>+</sup>	+	CO	3.90x10 <sup>-10</sup>	284

Appendices Table A.4.

$\text{CO}^+$	+	$\text{C}_2$	$\rightarrow$	$\text{C}_2^+$	+	$\text{CO}$	$8.40 \times 10^{-10}$	284
$\text{CO}^+$	+	$\text{H}$	$\rightarrow$	$\text{H}^+$	+	$\text{CO}$	$7.50 \times 10^{-10}$	284
$\text{CO}^+$	+	$\text{O}_2$	$\rightarrow$	$\text{O}_2^+$	+	$\text{CO}$	$1.20 \times 10^{-10}$	284
$\text{CO}^+$	+	$\text{O}$	$\rightarrow$	$\text{O}^+$	+	$\text{CO}$	$1.40 \times 10^{-10}$	284
$\text{CO}^+$	+	$\text{CO}_2$	$\rightarrow$	$\text{CO}_2^+$	+	$\text{CO}$	$1.00 \times 10^{-9}$	284
$\text{CO}^+$	+	$\text{H}_2\text{O}$	$\rightarrow$	$\text{H}_2\text{O}^+$	+	$\text{CO}$	$1.72 \times 10^{-9}$	284
$\text{CO}^+$	+	$\text{OH}$	$\rightarrow$	$\text{OH}^+$	+	$\text{CO}$	$3.10 \times 10^{-10}$	284
$\text{H}_3\text{O}^+$	+	$\text{CH}_2$	$\rightarrow$	$\text{CH}_3^+$	+	$\text{H}_2\text{O}$	$9.40 \times 10^{-10}$	284
$\text{H}_3\text{O}^+$	+	$\text{CH}$	$\rightarrow$	$\text{CH}_2^+$	+	$\text{H}_2\text{O}$	$6.80 \times 10^{-10}$	284
$\text{H}_3\text{O}^+$	+	$\text{C}_2\text{H}_3$	$\rightarrow$	$\text{C}_2\text{H}_4^+$	+	$\text{H}_2\text{O}$	$2.00 \times 10^{-9}$	284
$\text{H}_3\text{O}^+$	+	$\text{C}_2$	$\rightarrow$	$\text{C}_2\text{H}^+$	+	$\text{H}_2\text{O}$	$9.20 \times 10^{-10}$	284
$\text{H}_2\text{O}^+$	+	$\text{CH}_4$	$\rightarrow$	$\text{H}_3\text{O}^+$	+	$\text{CH}_3$	$1.40 \times 10^{-9}$	284
$\text{H}_2\text{O}^+$	+	$\text{CH}_2$	$\rightarrow$	$\text{CH}_3^+$	+	$\text{OH}$	$4.70 \times 10^{-10}$	284
$\text{H}_2\text{O}^+$	+	$\text{CH}_2$	$\rightarrow$	$\text{CH}_2^+$	+	$\text{H}_2\text{O}$	$4.70 \times 10^{-10}$	284
$\text{H}_2\text{O}^+$	+	$\text{CH}$	$\rightarrow$	$\text{CH}_2^+$	+	$\text{OH}$	$3.40 \times 10^{-10}$	284
$\text{H}_2\text{O}^+$	+	$\text{CH}$	$\rightarrow$	$\text{CH}^+$	+	$\text{H}_2\text{O}$	$3.40 \times 10^{-10}$	284
$\text{H}_2\text{O}^+$	+	$\text{C}$	$\rightarrow$	$\text{CH}^+$	+	$\text{OH}$	$1.10 \times 10^{-9}$	284
$\text{H}_2\text{O}^+$	+	$\text{C}_2\text{H}_6$	$\rightarrow$	$\text{H}_3\text{O}^+$	+	$\text{C}_2\text{H}_5$	$1.33 \times 10^{-9}$	284
$\text{H}_2\text{O}^+$	+	$\text{C}_2\text{H}_6$	$\rightarrow$	$\text{C}_2\text{H}_6^+$	+	$\text{H}_2\text{O}$	$6.40 \times 10^{-11}$	284
$\text{H}_2\text{O}^+$	+	$\text{C}_2\text{H}_6$	$\rightarrow$	$\text{C}_2\text{H}_4^+$	+	$\text{H}_2\text{O} + \text{H}_2$	$1.92 \times 10^{-10}$	284
$\text{H}_2\text{O}^+$	+	$\text{C}_2\text{H}_4$	$\rightarrow$	$\text{C}_2\text{H}_4^+$	+	$\text{H}_2\text{O}$	$1.50 \times 10^{-9}$	284
$\text{H}_2\text{O}^+$	+	$\text{C}_2\text{H}_2$	$\rightarrow$	$\text{C}_2\text{H}_2^+$	+	$\text{H}_2\text{O}$	$1.90 \times 10^{-9}$	284
$\text{H}_2\text{O}^+$	+	$\text{C}_2\text{H}$	$\rightarrow$	$\text{C}_2\text{H}_2^+$	+	$\text{OH}$	$4.40 \times 10^{-10}$	284
$\text{H}_2\text{O}^+$	+	$\text{C}_2\text{H}$	$\rightarrow$	$\text{C}_2\text{H}^+$	+	$\text{H}_2\text{O}$	$4.40 \times 10^{-10}$	284
$\text{H}_2\text{O}^+$	+	$\text{C}_2$	$\rightarrow$	$\text{C}_2\text{H}^+$	+	$\text{OH}$	$4.70 \times 10^{-10}$	284
$\text{H}_2\text{O}^+$	+	$\text{C}_2$	$\rightarrow$	$\text{C}_2^+$	+	$\text{H}_2\text{O}$	$4.70 \times 10^{-10}$	284

$\text{H}_2\text{O}^+$	+	$\text{H}_2$	$\rightarrow$	$\text{H}_3\text{O}^+$	+	$\text{H}$	$6.40 \times 10^{-10}$	<sup>284</sup>
$\text{H}_2\text{O}^+$	+	$\text{O}_2$	$\rightarrow$	$\text{O}_2^+$	+	$\text{H}_2\text{O}$	$4.60 \times 10^{-10}$	<sup>284</sup>
$\text{H}_2\text{O}^+$	+	$\text{O}$	$\rightarrow$	$\text{O}_2^+$	+	$\text{H}_2$	$4.00 \times 10^{-11}$	<sup>284</sup>
$\text{H}_2\text{O}^+$	+	$\text{H}_2\text{O}$	$\rightarrow$	$\text{H}_3\text{O}^+$	+	$\text{OH}$	$2.10 \times 10^{-09}$	<sup>284</sup>
$\text{H}_2\text{O}^+$	+	$\text{OH}$	$\rightarrow$	$\text{H}_3\text{O}^+$	+	$\text{O}$	$6.90 \times 10^{-10}$	<sup>284</sup>
$\text{OH}^+$	+	$\text{CH}_4$	$\rightarrow$	$\text{CH}_5^+$	+	$\text{O}$	$1.95 \times 10^{-10}$	<sup>284</sup>
$\text{OH}^+$	+	$\text{CH}_4$	$\rightarrow$	$\text{H}_3\text{O}^+$	+	$\text{CH}_2$	$1.31 \times 10^{-09}$	<sup>284</sup>
$\text{OH}^+$	+	$\text{CH}_2$	$\rightarrow$	$\text{CH}_3^+$	+	$\text{O}$	$4.80 \times 10^{-10}$	<sup>284</sup>
$\text{OH}^+$	+	$\text{CH}_2$	$\rightarrow$	$\text{CH}_2^+$	+	$\text{OH}$	$4.80 \times 10^{-10}$	<sup>284</sup>
$\text{OH}^+$	+	$\text{CH}$	$\rightarrow$	$\text{CH}_2^+$	+	$\text{O}$	$3.50 \times 10^{-10}$	<sup>284</sup>
$\text{OH}^+$	+	$\text{CH}$	$\rightarrow$	$\text{CH}^+$	+	$\text{OH}$	$3.50 \times 10^{-10}$	<sup>284</sup>
$\text{OH}^+$	+	$\text{C}$	$\rightarrow$	$\text{CH}^+$	+	$\text{O}$	$1.20 \times 10^{-09}$	<sup>284</sup>
$\text{OH}^+$	+	$\text{C}_2\text{H}_6$	$\rightarrow$	$\text{H}_3\text{O}^+$	+	$\text{C}_2\text{H}_4$	$1.60 \times 10^{-10}$	<sup>284</sup>
$\text{OH}^+$	+	$\text{C}_2\text{H}_6$	$\rightarrow$	$\text{C}_2\text{H}_6^+$	+	$\text{OH}$	$4.80 \times 10^{-11}$	<sup>284</sup>
$\text{OH}^+$	+	$\text{C}_2\text{H}_6$	$\rightarrow$	$\text{C}_2\text{H}_5^+$	+	$\text{H}_2 + \text{O}$	$3.20 \times 10^{-10}$	<sup>284</sup>
$\text{OH}^+$	+	$\text{C}_2\text{H}_6$	$\rightarrow$	$\text{C}_2\text{H}_4^+$	+	$\text{H}_2 + \text{OH}$	$1.04 \times 10^{-09}$	<sup>284</sup>
$\text{OH}^+$	+	$\text{C}_2\text{H}$	$\rightarrow$	$\text{C}_2\text{H}_2^+$	+	$\text{O}$	$4.50 \times 10^{-10}$	<sup>284</sup>
$\text{OH}^+$	+	$\text{C}_2\text{H}$	$\rightarrow$	$\text{C}_2\text{H}^+$	+	$\text{OH}$	$4.50 \times 10^{-10}$	<sup>284</sup>
$\text{OH}^+$	+	$\text{C}_2$	$\rightarrow$	$\text{C}_2\text{H}^+$	+	$\text{O}$	$4.80 \times 10^{-10}$	<sup>284</sup>
$\text{OH}^+$	+	$\text{C}_2$	$\rightarrow$	$\text{C}_2^+$	+	$\text{OH}$	$4.80 \times 10^{-10}$	<sup>284</sup>
$\text{OH}^+$	+	$\text{H}_2$	$\rightarrow$	$\text{H}_2\text{O}^+$	+	$\text{H}$	$1.01 \times 10^{-09}$	<sup>284</sup>
$\text{OH}^+$	+	$\text{O}_2$	$\rightarrow$	$\text{O}_2^+$	+	$\text{OH}$	$5.90 \times 10^{-10}$	<sup>284</sup>
$\text{OH}^+$	+	$\text{O}$	$\rightarrow$	$\text{O}_2^+$	+	$\text{H}$	$7.10 \times 10^{-10}$	<sup>284</sup>
$\text{OH}^+$	+	$\text{H}_2\text{O}$	$\rightarrow$	$\text{H}_2\text{O}^+$	+	$\text{OH}$	$1.59 \times 10^{-09}$	<sup>284</sup>
$\text{OH}^+$	+	$\text{H}_2\text{O}$	$\rightarrow$	$\text{H}_3\text{O}^+$	+	$\text{O}$	$1.30 \times 10^{-09}$	<sup>284</sup>
$\text{OH}^+$	+	$\text{OH}$	$\rightarrow$	$\text{H}_2\text{O}^+$	+	$\text{O}$	$7.00 \times 10^{-10}$	<sup>284</sup>



Appendices Table A.4.

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$\text{OH}^-$	+	$\text{CH}_3$	$\rightarrow$	$\text{CH}_3\text{OH}$	+	$\text{e}^-$	$1.00 \times 10^{-09}$	<sup>284</sup>
$\text{OH}^-$	+	$\text{CH}$	$\rightarrow$	$\text{CH}_2\text{O}$	+	$\text{e}^-$	$5.00 \times 10^{-10}$	<sup>284</sup>
$\text{OH}^-$	+	$\text{C}$	$\rightarrow$	$\text{CHO}$	+	$\text{e}^-$	$5.00 \times 10^{-10}$	<sup>284</sup>
$\text{OH}^-$	+	$\text{H}$	$\rightarrow$	$\text{H}_2\text{O}$	+	$\text{e}^-$	$1.40 \times 10^{-09}$	<sup>284</sup>

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